# product CUIDE 

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## About Unbrako



West Coast Distribution Center

Founded in 1911, Unbrako is the world leader in advancing the technology of bolted joints and meeting the needs of industry for stronger and better performing fasteners. Products such as the famous Unbrako ${ }^{\circledR}$ socket head cap screw and Durlok ${ }^{\circledR}$ fasteners are the solutions of choice for engineering applications across the world \& is used by industries such as the automotive, power generation, petrochemical, heavy machinery, construction and military sectors.

With an extensive international network in 35 countries, Unbrako provides a complete range of industrial fastening hardware including bolts, screws, SEM's, nuts, studbolts, self-locking fasteners, thread forming fasteners, among others.

Unbrako products are primarily used in performance critical applications and incorporate unique design and work-manship features that meet or exceed recognized international standards, resulting in higher tensile strength, improved fatigue resistance, ease of installation, reduced total cost of maintenance and extended life cycle.

With advanced manufacturing, engineering and logistics facilities, ISO/TS and CE certification, Unbrako is equipped to provide technical support and full-service package. Unbrako's focus is on building long - term relationships with its customers. Full-service includes engineering and design support, procurement and purchasing services, localized warehousing and transport, a variety of packaging options and choice of delivery frequencies - to provide the right answer to any customer need.

## In this Guide

In this guide you will find complete information about Unbrako socket screws, pins, hex keys, self locking Durlok ${ }^{\circledR}$ fasteners and related products, in high-tensile alloy steel. Everything you need to select, specify and order these precision products is at your finger tips. Furthermore, all data has been organized to let you find the facts you want with the greatest speed and least effort.

## Included in this guide are:

- Unbrako fastener product descriptions
- Features and technical data about each product
- Product sizes along with part numbers
- Technical discussions for application and use


## Packaging:

Unbrako provides a full-service package designed to suit customer needs, including a variety of packaging options and choice of delivery frequencies. The standard packaging is explained with each product.

## Types of packaging:

Pieces per Box - small box packingPieces per Carton - bulk packing in a cartonPieces per Bag - bulk packing in a bag
## Important Information

The use of precision fasteners in the worldwide market has led to the creation of many standards. These standards specify the fastener requirements: dimensions, material, strength levels, inspection etc. Different standards are the responsibility of various organization and are not always identical. Unbrako supplies precision fasteners manufactured to Unbrako internal specifications, designed to achieve maximum interchangeability with all standards. Reference Consensus standards referred to in this guide were current at the time of publication. However, Reference Consensus standards are subject to change by any standards organizations at any time.

A direct or indirect reference to a consensus standard to represent that a fastener conforms to particular requirements of the consensus standard shall not be construed as a representation that the fastener meets all the requirements of the consensus standard.

UNBRAKO products are manufactured in accordance with revisions valid at time of manufacture. Unbrako reserves the right to update or modify its manufacturing specifications without prior notice.

The specifications and other particulars contained in this Guide are subject to change without notice.


## Limited Warranty and Exclusive Remedy



Deepak Fasteners Ltd., through its Unbrako Division and associated companies, warrants that these products conform to industry standards specified herein and will be free from defects in materials and workmanship. This warranty is expressly given in lieu of any and all other express or implied warranties, including any implied warranty of merchantability or fitness for a particular purpose, and in lieu of any other obligation on the part of Deepak Fasteners.

Deepak Fasteners will at its option, repair or replace free of charge (excluding all shipping and handling costs) any products which have not been subject to misuse, abuse, or modification and which in its sole determination were not manufactured in compliance with the warranty given above.

Deepak Fasteners makes no representations or warranties, express or implied, that anything imported, made, used, sold, or otherwise provided under any sale agreement is or will be free from infringement of patents / other proprietary rights of any third persons. Nothing in this application, or any agreement, shall be construed as giving rise to any obligation on Deepak Fasteners part to indemnify or hold harmless any Buyer from any liability relating to Buyer's purchase, use, or re-sale of Deepak Fasteners product, or the incorporation of Deepak Fasteners product into another manufactured product.

The remedy provided herein shall be the exclusive remedy for any breach of warranty or any claim arising in any way out of the manufacture, sale or use of these products. In no event shall Deepak Fasteners be liable for consequential, incidental or any other damages of any nature whatsoever except those specifically provided herein for any breach of warranty or any claim arising in any way of the manufacture, sale or use of these products. No other person is authorized by Deepak Fasteners to give any other warranty, written or oral, pertaining to the products.


## Certified Laboratory

Our Laboratory is NABL ISO/IEC 17025:2005 certified, which facilitates in maintaining consistently high quality. The fasteners go through strict quality checks at every stage of the process. Our inspection facilities are equipped with state-of-the-art equipment for testing of both physical and metallurgical aspects of fasteners for the most demanding applications:

- Tensile \& Hardness testing
- Salt spray testing
- Digital profile analysis
- X-ray analysis of coating thickness
- Chemical composition analysis (Spectrometer)
- Impact Testing
- Dynamic fatigue testing
- Torque tension and friction testing
- Eddy current Testing
- Metallurgical Microscope with Image Analyzer



## International Certifications

Our production facilities are ISO 9001, ISO/TS 16949, ISO 14001 and BS OHSAS 18001 Certified. Our fasteners meet or exceed International Standards like DIN, ISO, ASTM, IS, BS etc. We have expertise not only in standard products, but also in made-to-order customized products.

## Specialized Coatings

We excel in a variety of coatings, which are done in-house. These are designed to provide required protection in different environments, e.g. Hot Dip Galvanizing, Mechanical Galvanizing, Electroplating (Zinc \& Copper Cadmium), PTFE Coating, Zinc-AI Flake Coating (Geomet, Delta Protekt) and Unbrako Wiscoat Coating.

## Specialized Coatings

A Product's lifespan and performance is not only measured by it's quality, grade and and specification, but also by it's surface finish. Choosing the correct coating for the application will prevent corrosion, enhance aesthetic value and add strength to the fastener, extending it's life and performance.

Unbrako excels in a variety of coatings done in-house, designed specifically to provide the required protection in such harsh environment. Technical information of a few of these coatings is set out below:

| MAIN COATINGS |  | ELECTROLYTIC COATINGS ZINC CADMIUM | HOT-DIP <br> GALVANISATION | METALLIC COATING ZINC FLAKE | PTFE |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Type of material |  | All metals | Steels | All metals | All metals |
| Process temperature |  | Bath $\mathrm{t}^{\circ}<90^{\circ} \mathrm{C}$ <br> Baking temp. $<250^{\circ} \mathrm{C}$ | $460^{\circ} \mathrm{C}-550^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}$ Process <br> $300^{\circ} \mathrm{C}$ Baking | $300^{\circ} \mathrm{C}$ Baking |
| Maximum service temperature without damage of coating |  | Zinc: $250^{\circ} \mathrm{C}$ Max <br> Cadmium : $235^{\circ} \mathrm{C}$ Max <br> chromating <br> Zinc \& Cadmium : <br> $70^{\circ} \mathrm{C}$ max | $300^{\circ} \mathrm{C}$ max | $280^{\circ} \mathrm{C}$ max | $280^{\circ} \mathrm{C}$ max |
| Usual thickness |  | Cadmium : <br> $3 \mu \mathrm{~m}$ to $20 \mu \mathrm{~m}$ | Individual - $43 \mu \mathrm{~m}$ Average $-54 \mu \mathrm{~m}$ | $5 \mu \mathrm{~m}-15 \mu \mathrm{~m}$ | $10 \mu \mathrm{~m}-20 \mu \mathrm{~m}$ |
| Average <br> Friction <br> Coefficient <br> Average <br> Friction <br> Coefficient | without lubrication | 0.16-0.22 | Seizure risks when bolt stress is $>40 \% \mathrm{YS}$ | 0.15-0.25 | 0.15-0.25 |
|  | with lubrication | 0.08-0.12 | 0.13-0.18 | 0.08-0.12 | 0.08-0.12 |
| Salt spray test (red corrosion) |  | Zine 5 to $7 \mu \mathrm{~m}: 48 \mathrm{~h}$ min Zinc chromating 5 to $7 \mu \mathrm{~m}$ : 96 h min Reinforced chromating : 200 hmin | $70 \mu \mathrm{~m}: 400 \mathrm{~h} \mathrm{~min}$ | 5-7 $\mu \mathrm{m}: 400 \mathrm{~h}$ min <br> 8-10 $\mu \mathrm{m}$ : <br> 1000h min | 1000h min |
| Hydrogen embrittlement |  | Descaling with inhibitor imperative baking for 100 Mpa steels | Descaling with inhibitor No risk process | No risk process | No risk process |
| Aspect |  | Bright | Matt or glossy | Matt aluminum | Matt Blue |

NOTE:- Specialist assistance is recommended when selecting these coatings.

## Quality Standards

## 1. Company Approvals:

Unbrako manufacturing facilities are approved to BS EN ISO 9001:2008
ISO/TS 16949:2009
BS OHSAS 18001:2007
ISO/TS 14001:2004
ISO 9001:2008
EN 14399 \& 15048

## 2. Quality Levels:

2.1 Final acceptance of a consignment is determined by applying attribute sampling plans as defined in BS 6001 Double sampling tables Level 1 (Normal Inspection).

### 2.2 Acceptance Levels are as follows:

2.2.1 Major Characteristics 1.5\% A.Q.L.
2.2.2 Minor (A) Characteristics 2.5\% A.Q.L.
2.2.3 Incidental (Minor B) Characteristics 4.0\% A.Q.L.
2.2.4 A.Q.L. for characteristics identified as critical by the user will be established by negotiation.
2.2.5 Zero acceptance for mixed, scrap or mutilated parts (100\% sort).

### 2.3 The following identifies the characteristics classified as Major, Minor (A) and Incidental (Minor B).

### 2.3.1 Major

i. Thread conformance
ii. Dimensions with a tolerance equal to or less than 0.002" total.
iii. Angles with a tolerance equal to or less than $1^{\circ}$ total.
iv. Surface texture equal to or less than 16 CLA.
v. Post Heat Treatment physical testing.
vi. Surface discontinuities.
vii. Straightness
viii. Concentricity e.g. Head/Shank/Thread.
ix. Underhead fillet area / bearing surface squareness.
x. Thread run-out.
xi. Hexagon Socket.
xii. Grip Length.

### 2.3.2 Minor (A)

i. Dimensions with a tolerance greater than $0.002^{\prime \prime}$ but not exceeding 0.008".
ii. Angles with a tolerance varying from $1^{\circ}$ up to and including $5^{\circ}$.
iii. Surface texture greater than 16 CLA and equal to or less than 32 CLA.
iv. Identification.
v. Burrs and tool marks.

### 2.3.3 Incidental (Minor B)

i. Dimensions with a tolerance greater than $0.008^{\prime \prime}$ total.
ii. Angles with a tolerance greater than $5^{\circ}$ total.
iii. Surface texture greater than 32 CLA.
iv. Visual characteristics.

## 3. Certifications:

Unbrako Standard Socket screw products carry a Certificate of Conformity on each and every box, incorporating a lot traceable number, free of charge.

In addition Socket Head Cap Screws greater than and equal to $1 / 4^{\prime \prime}$ and M5 have an e-code identifier stamped on the head of each part, allowing traceability even when the original box and label is not available.

Additionally, the following test certificates are available, subject to extra charge:
i. To DIN 50049 2.1 (EN10204 TYPE 2.1 CERT)
ii. To DIN 50049 2.2 (EN 10204 TYPE 2.2 CERT)
iii. To DIN 50049 2.3 (EN 10204 TYPE 2.2 CERT)
iv. To DIN 50049 3.1A (EN 10204 TYPE 3.1 CERT)
v. To DIN 50049 3.1B (EN 10204 TYPE 3.1 CERT)
vi. To DIN 50049 3.1C (EN 10204 TYPE 3.2 CERT)

## Product Terminology



## BODY

The unthreaded portion of the shank of a threaded fastener.

FILLET
Concave junction between the head and shank.

## HEAD

A headed fastener has one end enlarged into a preformed shape.

## LENGTH

The length of a headed fastener is the distance from intersection between the bearing surface \& the largest diameter to the extreme end of the fastener, measured parallel to the axis of the fastener. The length of a headless fastener is the distance from one extreme end to the other end, also measured parallel to the fastener.

NOMINAL SIZE
It is the basic major diameter of the thread.

## SHANK

The portion of a headed fastener which lies between the head and the extreme end of the fastener.

TORQUING
It is the act of tightening a fastener by turning either the bolt or nut.

## Thread Terminology



CREST
The outermost tip of a male thread as seen in a thread profile.

## FLANK

The thread surface connecting the crest with the root.

## BEARING SURFACE

The supporting or locating surface of a fastener with respect to the part it fastens or mates.

## MAJOR DIAMETER

The largest diameter of a thread.

## MINOR DIAMETER

The smallest diameter of a thread.
PITCH
The distance from a point on a screw thread to the corresponding point on the next screw thread.

## PITCH DIAMETER

Is the diameter of a theoretical cylinder that passes through the threads at a position that the width of thread ridge and thread groove are equal.

## ROOT

The bottom area between the sides of two adjacent threads.


## Thread Terminology

THREAD LAPS
Are surface defects caused by the folding over of metal in the thread.


## THREAD RUNOUT

is the area between the thread and shank or head of the fasteners The Unbrako radiused root runout provides a smooth from that distributes stress and increases the life of the fastener considerably.

THREAD STRESS AREA
The area of a cylindrical bar of the same material and properties as the thread and capable of supporting the same ultimate tensile load.

## Mechanical Terminology

## CREEP

Deformation that occurs over a period of time when a fastener is subjected to a constant stress at a constant high temperature.


ELONGATION
is the increase in the thread length or a fastener that would occur during tightening or loading.

## ENDURANCE LIMIT

The strength level below which a bolt or joint member will have an essentially infinite life under cyclic loading.

## FATIGUE LIFE

is the number of cycles of fluctuating stress and strain
 of a specified nature that a fastener will sustain before failure occurs.

IMPACT TEST
A test to determine the energy absorbed in fracturing a test bar at high velocity.

PROOF LOAD
is a specified test load which a fastener must withstand without any indication of failure.

## PROOF TEST

is any specified test required for a fastener to indicate that is suitable for the purpose intended.

## ROCKWELL HARDNESS (Hrc)

This is a specific method of measuring the hardness of a fastener. The "c" denotes a specific size indenter which penetrates the surface of the prepared specimen.

## SHEAR JOINT

A joint in which the fastener has the load applied across the axis and which tends to sever it.

## SHEAR STRENGTH

This is the maximum strength of the fastener when it is subjected to shear (transverse) loading.


## TENSILE STRENGTH

Is the force or stress required to break a fastener when the force or stress is applied in straight tension.


TENSION JOINT
A joint in which the fastener has the load applied to the longitudinal direction and which tends to elongate it.

## TORSION

is the twisting force applied to a fastener during tightening.

## YIELD STRENGTH

This is the maximum force or stress that can be applied to a fastener without permanent (plastic) deformationoccurring.


THE WロRLD LEADER

## Influence of Chemicals in Steel



Steel alloys using difference chemical elements are produced in order to improve the physical properties of the material and to achieve special properties:

## Carbon (C)

Although this is not considered to be an alloying element, it is the most important component in steel. It improves tensile strength, hardness and abrasion resistance. It reduces ductility, rigidity and machining.

## Manganese (Mn)

This is an oxidiser and degasifier and reacts with sulphur to improve forgeability. It increases tensile strength, hardness and durability.

## Phosphorus (P)

This increases tensile strength and hardness and improves machinability. It causes fragility in steel.

## Sulphur (S)

Improves machining qualities in the presence of manganese. It reduces weldability, impact, roughness, and ductility.

## Silicon (Si)

This is a deoxidiser and degasifier. It increases tensile strength, elasticity, hardness and forgeability.

## Chromium (Cr)

Increase breaking strength, hardness, durability, roughness, and resistance to high temperatures.

## Nickel (Ni)

This raises strength and hardness, while maintaining ductility and rigidity. It increa ses resistance to cracking and high temperatures.

## Molybdenum (Mo)

This in creases strength, hardness, durability, and rigidity, together with resistance to creaking \& to high temperatures.

## Titanium (Ti)

This is used as a stabilising element in sta inless steels. It has a great affinity for carbon.


## High-performance Socket Screws



## Why Socket Screws? Why Unbrako?

The most important reasons for the increasing use of socket head cap screws in industry are safety, reliability and economy. All three reasons are directly traceable to the superior performance of socket screws vs. other fasteners due to their superior strength and advanced design.

Reliability, higher pressures, stresses and speeds in todays machines and equipment demand stronger, more reliable fasteners to hold them together.

Rising costs make failure and downtime intolerable. Bigger, more complex units break down more frequently despite every effort to prevent it.

This is why the reliability of every component has become critical. Components must stay together to function properly, and to keep them together joints must stay tight.

Unbrako developed the first internal hex socket screw and is the world's leading socket screw brand with more than 100 years' experience of supplying to the highend industries, such as the automotive, infrastructure, aerospace, petrochemical, heavy machinery and military sectors.

UNBRAKO socket cap screws offer joint reliability, safety with maximum strength and fatigue resistance greater than any other threaded fastener.

## Higher Tensile Strength

Unbrako 12.9 metric alloy steel socket head cap screws are manufactured to strength levels of $1300 / 1250 \mathrm{MPa}$ (depending on dia) compared to the industry standard of 1220 MPa . For inch sizes, Unbrako manufactures to 190/180 Ksi compared to the industry standard per ASTM A574 of 180/170 Ksi.

This higher tensile strength can be translated into savings. Fewer socket screws
of the same size can be used to achieve the same clamping force in the joint. A joint requiring $12 \times 1-3 / 8^{\prime \prime}$ Grade 5 hex heads would need only 7 UNBRAKO socket head cap screws. Thus, there are fewer holes to drill \& tap, fewer screws to buy \& handle.

Using smaller diameter socket head cap screws vs. larger hex screws costs less to drill and tap, need less space, require no additional wrench space, take less energy to drive, and there is also weight saving.

## Greater Fatigue Strength

Joints that are subject to external stress loading are susceptible to fatigue failure. UNBRAKO socket screws have distinct advantages that give you an extra bonus of protection against this hazard, namely - design improvements, mechanical properties \& closely controlled manufacturing processes.

## High-performance Socket Screws

Head with increased bearing area for greater load carrying capability. Precision forged for symmetrical grain flow, maximum strength.

Specially designed Elliptical fillet doubles fatigue life at critical head-shank juncture.
" 3 -R" (radiused-root runout) increases fatigue life at this critical juncture.


CONVENTIONAL THREAD
RUNOUT - Note sharp angle at root where high stress concentration soon develops crack which penetrates into body of the screw.

UNBRAKO "3-R" (Radiused Root Runout) THREAD -
Controlled radius of runout root provides a smooth form that distributes stress and increases fatigue life of thread run-out as a much as $300 \%$ in certain sizes.

Total Traceability: Patented E-CODE ${ }^{\text {TM }}$ head marking system allows tracing of test records to specific production batches


Deep, accurate socket for high torque wrenching. Knurls for easier handling. Marked for easier identification.

Fully formed radiused thread increases fatigue life $100 \%$ over flat root thread forms.

Controlled heat treatment produces maximum strength without brittleness and decarburization


Counterbored Protruding


Controlled angle under the head ensures maximum flushness and side wall contact. Non-slip Hex socket prevents marring of material.
Suitable for all high tensile applications. Up to 190,000 psi/ 1300 Mpa- highest of any socket cap screw. Use Stainless for corrosive, cryogenic or elevated temperature environment.

Suitable for use in parts too thin for standard Socket Head Cap Screw and for applications with limited clearance.

Fasten collars, sheaves, gears, knobs on shafts. Locate machine parts. Self-locking knurled cup point is standard. Special Points like Flat, Dog, Cone \& Plain Cup are also available.

Replaces costly special parts - shafts, pivots, pins, guides, linkages and trunnion mountings. Also standard for tool and die industries.

Low head streamline design. Use them in materials too thin to countersink; also for non-critical loading requiring heat treated screws (

## Application / Features

## Micro Series - M1.4 to M2.6



Suitable for all high tensile applications. Up to 1300 Mpa- highest of any socket cap screw.

Equivalent Standards
ISO 4762, DIN 912, ASME B18.3.1M
BS 4168-1
Mechanical Properties

| Screw Size | $\leq$ M16 | $>$ M16 |
| :--- | :--- | :--- |
| Heat Treatment | $40-43 \mathrm{HRC}$ | $40-43 \mathrm{HRC}$ |
| Tensile Strength | $1300 \mathrm{~N} / \mathrm{mm}^{2}$ | $1250 \mathrm{~N} / \mathrm{mm}^{2}$ |
| Yield Strength | $1170 \mathrm{~N} / \mathrm{mm}^{2}$ | $1124 \mathrm{~N} / \mathrm{mm}^{2}$ |
| Shear Strength | $780 \mathrm{~N} / \mathrm{mm}^{2}$ | $750 \mathrm{~N} / \mathrm{mm}^{2}$ |
| Min. Elongation | $9 \%$ | $9 \%$ |

Notes:

1. Property Class : 12.9
2. Thread Class : 4 g 6 g
3. Working Temperature : $-50^{\circ} \mathrm{C}$ to $+300^{\circ} \mathrm{C}$
4. Torques calculated in accordance with

VDI 2230 "Systematic calculation of high duty bolted joints" with o $0.2=1080 \mathrm{~N} / \mathrm{mm}^{2}$ and $\mu=0.125$ for plain finish and $\mu=0.094$ for plated.


Product Dimensions (Micro Sizes)

| Thread Size nom | Pitch | Head <br> Diameter A max | Hex Socket Size W nom | Head <br> Height H max | Transition Dia da nom | Length L |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | min | max |
| M1.4 | 0.30 | 2.6 | 1.27 | 1.4 | 1.8 | 3 | 6 |
| M1.6 | 0.35 | 3.0 | 1.50 | 1.6 | 2.0 | 3 | 6 |
| (M1.7) | 0.35 | 3.0 | 1.50 | 1.7 | 2.1 | 3 | 6 |
| M1.8 | 0.35 | 3.4 | 1.50 | 1.8 | 2.3 | 3 | 6 |
| M2 | 0.40 | 3.8 | 1.50 | 2.0 | 2.6 | 3 | 12 |
| (M2.3) | 0.40 | 4.0 | 2.00 | 2.3 | 2.9 | 4 | 15 |
| M2.5 | 0.45 | 4.5 | 2.00 | 2.5 | 3.1 | 4 | 15 |
| (M2.6) | 0.45 | 4.5 | 2.00 | 2.6 | 3.2 | 4 | 15 |

Thread Recommended Torques Setting

| Size <br> nom | Unplated |  | Plated |  | Induced Load |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Nm | Ibf.in | Nm | Ibf.in | kN | lbf |
| M1.4 | 0.20 | 1.8 | 0.15 | 1.3 | 733 | 164 |
| M1.6 | 0.29 | 2.6 | 0.22 | 2.0 | 930 | 208 |
| (M1.7) | 0.35 | 3.1 | 0.26 | 2.3 | 1,100 | 246 |
| M1.8 | 0.44 | 3.9 | 0.33 | 2.9 | 1,300 | 291 |
| M2 | 0.60 | 5.3 | 0.45 | 4.0 | 1,550 | 347 |
| (M2.3) | 0.95 | 8.4 | 0.71 | 6.3 | 2,230 | 500 |
| M2.5 | 1.21 | 10.7 | 0.90 | 8.0 | 2,590 | 580 |
| (M2.6) | 1.37 | 12.1 | 1.03 | 9.1 | 2,860 | 640 |

[^0]

Suitable for all high tensile applications. Up to 1300 Mpa- highest of any socket cap screw. Use Stainless for corrosive, cryogenic or elevated temperature environments.

## Equivalent Standards

ISO 4762, DIN 912, ASME B18.3.1M
BS 4168-1
Mechanical Properties

| Screw Size | $\leq$ M16 | $>$ M16 |
| :--- | :--- | :--- |
| Heat Treatment | $40-43 \mathrm{HRC}$ | $40-43 \mathrm{HRC}$ |
| Tensile Strength | $1300 \mathrm{~N} / \mathrm{mm}^{2}$ | $1250 \mathrm{~N} / \mathrm{mm}^{2}$ |
| Yield Strength | $1170 \mathrm{~N} / \mathrm{mm}^{2}$ | $1124 \mathrm{~N} / \mathrm{mm}^{2}$ |
| Shear Strength | $780 \mathrm{~N} / \mathrm{mm}^{2}$ | $750 \mathrm{~N} / \mathrm{mm}^{2}$ |
| Min. Elongation | $9 \%$ | $9 \%$ |

## Notes:

1. Screws with lengths equal to or shorter than listed in column 'L' are threaded to head.
2. Property Class : 12.9
3. Thread Class: 4g6g
4. Working Temperature : $-50^{\circ} \mathrm{C}$ to $+300^{\circ} \mathrm{C}$
5. Torques calculated in accordance with VDI 2230 "Systematic calculation of high duty bolted joints" with $\sigma 0.2=1080 \mathrm{~N} / \mathrm{mm}^{2}$ and $\mu=0.125$ for plain finish and $\mu=0.094$ for plated.

Head Marking



Product Dimensions (Standard Sizes)

| Thread | Pitch | Head Diameter A max | Hex <br> Socket Size W nom. | Head <br> Height H max | Socket <br> Depth F min. | Transition Dia da max | Length <br> Note 1 | Thread Length T ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |
| Size |  |  |  |  |  |  |  |  |
| nom. |  |  |  |  |  |  |  |  |
| M3 | 0.50 | 5.5 | 2.5 | 3.0 | 1.3 | 3.60 | 20 | 18 |
| M4 | 0.70 | 7.0 | 3.0 | 4.0 | 2.0 | 4.70 | 25 | 20 |
| M5 | 0.80 | 8.5 | 4.0 | 5.0 | 2.5 | 5.70 | 25 | 22 |
| M6 | 1.00 | 10.0 | 5.0 | 6.0 | 3.0 | 6.80 | 30 | 24 |
| M8 | 1.25 | 13.0 | 6.0 | 8.0 | 4.0 | 9.20 | 35 | 28 |
| M10 | 1.50 | 16.0 | 8.0 | 10.0 | 5.0 | 11.20 | 40 | 32 |
| M12 | 1.75 | 18.0 | 10.0 | 12.0 | 6.0 | 13.70 | 50 | 36 |
| (M14) | 2.00 | 21.0 | 12.0 | 14.0 | 7.0 | 15.70 | 55 | 40 |
| M16 | 2.00 | 24.0 | 14.0 | 16.0 | 8.0 | 17.70 | 60 | 44 |
| (M18) | 2.50 | 27.0 | 14.0 | 18.0 | 9.0 | 20.20 | 65 | 48 |
| M20 | 2.50 | 30.0 | 17.0 | 20.0 | 10.0 | 22.40 | 70 | 52 |
| (M22) | 2.50 | 33.0 | 17.0 | 22.0 | 11.0 | 24.40 | 70 | 56 |
| M24 | 3.00 | 36.0 | 19.0 | 24.0 | 12.0 | 26.40 | 80 | 60 |
| M27 | 3.00 | 40.0 | 19.0 | 27.0 | 13.5 | 30.40 | 90 | 66 |
| M30 | 3.50 | 45.0 | 22.0 | 30.0 | 15.5 | 33.40 | 100 | 72 |
| M33 | 3.50 | 50.0 | 24.0 | 33.0 | 18.0 | 36.40 | 100 | 78 |
| M36 | 4.00 | 54.0 | 27.0 | 36.0 | 19.0 | 39.40 | 110 | 84 |
| M42 | 4.50 | 63.0 | 32.0 | 42.0 | 24.0 | 45.60 | 130 | 96 |


| Thread Size nom. | Recommended Torques Setting |  |  |  | Induced Load |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Unplated |  | Plated |  |  |  |
|  | N-m | in-lbs. | N -m | in-lbs. | kN | lbf |
| M3 | 2.1 | 18.6 | 1.6 | 14.2 | 3.99 | 890 |
| M4 | 4.6 | 40.7 | 3.5 | 31.0 | 6.75 | 1,510 |
| M5 | 9.5 | 84.1 | 7.1 | 62.8 | 11.10 | 2,480 |
| M6 | 16.0 | 142.0 | 12.0 | 106.0 | 15.60 | 3,480 |
| M8 | 39.0 | 345.0 | 29.0 | 257.0 | 28.70 | 6,400 |
| M10 | 77.0 | 682.0 | 58.0 | 513.0 | 45.70 | 10,200 |
| M12 | 135.0 | 1,200.0 | 101.0 | 894.0 | 66.70 | 14,900 |
| (M14) | 215.0 | 1,900.0 | 161.0 | 1,420.0 | 91.30 | 20,400 |
| M16 | 330.0 | 2,920.0 | 248.0 | 2,190.0 | 126.00 | 28,100 |
| (M18) | 455.0 | 4,030.0 | 341.0 | 3,020.0 | 153.00 | 34,100 |
| M20 | 650.0 | 5,750.0 | 488.0 | 4,320.0 | 197.00 | 44,000 |
| (M22) | 870.0 | 7,700.0 | 652.0 | 5,770.0 | 245.00 | 54,700 |
| M24 | 1,100.0 | 9,740.0 | 825.0 | 7,300.0 | 284.00 | 63,400 |
| M27 | 1,650.0 | 14,600.0 | 1,238.0 | 11,000.0 | 374.00 | 83,400 |
| M30 | 2,250.0 | 19,900.0 | 1,688.0 | 15,000.0 | 454.00 | 101,000 |
| M33 | 3,050.0 | 27,000.0 | 2,287.0 | 20,200.0 | 550.00 | 123,000 |
| M36 | 3,850.0 | 34,100.0 | 2,888.0 | 25,000.0 | 664.00 | 148,000 |
| M42 | 6,270.0 | 55,500.0 | 4,700.0 | 41,600.0 | 889.00 | 198,000 |

Sizes in brackets are non-preferred standards

## Body and Grip Length Dimensions

- LG is the maximum grip length and is the distance from the bearing surface to the first complete thread.
- LB is the minimum body length and is the length of the unthreaded cylindrical portion of the shank.
- Dimensions for LB and LG are calculated from the following formula:

TRef $=(2 x$ Nominal Dia) plus 12 mm .
LG max = Nominal length "L" minus " $T$ "
LB min = Nominal length "L" minus ( $T+5$ pitches)



| Length | M18 |  | M20 |  | M22 |  | M24 |  | M27 |  | M30 |  | M33 |  | M36 |  | M42 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nom. | $\begin{gathered} L_{B} \\ (\text { Min. }) \end{gathered}$ | $\begin{gathered} L_{G} \\ (\text { Max. }) \end{gathered}$ | $\begin{gathered} L_{B} \\ \text { (Min.) } \end{gathered}$ | $L_{G}$ <br> (Мах.) | $\begin{gathered} L_{B} \\ \text { (Min.)(! } \end{gathered}$ | $\begin{gathered} L_{G} \\ (\text { Max. }) \end{gathered}$ | $\begin{gathered} L_{B} \\ (\text { Min. }) \end{gathered}$ | $\begin{gathered} L_{G} \\ (\text { Max. }) \end{gathered}$ | $\begin{gathered} L_{B} \\ \text { (Min.) } \end{gathered}$ | $\begin{gathered} L_{G} \\ \text { (Max.) } \end{gathered}$ | $\begin{gathered} L_{B} \\ \text { (Min.) } \end{gathered}$ | $\begin{gathered} L_{G} \\ \text { (Max.) } \end{gathered}$ | $\begin{gathered} L_{B} \\ \text { (Min.) } \end{gathered}$ | $\begin{gathered} L_{G} \\ (\text { Max. }) \end{gathered}$ | $\begin{gathered} L_{B} \\ (\text { Min. }) \end{gathered}$ | $\begin{gathered} L_{G} \\ (\text { Max. }) \end{gathered}$ | $\begin{gathered} L_{B} \\ \text { (Min.) } \end{gathered}$ | $\begin{gathered} L_{G} \\ (\text { Max. }) \end{gathered}$ |
| 70 | 9.5 | 22 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 80 | 19.5 | 32 | 15.5 | 28 | 11.5 | 24 |  |  |  |  |  |  |  |  |  |  |  |  |
| 90 | 29.5 | 42 | 25.5 | 38 | 21.5 | 34 | 15 | 30 |  |  |  |  |  |  |  |  |  |  |
| 100 | 39.5 | 52 | 35.5 | 48 | 31.5 | 44 | 25 | 40 | 19 | 34 |  |  |  |  |  |  |  |  |
| 110 | 49.5 | 62 | 45.5 | 58 | 41.5 | 54 | 35 | 50 | 29 | 44 | 20.5 | 38 | 14.5 | 32 |  |  |  |  |
| 120 | 59.5 | 72 | 55.5 | 68 | 51.5 | 64 | 45 | 60 | 39 | 54 | 30.5 | 48 | 24.5 | 42 | 16 | 36 |  |  |
| 130 | 69.5 | 82 | 65.5 | 78 | 61.5 | 74 | 55 | 70 | 49 | 64 | 40.5 | 58 | 34.5 | 52 | 26 | 46 |  |  |
| 140 | 79.5 | 92 | 75.5 | 88 | 71.5 | 84 | 65 | 80 | 59 | 74 | 50.5 | 68 | 44.5 | 62 | 36 | 56 | 21.5 | 44 |
| 150 | 89.5 | 102 | 85.5 | 98 | 81.5 | 94 | 75 | 90 | 69 | 84 | 60.5 | 78 | 54.5 | 72 | 46 | 66 | 31.5 | 54 |
| 160 | 99.5 | 112 | 95.5 | 108 | 91.5 | 104 | 85 | 100 | 79 | 94 | 70.5 | 88 | 64.5 | 82 | 56 | 76 | 41.5 | 64 |
| 180 | 119.5 | 132 | 115.5 | 128 | 111.5 | 124 | 105 | 120 | 99 | 114 | 90.5 | 108 | 84.5 | 102 | 76 | 96 | 61.5 | 84 |
| 200 |  |  | 135.5 | 148 | 131.5 | 144 | 125 | 140 | 119 | 134 | 110.5 | 128 | 104.5 | 122 | 96 | 116 | 81.5 | 104 |
| 220 |  |  |  |  | 151.5 | 164 | 145 | 160 | 139 | 154 | 130.5 | 148 | 124.5 | 142 | 116 | 136 | 101.5 | 124 |
| 240 |  |  |  |  |  |  | 165 | 180 | 159 | 174 | 150.5 | 168 | 144.5 | 162 | 136 | 156 | 121.5 | 144 |
| 260 |  |  |  |  |  |  |  |  | 179 | 194 | 170.5 | 188 | 164.5 | 182 | 156 | 176 | 141.5 | 164 |
| 280 |  |  |  |  |  |  |  |  |  |  | 190.5 | 208 | 184.5 | 202 | 176 | 196 | 161.5 | 184 |

All dimensions are in mm.

| Size | Part No. | Ibs. <br> $/ 1000$ |
| :--- | :--- | :--- | :---: |

M1.6 (0.35) - Key Size 1.5 mm

| Size | Part No. | Ibs. |
| :---: | :---: | :---: | :---: |
|  |  |  |

M4 (0.7) - Key Size 3mm

| $\mathrm{M} 1.6 \times 4$ | 104138 | 200 | 0.22 |
| ---: | ---: | ---: | ---: | | $\mathrm{M} 4 \times 45$ | 103022 | 200 | 10.49 |  |
| ---: | ---: | ---: | ---: | ---: |
| 6 | 104150 | 200 | 0.28 | 50 |
| 103023 | 200 | 11.53 |  |  |


| M5 (0.8)-Key Size 4mm |  |  |  |
| ---: | ---: | ---: | ---: |
| M5 × 10 | 122243 | 200 | 6.69 |
| 12 | 121094 | 200 | 7.22 |
| 14 | 400513 | 200 | 7.74 |
| 15 | 400510 | 200 | 8.03 |
| 16 | 103024 | 200 | 8.29 |
| 18 | 400522 | 200 | 8.82 |
| 20 | 113970 | 200 | 9.35 |
| 22 | 400523 | 200 | 9.88 |
| 25 | 121096 | 200 | 10.67 |
| 30 | 103029 | 200 | 12.32 |
| 35 | 115292 | 200 | 13.95 |
| 40 | 103030 | 200 | 15.58 |
| 45 | 103031 | 200 | 17.20 |
| 50 | 103035 | 200 | 18.83 |
| 55 | 103038 | 200 | 20.48 |
| 60 | 103040 | 200 | 22.11 |
| 65 | 106225 | 200 | 23.74 |
| 70 | 106228 | 200 | 25.37 |


| M8 (1.25) - Key Size 6 mm |  |  |  |
| ---: | ---: | ---: | ---: |
| $\mathrm{M} 8 \times 10$ | 103056 | 200 | 22.31 |
| 12 | 114972 | 200 | 23.61 |
| 14 | 400524 | 200 | 24.99 |
| 15 | 400514 | 200 | 25.74 |
| 16 | 103058 | 200 | 26.42 |
| 18 | 400569 | 200 | 27.81 |
| 20 | 122086 | 200 | 29.19 |
| 22 | 120642 | 200 | 30.49 |
| 25 | 119351 | 200 | 32.63 |
| 30 | 119383 | 200 | 36.08 |
| 35 | 122113 | 200 | 39.51 |
| 40 | 113143 | 200 | 43.65 |
| 45 | 121076 | 200 | 48.55 |
| 50 | 121068 | 100 | 52.07 |
| 55 | 103063 | 100 | 56.30 |
| 60 | 121070 | 100 | 60.50 |
| 65 | 103064 | 100 | 65.45 |
| 70 | 103066 | 100 | 69.67 |
| 75 | 103069 | 100 | 73.90 |
| 80 | 103070 | 100 | 78.12 |
| 90 | 103073 | 100 | 86.55 |
| 100 | 103075 | 100 | 94.60 |
| 110 | 103076 | 100 | 103.44 |
| 120 | 103077 | 100 | 111.89 |
| 130 | 106230 | 100 | 120.34 |
| 140 | 106231 | 100 | 127.95 |
| 150 | 106232 | 100 | 143.00 |
| 160 | 106233 | 50 | 144.83 |
| 180 | 106234 | 50 | 162.56 |
| 200 | 106235 | 50 | 179.43 |
|  |  |  |  |
|  |  |  |  |
| 10 |  |  |  |


| M10 (1.5)-Key Size 8mm |  |  |  |
| ---: | ---: | ---: | ---: |
| M10 x 10 | 106236 | 200 | 39.34 |
| 12 | 106237 | 200 | 41.65 |
| 15 | 400525 | 200 | 44.75 |
| 16 | 103080 | 200 | 45.83 |
| 18 | 400526 | 200 | 48.00 |
| 20 | 113163 | 200 | 50.16 |
| 25 | 115060 | 200 | 55.57 |
| 30 | 122114 | 200 | 61.23 |
| 35 | 113257 | 200 | 86.37 |
| 40 | 100845 | 100 | 72.09 |
| 45 | 121088 | 100 | 78.45 |
| 50 | 125660 | 100 | 85.07 |

Sizes above the bold line are threaded to head.

| Size | Part No. | lbs. <br> $/ 1000$ |  |
| ---: | ---: | ---: | ---: |
| M10 (1.5)-Key Size 8 mm |  |  |  |
| M10 55 | 103087 | 100 | 93.02 |
| 60 | 122217 | 100 | 98.32 |
| 65 | 103088 | 100 | 104.94 |
| 70 | 125786 | 100 | 112.90 |
| 75 | 103090 | 100 | 119.55 |
| 80 | 103091 | 100 | 126.17 |
| 90 | 103094 | 50 | 126.48 |
| 100 | 103095 | 50 | 137.35 |
| 110 | 103096 | 50 | 164.56 |
| 120 | 103097 | 50 | 179.26 |
| 130 | 106240 | 50 | 192.52 |
| 140 | 106241 | 50 | 212.08 |
| 150 | 106242 | 50 | 225.94 |
| 160 | 106243 | 50 | 239.80 |
| 180 | 106244 | 50 | 258.85 |
| 200 | 106245 | 50 | 285.38 |
| 220 | 400517 | 25 | 311.92 |


| Size | Part No. | $\theta$ | $\begin{aligned} & \text { lbs. } \\ & \text { /1000 } \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| M14 (2) - Key Size 12mm |  |  |  |
| M14 $\times 35$ | 400530 | 50 | 140.36 |
| 40 | 400531 | 50 | 151.14 |
| 45 | 400532 | 50 | 161.90 |
| 50 | 120863 | 50 | 172.68 |
| 55 | 400533 | 50 | 183.46 |
| 60 | 112000 | 50 | 196.48 |
| 65 | 400534 | 50 | 209.48 |
| 70 | 400535 | 50 | 227.46 |
| 75 | 400536 | 50 | 235.53 |
| 80 | 400537 | 50 | 248.56 |
| 90 | 400538 | 50 | 274.58 |
| 100 | 400539 | 50 | 300.63 |
| 110 | 400540 | 50 | 326.66 |
| 120 | 400508 | 50 | 352.10 |
| M16 (2) - Key Size 14mm |  |  |  |
| M16 25 | 106248 | 25 | 169.7 |
| 30 | 103112 | 25 | 184.1 |
| 35 | 103113 | 25 | 199.1 |
| 40 | 125751 | 25 | 213.6 |
| 45 | 103115 | 25 | 228.1 |
| 50 | 112474 | 25 | 242.0 |
| 55 | 103117 | 25 | 256.5 |
| 60 | 112594 | 25 | 271.0 |
| 65 | 103118 | 25 | 288.0 |
| 70 | 103119 | 25 | 305.0 |
| 75 | 103120 | 25 | 322.1 |
| 80 | 125658 | 25 | 339.2 |
| 90 | 103122 | 25 | 371.8 |
| 100 | 103123 | 25 | 407.3 |
| 110 | 103124 | 25 | 441.4 |
| 120 | 103126 | 25 | 475.5 |
| 130 | 103127 | 25 | 509.6 |
| 140 | 103128 | 25 | 541.2 |
| 150 | 103129 | 25 | 577.8 |
| 160 | 103364 | 25 | 609.4 |
| 180 | 107460 | 25 | 679.1 |
| 200 | 107448 | 25 | 748.2 |
| 300 | 400578 | 5 | 1096.5 |


| Size | Part No. | lbs. <br> $/ 1000$ |
| :--- | :--- | :---: | :---: |

M18 (2.5) - Key Size 14 mm

| M18 $\times 90$ | 400550 | 25 | 486.6 |
| ---: | ---: | ---: | ---: |
| 100 | 400551 | 25 | 532.2 |
| 120 | 400552 | 25 | 618.6 |

## M20 (2.5) - Key Size 17 mm

| M20 $\times 30$ | 107465 | 25 | 329.4 |
| ---: | ---: | ---: | ---: |
| 35 | 107466 | 25 | 352.1 |
| 40 | 103130 | 25 | 374.7 |


| 45 | 103131 | 25 | 397.3 |
| ---: | ---: | ---: | ---: |
| 50 | 103132 | 25 | 420.0 |
| 55 | 103136 | 25 | 442.7 |


| 60 | 103137 | 25 | 465.3 |
| ---: | ---: | ---: | ---: |
| 65 | 103138 | 25 | 487.9 |
| 70 | 103141 | 25 | 510.6 |
| 75 | 103142 | 25 | 537.3 |

- 

| 75 | 103142 | 25 | 537.3 |
| :--- | :--- | :--- | :--- |
| 80 | 103143 | 25 | 563.9 |
| 90 | 103144 | 25 | 617.2 |


| 100 | 103145 | 25 | 670.5 |
| :--- | :--- | :--- | :--- |
| 110 | 103146 | 25 | 723.8 |


| 120 | 103148 | 25 | 777.1 |
| :--- | :--- | :--- | :--- |
| 130 | 103150 | 10 | 826.8 |


| 140 | 103151 | 10 | 880.0 |
| ---: | ---: | ---: | ---: |
| 150 | 103152 | 10 | 934.3 |
| 160 | 107462 | 10 | 990.2 |
| 180 | 107463 | 10 | 1096.8 |
| 200 | 107464 | 5 | 1203.3 |
| 220 | 400553 | 5 | 1321.5 |
| 240 | 400554 | 5 | 1428.2 |
| 260 | 400555 | 5 | 1534.9 |
| 280 | 400556 | 5 | 1641.9 |
| 300 | 400557 | 5 | 1748.4 |
| 340 | 796973 | 5 | 1960.30 |


| M22 (2.5) - Key Size 17mm |  |  |  |
| ---: | ---: | ---: | ---: |
| M22 $\times 80$ | 180186 | 10 | 739.2 |
| 90 | 180187 | 10 | 805.2 |
| 100 | 180188 | 10 | 871.2 |
| 110 | 180189 | 10 | 937.2 |
| 140 | 180192 | 10 | 1135.2 |


| M18 (2.5) - Key Size 14 mm |  |  |  |
| ---: | ---: | ---: | ---: |
| M18 $\times 35$ | 400541 | 25 | 272.8 |
| 40 | 400542 | 25 | 290.8 |
| 45 | 400606 | 25 | 308.8 |
| 50 | 100844 | 25 | 326.0 |
| 60 | 400544 | 25 | 362.9 |
| 65 | 400545 | 25 | 380.9 |
| 70 | 400546 | 25 | 402.6 |
| 80 | 400549 | 25 | 445.7 |


| M24 (3) - Key Size 19mm |  |  |  |
| ---: | :---: | :---: | :---: |
| M24 x 40 | 106249 | 10 | 594.0 |
| 45 | 103153 | 10 | 627.0 |
| 50 | 103155 | 10 | 672.7 |
| 55 | 103157 | 10 | 705.7 |
| 60 | 103158 | 10 | 738.1 |
| 65 | 103159 | 10 | 770.7 |
| 70 | 103160 | 10 | 801.8 |
| 75 | 103161 | 10 | 836.0 |
| 80 | 103162 | 10 | 868.7 |

Sizes above the bold line are threaded to head. Property Class: 12.9

| Size | Part No. | lbs. |
| ---: | :---: | :---: | :---: |
| M24 (3) - Key Size 19mm |  |  |
| 1000 |  |  |


| M30 (3.5) - Key Size 22mm |  |  |  |
| :---: | :---: | :---: | :---: |
| M $30 \times 70$ | 116464 | 1 | 1419.8 |
| 80 | 140610 | 1 | 1518.0 |
| 90 | 140611 | 1 | 1621.7 |
| 100 | 140612 | 1 | 1724.0 |
| 110 | 140613 | 1 | 1881.0 |
| 120 | 140614 | 1 | 2004.7 |
| 130 | 140615 | 1 | 2125.5 |
| 140 | 140616 | 1 | 2244.0 |
| 150 | 140617 | 1 | 2366.0 |
| 160 | 140618 | 1 | 2486.0 |
| 180 | 140620 | 1 | 2728.0 |
| 200 | 140621 | 1 | 2970.0 |
| 280 | 140625 | 1 | 3936.5 |
| 300 | 400626 | 1 | 4177.9 |
| 320 | 180848 | 1 | 4419.8 |
| M36 (4) - Key Size 27mm |  |  |  |
| M36 x 80 | 140629 | 1 | 2388.9 |
| 90 | 140630 | 1 | 2530.0 |
| 100 | 140631 | 1 | 2681.1 |
| 120 | 140633 | 1 | 3055.0 |
| 130 | 400634 | 1 | 3229.5 |
| 140 | 140635 | 1 | 3351.3 |
| 150 | 140636 | 1 | 3577.3 |
| 160 | 140637 | 1 | 3751.3 |
| 180 | 140639 | 1 | 4098.9 |
| 200 | 140640 | 1 | 4466.0 |
| 220 | 180294 | 1 | 4794.5 |
| 240 | 140641 | 1 | 5142.3 |
| 260 | 140642 | 1 | 5490.1 |
| 280 | 180411 | 1 | 5837.9 |
| 300 | 140643 | 1 | 6185.6 |
| 320 | 180490 | 1 | 6533.4 |

## Deal with CORBOSTON The Intelligent way!

## Check out a host of coatings available from Unbrako:

- Zinc Electroplating
- Mechanical Galvanizing
- Hot Dip Galvanizing
- Zinc-Al Flake
- Unbrako Wiscoat
- PTFE


Suitable for all high tensile applications. Up to 190,000 psi highest of any socket cap screw. Use Stainless for corrosive, cryogenic or elevated temperature environments.

Equivalent Standards
ASME B18.3

## Mechanical Properties

| Screw Size | $\geq 1 / 2$ | $<1 / 2$ |
| :--- | :---: | :---: |
| Heat Treatment | $39-43 \mathrm{RC}$ | $39-43 \mathrm{RC}$ |
| Tensile Strength | 190 ksi | 180 ksi |
| Yield Strength | 170 ksi | 162 ksi |
| Shear Strength | 114 ksi | 108 ksi |

Material: Unbrako High Grade Alloy Steel
Elongation is 2 inches - $10 \%$ min.
Reduction of area - 35\% min.
Length 'L' Tolerance (in)

|  | over | over |
| :---: | :---: | :---: |
| up to | $1^{\prime \prime}$ to | $21 / 2^{\prime \prime}$ |
| $1^{\prime \prime}$ | $21 / 2^{\prime \prime}$ | to |

Diameter incl. incl. $6^{\prime \prime}$ incl. over 6"

| \#0 thru 3/8 incl. | -.03 | -.04 | -.06 | -.12 |
| :--- | :--- | :--- | :--- | :--- |
| $7 / 16$ to $3 / 4$ incl. | -.03 | -.06 | -.08 | -.12 |
| $7 / 8$ to $1-1 / 2$ incl. | -.05 | -.10 | -.14 | -.20 |

over 1 1/2

## NOTES:

1. Thread Class: \#0 to $1^{\prime \prime}: 3 \mathrm{~A}$, over $1^{\prime \prime}: 2 \mathrm{~A}$
2. Working Temperature: $-50^{\circ} \mathrm{C}$ to $+300^{\circ} \mathrm{C}$
3. Torques calculated in accordance with VDI 2230 "Systematic calculation of high duty bolted joints" with $\sigma 0.2=155$ K.S.I. and $\mu=0.125$ for plain finish and $\mu=0.094$ for plated. Above $0.625^{\prime \prime}$ dia. $\sigma 0.2=140$ K.S.I.
4. The following diameters are fully interchangeable between 1936 and 1960 series:- No 10, 1/4", 3/8", 1/2" for both UNC and UNF

## Head Marking


' X ' represents Lot Traceability E-CODE

Suitable for all high tensile applications. Up to 190,000 psi highest of any socket cap screw. Use Stainless for corrosive, cryogenic or elevated temperature environments.

Equivalent Standards ASME B18.3

## Mechanical Properties

| Screw Size | $\geq 1 / 2$ | $<1 / 2$ |
| :--- | :--- | :---: |
| Heat Treatment | $39-43 \mathrm{RC}$ | $39-43 \mathrm{RC}$ |
| Tensile Strength | 190 ksi | 180 ksi |
| Yield Strength | 170 ksi | 162 ksi |
| Shear Strength | 114 ksi | 108 ksi |

Material: Unbrako High Grade Alloy Steel
Elongation is 2 inches - 10\% min.
Reduction of area - 35\% min.

## NOTES:

1. Thread Class: \#0 to 1"-3A, over 1"-2A
2. Working Temperature: $-50^{\circ} \mathrm{C}$ to $+300^{\circ} \mathrm{C}$
3. Torques calculated in accordance with VDI 2230 "Systematic calculation of high duty bolted joints" with $\sigma 0.2=155$ K.S.I. and $\mu=0.125$ for plain finish and $\mu=0.094$ for plated. Above $0.625^{\prime \prime}$ dia. $\sigma 0.2=140$ K.S.I.
4. The following diameters are fully interchangeable between 1936 and 1960 series:- No 10, 1/4", 3/8", $1 / 2$ " for both UNC and UNF

## Head Marking





| Size | Part No. | lbs. <br> $/ 1000$ |  |
| ---: | :---: | :---: | :---: |
| \#0-80 UNF - Key Size 0.05" |  |  |  |
| \#0 $\times 3 / 16$ | 117137 | 100 | 0.17 |
| $1 / 4$ | 117153 | 100 | 0.18 |
| $3 / 8$ | 121059 | 100 | 0.22 |
| $\# 1-72$ UNF - Key Size 1/16" |  |  |  |
|  |  |  |  |
| \#1 x 1/4 | 117202 | 100 | 0.36 |
| $3 / 8$ | 102704 | 100 | 0.45 |


| Size | Part No. | lbs. <br> $/ 1000$ |  |
| ---: | :---: | :---: | :---: |
| $\# 6-32$ UNC - Key |  |  | Size 7/64" |
| $\# 6 \times 3 / 8$ | 113440 | 100 | 2.42 |
| $1 / 2$ | 118792 | 100 | 2.86 |
| $5 / 8$ | 118808 | 100 | 3.30 |
| $3 / 4$ | 118824 | 100 | 3.61 |
| $7 / 8$ | 118840 | 100 | 4.00 |
| 1 | 118856 | 100 | 4.38 |
| $11 / 4$ | 112179 | 100 | 5.68 |
| $11 / 2$ | 114328 | 100 | 6.45 |

Size Part No. $\bigoplus \begin{gathered}\text { Ibs. } \\ / 1000\end{gathered}$

| $\# 10-24$ UNC - Key Size 5/32" |  |  |  |
| ---: | :---: | :---: | :---: |
| $\# 10 \times 13 / 4$ | 103248 | 100 | 14.96 |
| 2 | 103264 | 100 | 16.94 |
| $21 / 4$ | 108823 | 100 | 19.12 |
| $21 / 2$ | 106226 | 100 | 20.83 |
| $23 / 4$ | 103477 | 100 | 23.01 |
| 3 | 106355 | 100 | 24.46 |
| $31 / 2$ | 116278 | 100 | 28.38 |
| 4 | 116279 | 100 | 32.34 |


| \#2-56 UNC - Key Size 5/64" |  |  |  |
| ---: | ---: | ---: | ---: |
| \#2×3/16 | 105493 | 100 | 0.47 |
| $1 / 4$ | 105509 | 100 | 0.58 |
| $3 / 8$ | 113307 | 100 | 0.75 |
| $1 / 2$ | 113323 | 100 | 0.93 |
| $5 / 8$ | 700572 | 100 | 1.05 |
| $3 / 4$ | 700573 | 100 | 1.18 |
| 1 | 700574 | 100 | 1.44 |


| \#6-40 UNF - Key Size 7/64" |  |  |  |
| ---: | ---: | ---: | ---: |
| \#6 $\times 1 / 4$ | 102720 | 100 | 2.09 |
| $3 / 8$ | 111564 | 100 | 2.53 |
| $1 / 2$ | 111581 | 100 | 2.79 |
| $5 / 8$ | 111597 | 100 | 3.19 |
| $3 / 4$ | 114012 | 100 | 3.56 |
| 1 | 700842 | 100 | 4.22 |
| \#8-32 UNC - Key Size 9/64" |  |  |  |
| \#8 $\times 1 / 4$ | 118872 | 100 | 3.08 |
| $5 / 16$ | 117320 | 100 | 3.63 |
| $3 / 8$ | 118888 | 100 | 3.96 |
| $1 / 2$ | 118904 | 100 | 4.53 |
| $5 / 8$ | 118920 | 100 | 4.84 |
| $3 / 4$ | 118936 | 100 | 5.50 |
| $7 / 8$ | 103140 | 100 | 6.20 |
| 1 | 103156 | 100 | 6.69 |
| $11 / 4$ | 103174 | 100 | 8.12 |
| $11 / 2$ | 103190 | 100 | 9.66 |
| $13 / 4$ | 117451 | 100 | 11.18 |
| 2 | 117516 | 100 | 12.39 |
| $21 / 4$ | 120791 | 100 | 15.29 |


| \#10-32 UNF - Key Size 5/32" |  |  |  |
| ---: | :---: | :---: | ---: |
| $\# 10 \times 1 / 4$ | 111756 | 100 | 4.80 |
| $5 / 16$ | 116280 | 100 | 5.30 |
| $3 / 8$ | 117733 | 100 | 5.50 |
| $1 / 2$ | 117749 | 100 | 6.25 |
| $5 / 8$ | 117765 | 100 | 7.00 |
| $3 / 4$ | 117781 | 100 | 7.70 |
| $7 / 8$ | 117798 | 100 | 8.45 |
| 1 | 117814 | 100 | 9.20 |
| $11 / 4$ | 117830 | 100 | 11.79 |
| $11 / 2$ | 117847 | 100 | 13.07 |
| $13 / 4$ | 117863 | 100 | 14.96 |
| 2 | 117879 | 100 | 16.94 |
| $21 / 4$ | 107085 | 100 | 19.54 |
| $21 / 2$ | 107150 | 100 | 21.12 |
| 3 | 107182 | 100 | 25.01 |


| $1 / 4-20$ UNC - Key Size $3 / 16^{\prime \prime}$ |  |  |  |
| ---: | ---: | ---: | ---: |
| $1 / 4 \times 1 / 4$ | 120048 | 100 | 9.00 |
| $3 / 8$ | 105232 | 100 | 10.30 |
| $1 / 2$ | 105248 | 100 | 11.59 |
| $5 / 8$ | 108937 | 100 | 12.89 |
| $3 / 4$ | 108954 | 100 | 14.19 |
| $7 / 8$ | 108969 | 100 | 15.49 |
| 1 | 105256 | 100 | 16.72 |
| $11 / 4$ | 105272 | 100 | 19.36 |
| $13 / 8$ | 117409 | 100 | 20.72 |
| $11 / 2$ | 105288 | 100 | 22.77 |
| $13 / 4$ | 105304 | 100 | 26.16 |
| 2 | 105320 | 100 | 29.48 |
| $21 / 4$ | 105336 | 100 | 32.91 |
| $21 / 2$ | 118338 | 100 | 36.30 |
| $23 / 4$ | 118355 | 100 | 39.67 |
| 3 | 118371 | 100 | 43.05 |
| $31 / 4$ | 117539 | 100 | 46.46 |
| $31 / 2$ | 117573 | 100 | 49.81 |
| $33 / 4$ | 117605 | 100 | 53.20 |
| 4 | 109434 | 100 | 57.35 |
| $41 / 2$ | 109499 | 100 | 64.11 |
| 5 | 114978 | 100 | 70.86 |


| Size | Part No. | 5 | $\begin{aligned} & \text { lbs. } \\ & \text { /1000 } \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| 1/4-20 UNC - Key Size 3/16" |  |  |  |
| $1 / 4 \times 51 / 2$ | 105637 | 100 | 77.64 |
| 6 | 115042 | 100 | 84.39 |
| 1/4-28 UNF - Key Size 3/16" |  |  |  |
| $1 / 4 \times 1 / 4$ | 114545 | 100 | 9.00 |
| 3/8 | 117896 | 100 | 10.30 |
| 1/2 | 117913 | 100 | 11.59 |
| 5/8 | 111454 | 100 | 12.89 |
| 3/4 | 111471 | 100 | 14.19 |
| 7/8 | 111487 | 100 | 15.49 |
| 1 | 111503 | 100 | 16.72 |
| $11 / 4$ | 111519 | 100 | 19.36 |
| $11 / 2$ | 111535 | 100 | 22.77 |
| $13 / 4$ | 108026 | 100 | 26.16 |
| 2 | 108042 | 100 | 29.48 |
| $21 / 4$ | 108057 | 100 | 32.91 |
| $21 / 2$ | 118427 | 100 | 36.30 |
| $23 / 4$ | 118460 | 100 | 40.70 |
| 3 | 118476 | 100 | 43.05 |
| $31 / 2$ | 116281 | 100 | 51.44 |
| 4 | 116283 | 100 | 58.19 |


| $5 / 16-18$ UNC - Key Size $1 / 4^{\prime \prime}$ |  |  |  |
| ---: | ---: | ---: | ---: |
| $5 / 16 \times 3 / 8$ | 118387 | 100 | 18.79 |
| $1 / 2$ | 118403 | 100 | 20.68 |
| $5 / 8$ | 118419 | 100 | 22.88 |
| $3 / 4$ | 118436 | 100 | 25.30 |
| $7 / 8$ | 104055 | 100 | 27.24 |
| 1 | 104071 | 100 | 29.70 |
| $11 / 4$ | 104088 | 100 | 33.99 |
| $11 / 2$ | 104104 | 100 | 38.50 |
| $13 / 4$ | 104121 | 100 | 45.01 |
| 2 | 104137 | 100 | 48.84 |
| $21 / 4$ | 104153 | 100 | 55.86 |
| $21 / 2$ | 109900 | 100 | 59.62 |
| $23 / 4$ | 109916 | 100 | 66.73 |
| 3 | 109932 | 100 | 70.40 |
| $31 / 4$ | 109950 | 50 | 74.71 |
| $31 / 2$ | 109966 | 50 | 81.80 |
| 4 | 109833 | 100 | 92.64 |
| $41 / 2$ | 109866 | 100 | 100.85 |
| 5 | 103652 | 100 | 110.68 |
| $51 / 2$ | 121215 | 100 | 125.20 |
| 6 | 103684 | 100 | 136.07 |


| $5 / 16-24$ UNF-Key Size $5 / 32^{\prime \prime}$ |  |  |  |  |  |  |  |  |  | 20.90 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | :---: | :---: | :---: |
|  | 100 | $7 / 8$ | 110917 | 100 | 42.46 |  |  |  |  |  |
| $5 / 16 \times 1 / 2$ | 108073 | 1 | 110934 | 100 | 47.52 |  |  |  |  |  |
| $5 / 8$ | 104516 | 100 | 22.04 |  |  |  |  |  |  |  |
| $3 / 4$ | 104532 | 100 | 24.29 | $11 / 4$ | 110950 | 100 | 51.68 |  |  |  |


| Size | Part No. | lbs. <br> $/ 1000$ |  |
| ---: | :---: | :---: | :---: |
| $5 / 16-24$ UNF - Key Size $1 / 4^{\prime \prime}$ |  |  |  |
| $5 / 16 \times 7 / 8$ | 104548 | 100 |  |
| 1 | 110752 | 100 |  |
| $11 / 4$ | 110769 | 100 |  |
| $11 / 2$ | 110786 | 100 |  |
| $13 / 4$ | 110802 | 100 |  |
| 2 | 110818 | 100 |  |
| $21 / 4$ | 110834 | 100 |  |
| $21 / 2$ | 110850 | 100 |  |
| $23 / 4$ | 105606 | 100 |  |
| 3 | 105344 | 100 |  |
| $31 / 2$ | 106016 | 100 |  |
| 4 | 120995 | 100 |  |

Size Part No. $\wp$| Ibs. |
| :---: |
| $/ 1000$ |

| $3 / 8-24$ UNF - Key Size 5/16" |  |  |  |
| ---: | ---: | ---: | ---: |
| $3 / 8 \times 13 / 4$ | 116440 | 50 | 65.49 |
| 2 | 116456 | 50 | 73.04 |
| $21 / 4$ | 116472 | 50 | 80.81 |
| $21 / 2$ | 116488 | 50 | 88.44 |
| $23 / 4$ | 112246 | 50 | 100.10 |
| 3 | 116504 | 50 | 106.74 |
| $31 / 4$ | 400467 | 50 | 111.41 |
| $31 / 2$ | 112278 | 50 | 119.06 |
| 4 | 119090 | 50 | 137.37 |
| $41 / 2$ | 108318 | 50 | 152.68 |

7/16-14 UNC - Key Size 3/8"

| $7 / 16 \times 3 / 4$ | 107385 | 100 | 58.19 |
| ---: | ---: | ---: | ---: |
| $7 / 8$ | 107417 | 100 | 61.01 |
| 1 | 107449 | 100 | 66.59 |
| $11 / 4$ | 118520 | 50 | 75.02 |
| $11 / 2$ | 118554 | 50 | 81.84 |
| $13 / 4$ | 118586 | 50 | 91.89 |
| 2 | 118619 | 50 | 105.34 |
| $21 / 4$ | 116299 | 50 | 113.78 |
| $21 / 2$ | 116332 | 50 | 126.21 |
| $23 / 4$ | 116364 | 25 | 134.66 |
| 3 | 116396 | 25 | 147.09 |
| $31 / 2$ | 110568 | 25 | 167.97 |
| 4 | 115611 | 25 | 188.85 |
| $41 / 2$ | 104743 | 25 | 209.73 |
| 5 | 110554 | 25 | 230.58 |
|  |  |  |  |

7/16-20 UNF - Key Size 3/8"

| $7 / 16 \times 1$ | 116520 | 100 | 69.15 |
| ---: | ---: | ---: | ---: |
| $11 / 4$ | 104561 | 50 | 78.23 |
| $11 / 2$ | 104577 | 50 | 87.32 |
| 2 | 104593 | 50 | 108.86 |
| $21 / 2$ | 105615 | 50 | 130.39 |
| 3 | 122789 | 25 | 150.61 |
| $31 / 2$ | 116284 | 25 | 171.47 |

1/2-13 UNC - Key Size 3/8"

| $1 / 2 \times 1 / 2$ | 115644 | 50 | 74.36 |
| ---: | ---: | ---: | ---: |
| $5 / 8$ | 115677 | 50 | 79.95 |
| $3 / 4$ | 102603 | 50 | 85.51 |
| $7 / 8$ | 102636 | 50 | 91.08 |
| 1 | 102670 | 50 | 96.69 |
| $11 / 4$ | 102703 | 50 | 107.80 |
| $11 / 2$ | 107950 | 50 | 118.80 |
| $13 / 4$ | 108016 | 50 | 130.17 |
| 2 | 102464 | 50 | 141.24 |
| $21 / 4$ | 110772 | 25 | 154.88 |
| $21 / 2$ | 110837 | 25 | 168.63 |


| Size | Part No. | 5 | $\begin{aligned} & \text { lbs. } \\ & \text { /1000 } \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| 1/2-13 UNC - Key Size 3/8" |  |  |  |
| 1/2 $\times 23 / 4$ | 110903 | 25 | 182.16 |
| 3 | 120761 | 25 | 195.91 |
| $31 / 4$ | 111303 | 25 | 212.08 |
| $31 / 2$ | 111575 | 25 | 223.23 |
| $33 / 4$ | 103111 | 25 | 241.87 |
| 4 | 111608 | 25 | 257.51 |
| $41 / 4$ | 107772 | 25 | 264.18 |
| $41 / 2$ | 111641 | 25 | 287.98 |
| 43/4 | 119162 | 25 | 293.99 |
| 5 | 111673 | 25 | 305.76 |
| $51 / 4$ | 107805 | 25 | 316.29 |
| $51 / 2$ | 115511 | 25 | 340.78 |
| $53 / 4$ | 107839 | 25 | 346.08 |
| 6 | 115544 | 25 | 371.36 |
| $61 / 4$ | 105005 | 10 | 375.98 |
| $61 / 2$ | 115576 | 10 | 393.73 |
| 7 | 109736 | 10 | 416.83 |
| $71 / 2$ | 107937 | 10 | 446.62 |
| 8 | 109768 | 10 | 468.95 |
| $81 / 2$ | 108003 | 10 | 501.16 |
| 9 | 102417 | 10 | 523.60 |
| 10 | 102451 | 10 | 578.16 |
| 11 | 108275 | 10 | 637.78 |
| 12 | 105569 | 10 | 692.34 |


| Size | Part No. | Ibs. <br> $/ 1000$ |
| :--- | :--- | :--- | :--- |


| Size | Part No. | Ibs. <br>  1000 |
| :--- | :--- | :--- | :---: |


| $5 / 8-11$ UNC - Key Size $1 / 2^{\prime \prime}$ |  |  |  |
| ---: | ---: | ---: | ---: |
| $5 / 8 \times 13 / 4$ | 116335 | 25 | 225.39 |
| 2 | 111036 | 25 | 241.30 |
| $21 / 4$ | 111069 | 25 | 255.82 |
| $21 / 2$ | 111101 | 25 | 287.76 |
| $23 / 4$ | 116639 | 25 | 305.49 |
| 3 | 116673 | 25 | 323.09 |
| $31 / 4$ | 116705 | 25 | 351.74 |
| $31 / 2$ | 116737 | 25 | 369.69 |
| 4 | 102196 | 25 | 408.58 |
| $41 / 2$ | 102047 | 25 | 451.64 |
| 5 | 120714 | 25 | 498.10 |
| $51 / 2$ | 120746 | 10 | 544.50 |
| 6 | 120778 | 10 | 580.14 |
| $61 / 2$ | 111320 | 10 | 626.56 |
| 7 | 111354 | 10 | 672.98 |
| $71 / 2$ | 122898 | 10 | 708.47 |
| 8 | 104175 | 10 | 755.04 |
| $81 / 2$ | 109197 | 10 | 801.46 |
| 9 | 118276 | 5 | 836.88 |
| 10 | 106599 | 5 | 922.46 |
| 11 | 107003 | 5 | 1015.52 |
| 12 | 115134 | 5 | 1110.12 |


| $3 / 4-10$ UNC - Key Size 5/8" |  |  |  |
| ---: | ---: | ---: | ---: |
| $3 / 4 \times 31 / 2$ | 111689 | 25 | 550.00 |
| $33 / 4$ | 111246 | 25 | 577.30 |
| 4 | 111722 | 25 | 623.02 |
| $41 / 2$ | 104539 | 25 | 674.78 |
| 5 | 110759 | 25 | 746.46 |
| $51 / 2$ | 110793 | 10 | 798.16 |
| 6 | 121562 | 10 | 869.66 |
| $61 / 2$ | 110858 | 10 | 921.58 |
| 7 | 110891 | 10 | 993.08 |
| 8 | 110924 | 10 | 1116.28 |
| $81 / 2$ | 103863 | 10 | 1168.20 |
| 9 | 107374 | 10 | 1239.92 |
| $91 / 2$ | 107438 | 10 | 1291.62 |
| 10 | 118545 | 10 | 1363.12 |
| 11 | 121572 | 10 | 1486.54 |
| 12 | 118610 | 10 | 1609.96 |
| 13 | 108283 | 10 | 1733.38 |


| $3 / 4-16$ UNF - Key Size $5 / 8^{\prime \prime}$ |  |  |  |
| ---: | ---: | ---: | ---: |
| $3 / 4 \times 1 \quad 1 / 4$ | 700952 | 25 | 298.54 |
| $11 / 2$ | 120615 | 25 | 324.50 |
| 2 | 120376 | 25 | 376.29 |
| $21 / 2$ | 138871 | 25 | 428.12 |
| 3 | 102344 | 25 | 499.64 |
| $31 / 2$ | 117976 | 25 | 551.41 |
| 4 | 118041 | 25 | 623.04 |
| $41 / 2$ | 114043 | 25 | 674.78 |
| 5 | 116293 | 25 | 746.46 |
| 6 | 700962 | 10 | 869.66 |


| $7 / 8-9$ UNC - Key Size $3 / 4^{\prime \prime}$ |  |  |  |
| ---: | :---: | :---: | ---: |
| $7 / 8 \times 2$ | 110957 | 10 | 559.37 |
| $21 / 4$ | 116447 | 10 | 594.88 |
| $21 / 2$ | 116479 | 10 | 630.52 |
| $23 / 4$ | 116511 | 10 | 665.94 |
| 3 | 104568 | 10 | 701.36 |
| $31 / 4$ | 104600 | 10 | 765.16 |
| $31 / 2$ | 104632 | 10 | 800.58 |
| 4 | 104665 | 10 | 899.80 |
| $41 / 2$ | 104697 | 10 | 968.00 |
| 5 | 104729 | 10 | 1041.79 |
| $51 / 2$ | 104761 | 10 | 1140.92 |
| 6 | 104793 | 10 | 1210.00 |
| $61 / 2$ | 110251 | 10 | 1311.20 |
| 7 | 115937 | 10 | 1382.26 |
| 8 | 115970 | 10 | 1552.32 |

# Socket Head Cap Screws - 1960 Series 

## (0) 튼

| Size | Part No. | lbs. <br> $/ 1000$ |  |
| :---: | :---: | :---: | :---: |
| $7 / 8-14$ UNF - Key Size $3 / 4^{\prime \prime}$ |  |  |  |
| $7 / 8 \times 2$ | $1 / 2$ | 106327 | 10 |
| 3 | $1 / 2$ | 105086 | 10 |


| $1-8$ UNC - Key Size 3/4" |  |  |  |
| ---: | :---: | :---: | ---: |
| $1 \times 11 / 2$ | 102584 | 10 | 698.72 |
| 2 | 116002 | 10 | 809.29 |
| $21 / 4$ | 116035 | 10 | 836.00 |
| $21 / 2$ | 115091 | 10 | 887.04 |
| $23 / 4$ | 115123 | 10 | 932.80 |
| 3 | 104702 | 10 | 887.13 |
| $31 / 4$ | 115189 | 10 | 1026.34 |
| $31 / 2$ | 114821 | 10 | 1113.66 |
| 4 | 114853 | 10 | 1160.52 |
| $41 / 2$ | 114888 | 10 | 1301.39 |
| 5 | 114920 | 10 | 1424.08 |
| $51 / 2$ | 103572 | 10 | 1520.82 |
| 6 | 103589 | 10 | 1646.35 |
| $61 / 2$ | 103606 | 10 | 1775.18 |
| 7 | 103623 | 10 | 1868.68 |
| $71 / 2$ | 100398 | 10 | 1997.27 |
| 8 | 122961 | 10 | 2090.88 |
| $81 / 2$ | 105063 | 10 | 2219.58 |
| 9 | 116867 | 10 | 2313.08 |
| $91 / 2$ | 121557 | 10 | 2441.78 |
| 10 | 116899 | 10 | 2535.50 |
| 11 | 102035 | 5 | 2757.70 |
| 12 | 104168 | 5 | 2979.90 |
| 14 | 121558 | 5 | 3424.52 |
| 2 |  |  |  |


| 1 1-12 UNF Key Size 3/4" |  |  |  |
| ---: | :---: | :---: | ---: |
| $1 \times 23 / 4$ | 117604 | 10 | 964.06 |
| $31 / 2$ | 109908 | 10 | 1108.21 |
| $51 / 2$ | 105362 | 10 | 1520.20 |
| 6 | 116289 | 10 | 1646.26 |
| 8 | 105350 | 10 | 2090.88 |

1 1/4-7 UNC - Key Size 7/8"

| $11 / 4 \times 21 / 2$ | 115451 | 1 | 1596.98 |
| ---: | ---: | ---: | ---: |
| 3 | 115468 | 1 | 1745.57 |
| $31 / 2$ | 121587 | 1 | 1893.98 |
| 4 | 104842 | 1 | 2086.48 |
| $41 / 2$ | 104857 | 1 | 2136.29 |
| 5 | 112918 | 1 | 2433.86 |
| $51 / 2$ | 104887 | 1 | 2596.00 |
| 6 | 110103 | 1 | 2781.13 |
| $61 / 2$ | 110118 | 1 | 2954.82 |
| 7 | 110136 | 1 | 3124.00 |
| 8 | 110152 | 1 | 3475.78 |
| 9 | 110168 | 1 | 3822.94 |

Size Part No. $\quad$| lbs. |
| :---: |
| $/ 1000$ |

| 1 |  |  |  |  | $1 / 4-7$ UNC - Key Size 7/8" |
| ---: | :---: | :---: | ---: | :---: | :---: |
| $11 / 4 \times 10$ | 110184 | 1 | 4170.32 |  |  |
| 12 | 110201 | 1 | 4864.86 |  |  |


| $11 / 4-12$ UNF - Key Size 7/8" |  |  |  |
| ---: | :---: | :---: | ---: |
| $11 / 4 \mathrm{X} 3$ | $1 / 2$ | 106603 | 1 | 1912.90


| 1 1/2-6 UNC - Key Size $1^{\prime \prime}$ |  |  |  |
| ---: | :---: | :---: | ---: |
| $11 / 2 \times 3$ | 110217 | 1 | 2772.66 |
| $31 / 2$ | 110234 | 1 | 2984.30 |
| 4 | 110250 | 1 | 3195.94 |
| $41 / 2$ | 115919 | 1 | 3407.58 |
| 5 | 115936 | 1 | 3715.36 |
| $51 / 2$ | 115953 | 1 | 3965.39 |
| 6 | 115969 | 1 | 4215.42 |
| $61 / 2$ | 115985 | 1 | 4465.34 |
| 7 | 116001 | 1 | 4323.00 |
| 8 | 116017 | 1 | 4816.02 |
| 9 | 116033 | 1 | 5715.60 |
| 10 | 116050 | 1 | 6215.88 |
| 12 | 116068 | 1 | 7215.78 |


| 1 1/2-12 UNF Key Size $1^{\prime \prime}$ |  |  |  |
| ---: | :---: | :---: | ---: |
| $11 / 2 \times 3$ | 103034 | 1 | 2772.66 |
| $31 / 2$ | 116143 | 1 | 2984.30 |
| 4 | 110258 | 1 | 3195.94 |
| $41 / 2$ | 110290 | 1 | 3407.58 |
| 5 | 110697 | 1 | 3715.36 |
| $51 / 2$ | 109136 | 1 | 3965.28 |
| 6 | 106106 | 1 | 4215.42 |
| 8 | 100447 | 1 | 4816.02 |
| 10 | 114786 | 1 | 6215.88 |

Note:

- Sizes above the bold line are threaded to head.
- The following diameters are fully interchangeable between 1936 and 1960 series:-
No 10, $1 / 4^{\prime \prime}, 3 / 8^{\prime \prime}, 1 / 2^{\prime \prime}$ both UNC and UNF


## SOCKET LOW HEAD CAP SCREWS

Low Head Socket Cap Screws are High Strength, precision fasteners designed for applications where head height clearance is a problem.

Low Head Socket Head Cap Screws cannot be pre-loaded as high as a standard socket head cap screw because of their reduced head height and smaller socket size.

Low Head Socket Head Cap Screws are manufactured from High Strength Alloy Steel and have a Black Oxide finish.

Smooth, burr-free sockets, uniformly concentric and usable to full depth for correct wrench engagement.

Highest standards of quality, material, manufacture and performance.


Hardness : 40-43 HRC
33-39 HRC

Tensile Strength : $1040 \mathrm{~N} / \mathrm{mm}^{2}$
Yield Strength : $940 \mathrm{~N} / \mathrm{mm}^{2}$


High Strength Fasteners for applications with limited clearance.


Suitable for use in parts too thin for standard Socket Head Cap Screw and for applications with limited clearance.

## Equivalent Standards

DIN $7984+6912$
(Except for Head \& Socket Dims)

## Mechanical Properties

Material: Unbrako High Grade Alloy Steel
Property Class: 10.9
Heat Treatment: Rc 33-39
Tensile Strength: $1040 \mathrm{~N} / \mathrm{mm}^{2}$
Yield Strength: $940 \mathrm{~N} / \mathrm{mm}^{2}$
Shear Strength: $624 \mathrm{~N} / \mathrm{mm}^{2}$
Min. Elongation: 9\%

## NOTES:

1. Body and Grip Lengths are same as metric Socket Head Cap Screws. (see page no.16)
2. Thread Class: 6 g
3. Working Temperature: $-50^{\circ} \mathrm{C}$ to $+300^{\circ} \mathrm{C}$
4. Sizes M5 and larger are stamped U 10.9. Torques calculated in accordance with VDI 2230 "Systematic calculation of high duty bolted joints" with $\sigma 0.2=900 \mathrm{~N} / \mathrm{mm} 2$ and $\mu=0.125$ for plain finish and $\mu=0.094$ for plated.

Length 'L' Tolerance (mm)

| Screws <br> Over | Up to and <br> including | Tolerance |
| :--- | :---: | :---: |
| - | 50 | $\pm 0.25$ |
| 50 | 80 | $\pm 0.50$ |
| 80 | 120 | $\pm 0.70$ |
| 120 | 250 | $\pm 0.80$ |
| 250 | - | $\pm 1.00$ |

## Head Marking



Head markings may vary slightly depending on manufacturing practice. UNBRAKO and UNB are recognized identifications for M5 diameter \& larger.


Product Dimensions


| Thread size nom. | Recommended Seating Torque |  |  |  | Induced Load |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Unplated |  | Plated |  |  |  |
|  | N-m | Ibf.In. | N-m | Ibf.ln. | kN | Ibf. |
| M4 | 3.8 | 33.6 | 2.9 | 25.7 | 5.65 | 1,270 |
| M5 | 8.0 | 70.8 | 6.0 | 53.1 | 9.20 | 2,068 |
| M6 | 13.0 | 115.0 | 9.8 | 86.7 | 13.00 | 2,920 |
| M8 | 32.0 | 283.0 | 24.0 | 212.0 | 23.90 | 5,370 |
| M10 | 64.0 | 566.0 | 48.0 | 425.0 | 38.00 | 8,540 |
| M12 | 110.0 | 974.0 | 83.0 | 735.0 | 55.50 | 12,470 |
| M16 | 275.0 | 2,434.0 | 206.0 | 1,820.0 | 105.00 | 23,600 |
| M20 | 550.0 | 4,870.0 | 405.0 | 3,585.0 | 164.00 | 36,800 |

as per Unbrako standard


Suitable for use in parts too thin for standard Socket Head Cap Screw and for applications with limited clearance.

Equivalent Standards

| ASME B18.3 |  |
| :--- | :--- |
| Mechanical Properties |  |
| Hardness | RC $38-43$ |
| Tensile Stress | 170,000 psi min. |
| Yield Strength | 150,000 psi min. |

Length 'L' Tolerance (in)

| Screw Over | upto \& incl | Tolerance |
| :---: | :---: | :---: |
| - | 1 | -.030 |
| 1 | $21 / 2$ | -.040 |
| $21 / 2$ | - | -.060 |

## Tensile and Shear Strength

| Thread size nom. | Tensile Strength - lbs. min. |  | Shear strength in threads (calculated lbs.) |  |
| :---: | :---: | :---: | :---: | :---: |
|  | UNRC | UNRF | UNRC | UNRF |
| \#8 | 2,380 | 2,500 | 1,450 | 1,570 |
| \#10 | 2,980 | 3,400 | 1,700 | 2,140 |
| 1/4 | 5,410 | 6,180 | 3,090 | 3,900 |
| 5/16 | 8,910 | 9,870 | 4,930 | 6,210 |
| 3/8 | 13,200 | 14,900 | 7,450 | 9,400 |
| 1/2 | 24,100 | 27,200 | 13,600 | 17,100 |

Product Dimensions

| Thread size nom. | Thread per Inch UNRC UNRF |  | Body Diameter B max | Head Diameter A |  | Hex <br> Socket Size W nom. | Head <br> Height <br> H |  | Fillet Extension R |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | max | min | max |  | min | max | min |
| \#8 | 32 | 36 |  | 0.1640 | . 270 | . 265 | . 0781 | . 085 | . 079 | . 012 | . 007 |
| \#10 | 24 | 32 | 0.1900 | . 312 | . 307 | . 0938 | . 098 | . 092 | . 014 | . 009 |
| 1/4 | 20 | 28 | 0.2500 | . 375 | . 369 | . 1250 | . 127 | . 121 | . 014 | . 009 |
| 5/16 | 18 | 24 | 0.3125 | . 437 | . 431 | . 1562 | . 158 | . 152 | . 017 | . 012 |
| 3/8 | 16 | 24 | 0.3750 | . 562 | . 556 | . 1875 | . 192 | . 182 | . 020 | . 015 |
| 1/2 | 13 | 20 | 0.5000 | . 750 | . 743 | . 2500 | . 254 | . 244 | . 026 | . 020 |


|  | Socket | Thread <br> Thread <br> size | Depth <br> nom. |
| :---: | :---: | :---: | :---: |
| min. | Tength <br> ref. | Recommended <br> seating torque |  |
| $\# 8$ | .060 | .875 | in-lbs. |
| $\# 10$ | .072 | .875 | 25 |
| $1 / 4$ | .094 | 1.000 | 35 |
| $5 / 16$ | .110 | 1.125 | 157 |
| $3 / 8$ | .115 | 1.250 | 278 |
| $1 / 2$ | .151 | 1.500 | 667 |

## NOTES:

1. Body and Grip lengths are same as

UNC/UNF Socket Head Cap Screws.
(see pageno. 24)
2. Thread Class: 3 A UNRC and UNRF

## Head Marking



Head markings may vary slightly depending on manufacturing practice. UNBRAKO and UNB are recognized identifications for $1 / 4^{\prime \prime}$ diameter \& larger.

## 10．9 Metric

| Size | Part No． | lbs． <br> $/ 1000$ |  |
| ---: | :---: | :---: | :---: |
|  | $M 4(0.7)$－Key Size $3 M M$ |  |  |
| $M 4 \times 8$ | 106250 | 200 | 2.86 |
| 10 | 106251 | 200 | 3.30 |
| 12 | 106255 | 200 | 3.74 |
| 16 | 106256 | 200 | 4.40 |
| 20 | 106257 | 200 | 5.06 |
| 25 | 106260 | 200 | 6.16 |
| 30 | 406185 | 200 | 7.04 |


| M5（0．8）－Key Size 4MM |  |  |  |
| ---: | :---: | :---: | ---: |
| M5 x 8 | 106262 | 200 | 4.84 |
| 10 | 103500 | 200 | 5.50 |
| 12 | 103501 | 200 | 6.38 |
| 15 | 400790 | 200 | 7.26 |
| 16 | 103502 | 200 | 7.48 |
| 20 | 103597 | 200 | 8.80 |
| 25 | 103503 | 200 | 10.56 |
| 30 | 103505 | 200 | 11.26 |


| M6（1）－Key Size 5MM |  |  |  | 40 | 103564 | 25 | 183.04 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M6x 8 | 106263 | 200 | 6.60 | 45 | 106277 | 25 | 199.76 |
| 10 | 103508 | 200 | 8.14 | 50 | 103565 | 25 | 216.48 |
| 12 | 103509 | 200 | 8.89 | 60 | 103566 | 25 | 249.92 |
| 15 | 400792 | 200 | 10.56 | 90 | 103574 | 25 | 356.40 |
| 16 | 103511 | 200 | 10.41 | 100 | 103575 | 25 | 383.68 |


| 20 | 103512 | 200 | 12.76 |
| :--- | :--- | :--- | :--- |
| 25 | 103515 | 200 | 15.18 |
| 30 | 103516 | 200 | 17.38 |
| 35 | 103517 | 200 | 19.80 |
| 40 | 103518 | 200 | 22.00 |
| 45 | 106264 | 200 | 24.42 |

M8（1．25）－Key Size 6MM

| M8 x 12 | 103519 | 200 | 18.04 |
| ---: | ---: | ---: | ---: |
| 15 | 400791 | 200 | 20.46 |
| 16 | 103520 | 200 | 21.34 |
| 20 | 103521 | 200 | 24.64 |
| 25 | 103525 | 200 | 28.82 |
| 30 | 103526 | 200 | 33.00 |
| 35 | 103528 | 200 | 36.96 |
| 40 | 103529 | 200 | 41.14 |


| M10（1．5）－Key Size 8MM |  |  |  |
| ---: | ---: | ---: | ---: |
| M10 $\times 16$ | 103532 | 200 | 35.86 |
| 20 | 103533 | 200 | 40.19 |
| 25 | 103534 | 200 | 45.65 |
| 30 | 103535 | 200 | 54.12 |


| M20（2．5）－Key Size 14MM |  |  |  |
| ---: | :---: | :---: | :---: |
| M20 $\times 40$ | 103578 | 25 | 301.4 |
| 50 | 103580 | 25 | 354.2 |
| 60 | 103581 | 25 | 407.0 |
| 100 | 103599 | 25 | 631.4 |

Sizes above the bold line are threaded to head．


| $\# 10-24$ UNC－Key Size 3／32＂1 |  |  |  |
| :---: | :---: | :---: | :---: |
| $\# 10 \times 3 / 8$ | 100556 | 100 | 4.18 |
| $1 / 2$ | 100579 | 100 | 4.75 |
| $5 / 8$ | 100505 | 100 | 5.48 |
| $3 / 4$ | 100717 | 100 | 6.18 |
| 1 | 100623 | 100 | 8.36 |


| $\# 10-32$ UNF－Key Size 3／32＂ |  |  |  |
| ---: | ---: | ---: | ---: |
| $\# 10 \times 3 / 8$ | 100575 | 100 | 4.40 |
| $1 / 2$ | 100541 | 100 | 5.06 |
| $5 / 8$ | 100542 | 100 | 5.79 |
| $3 / 4$ | 100718 | 100 | 6.82 |
| $1 / 4-20$ UNC－Key Size 1／8＂ |  |  |  |
| $1 / 4 \times 3 / 8$ | 100506 | 100 | 7.70 |
| $1 / 2$ | 100607 | 100 | 9.02 |
| $5 / 8$ | 100507 | 100 | 9.94 |
| $3 / 4$ | 100508 | 100 | 11.66 |
| 1 | 100719 | 100 | 14.08 |


| $5 / 16-18$ UNC－Key Size 5／32＂ |  |  |  |
| ---: | ---: | ---: | ---: |
| $5 / 16 \times 1 / 2$ | 100720 | 100 | 14.74 |
| $3 / 4$ | 100543 | 100 | 18.92 |
| 1 | 100620 | 100 | 23.10 |
| $11 / 4$ | 100686 | 100 | 26.60 |
| $11 / 2$ | 100544 | 100 | 31.68 |


| $3 / 8-16$ UNC－Key Size 3／16＂ |  |  |  |  |
| ---: | ---: | ---: | ---: | ---: |
|  | $3 / 8 \times 1 / 2$ | 100608 | 100 | 25.08 |
| $3 / 4$ | 100609 | 100 | 30.58 |  |
| 1 | 100509 | 100 | 36.70 |  |
| $11 / 4$ | 100613 | 100 | 43.56 |  |
| $11 / 2$ | 100565 | 100 | 48.93 |  |

All inch sizes are threaded to head．

# SOCKET HEAD SHOULDER SCREWS 

Unbrako shoulder screws are hardened shafts with a knurled head and threaded portion. The shoulder formed where the threads meet the larger diameter body acts as a stop when the screw is threaded into a tapped hole, permitting the screw to be used as a pivot, shaft, or stationary guide.

Unbrako shoulder screws are used to operate stripper plates and in pressure pads a wide variety of tool and die work. They are also used as shafts or pivots, holding pulleys, gears, cams and cam followers, ratchets and circular form tools. Stationary guide applications including locating pins in fixtures, latch stops, alignment of stationary members, linkage blocks, and stock guides in dies. Unbrako shoulder screws are especially advantageous in applications where the fastened part must be removed frequently. For instance, when the shoulder screw is used as a shaft for circular form tools, the screw can be removed to permit sharpening of the tool in a matter of seconds. Assembly is equally as fast.

Unbrako shoulder screws are made of high grade alloy steel the precision tolerance on the shoulder provides close and accurate mating with the fastened components. Unbrako manufactures to a tolerance position closer than that required by international standards.

## FEATURES

Precision hex socket for maximum wrenching strength permits full tightening without cracking or reaming socket, yet provides ample metal in the crucial fillet area for maximum head strength.

Neck allows assembly with no chamfering or other hole preparation.

Knurled head for sure finger grip and fast assembly
ed concentricity between head and body for easier, more accurate assembly

Controlled root radius doubles fatigue life of threads by reducing stress concentrations and avoiding sharp corners where failures may start. Contour following flow lines of rolled threads provide extra strength, prevent stripping.

Shoulder diameter held to close tolerance



Replaces costly special parts－shafts， pivots，pins，guides，linkages and trunnion mountings．Also standard for tool and die industries．

## Equivalent Standard

Specification：Generally conforming to ISO 7379，ASME B18．3．3M，BS 4168－7

## Mechanical Properties

Material：Unbrako High Grade Alloy Steel
Thread Class：4g6g
Hardness：Rc 39－43
Shear Strength： $730 \mathrm{~N} / \mathrm{mm} 2$
Working Temperatures：$-50^{\circ} \mathrm{C}$ to $300^{\circ} \mathrm{C}$

## Note

Because of their configuration，these screws cannot be tensile tested．

## Head Marking



Head markings may vary slightly depending on manufacturing practice． UNBRAKO and UNB are recognized identifications for M6 diameter \＆larger．


Product Dimensions

| Body size nom | Thread size | Pitch | Head Diameter A | $\begin{gathered} \text { Hex } \\ \text { Socket Size } \\ \text { W } \end{gathered}$ | Head <br> Height <br> H | Socket Depth T | Shoulder diameter |  | J |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | max | nom | max | min | max | min | max |
| 6 | M5 | 0.80 | 10.00 | 3 | 4.50 | 2.4 | 6 | 5.96 | 3.84 |
| 8 | M6 | 1.00 | 13.00 | 4 | 5.50 | 3.3 | 8 | 7.95 | 4.56 |
| 10 | M8 | 1.25 | 16.00 | 5 | 7.00 | 4.2 | 10 | 9.95 | 6.23 |
| 12 | M10 | 1.50 | 18.00 | 6 | 8.00 | 4.9 | 12 | 11.95 | 7.89 |
| 16 | M12 | 1.75 | 24.00 | 8 | 10.00 | 6.6 | 16 | 15.95 | 9.54 |
| 20 | M16 | 2.00 | 30.00 | 10 | 14.00 | 8.8 | 20 | 19.95 | 13.20 |
| 24 | M20 | 2.50 | 36.00 | 12 | 16.00 | 10.0 | 24 | 23.95 | 16.54 |


| Body size nom． | $\begin{gathered} \text { da } \\ \max \end{gathered}$ | $\underset{\max }{N}$ | $\underset{\max }{\mathrm{G}}$ | $\underset{\max }{M}$ | Thread Length E max | Recommended seating torque |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | N －m | in－lbs． |
| 6 | 6.80 | 2.00 | 5.62 | 1.85 | 9.75 | 7 | 60 |
| 8 | 9.20 | 2.50 | 7.62 | 1.85 | 11.25 | 12 | 105 |
| 10 | 11.20 | 3.00 | 9.62 | 1.85 | 13.25 | 29 | 255 |
| 12 | 14.20 | 3.50 | 11.62 | 1.85 | 16.40 | 57 | 500 |
| 16 | 18.20 | 4.00 | 15.62 | 1.85 | 18.40 | 100 | 885 |
| 20 | 22.40 | 4.50 | 19.62 | 2.50 | 22.40 | 240 | 2，125 |
| 24 | 26.40 | 5.60 | 23.62 | 2.65 | 27.40 | 470 | 4，160 |

CONCENTRICITY－Body to head O．D．within 0．002 TIR when checked in $a^{\prime}$ V＇block．Body to thread P．D．within 0.004 TIR when checked at a distance of 0.188 from the shoulder at the threaded end．Squareness， concentricity，parallelism and bow of body to thread P．D．shall be within 0.005 TIR per inch of body length with a maximum of 0.020 when seated against the shoulder in a threaded bush and checked on the body at a distance of 2 M from the underside of the head．

| Size | Part No. | lbs. <br> $/ 1000$ |
| :--- | :--- | :--- | :---: |

6 mm (M5-0.8) - Key Size 3mm

| $6 \times 10$ | 105364 | 50 | 12.43 |
| ---: | ---: | ---: | ---: |
| 12 | 105365 | 50 | 13.49 |
| 16 | 105366 | 50 | 15.58 |
| 20 | 105368 | 50 | 17.93 |
| 25 | 105370 | 50 | 20.28 |
| 30 | 105372 | 50 | 22.90 |
| 40 | 105373 | 50 | 28.14 |


| $8 \mathrm{~mm}($ M6-1) - Key Size 4mm |  |  |  |
| :---: | :---: | :---: | :---: |
| $8 \times 12$ | 105375 | 50 | 26.00 |
| 16 | 105377 | 50 | 29.63 |
| 20 | 105379 | 50 | 33.29 |
| 25 | 105380 | 50 | 37.84 |
| 30 | 105381 | 50 | 42.39 |
| 40 | 105383 | 50 | 51.50 |
| 50 | 105386 | 50 | 60.59 |


| $10 \mathrm{~mm}($ M8-1.25 $)$ |  |  |  |
| ---: | ---: | ---: | ---: |
| $10 \times 16$ | 105388 | 50 | 51.04 |
| 20 | 105390 | 50 | 56.72 |
| 25 | 105392 | 50 | 63.82 |
| 30 | 105393 | 50 | 70.91 |
| 40 | 105394 | 50 | 85.07 |
| 50 | 105395 | 50 | 99.26 |
| 60 | 105396 | 50 | 113.30 |
| 70 | 105402 | 50 | 127.60 |
| 80 | 106422 | 50 | 141.79 |

12mm (M10-1.5) - Key Size 6 mm

| $12 \times 15$ | 401485 | 25 | 78.56 |
| ---: | ---: | ---: | ---: |
| 16 | 105404 | 25 | 80.61 |
| 20 | 105406 | 25 | 88.70 |
| 25 | 105407 | 25 | 98.85 |
| 30 | 105410 | 25 | 109.01 |
| 40 | 105411 | 25 | 129.29 |
| 50 | 105412 | 25 | 149.58 |
| 60 | 105416 | 25 | 169.86 |
| 70 | 105417 | 25 | 190.15 |
| 80 | 105420 | 25 | 210.43 |
| 90 | 105427 | 25 | 230.74 |
| 100 | 105433 | 25 | 251.02 |

16mm (M12-1.75) - Key Size 8mm

| $16 \times 30$ | 105434 | 25 | 203.02 |
| ---: | ---: | ---: | ---: |
| 40 | 105435 | 25 | 238.70 |
| 50 | 105436 | 25 | 274.38 |
| 60 | 105437 | 25 | 310.05 |
| 70 | 105438 | 25 | 345.73 |


| Size | Part No. | lbs. <br> $/ 1000$ |
| :--- | :--- | :---: | :---: |


| $16 \mathrm{~mm}(\mathrm{M} 12-1.75)$ |  |  |  |
| ---: | :---: | :---: | :---: |
| $16 \times 80$ | 105440 | 25 | 381.39 |
| 90 | 106343 | 25 | 417.08 |
| 100 | 106344 | 25 | 452.76 |
| 120 | 106346 | 25 | 524.11 |
|  |  |  |  |
| 20 mm | (M16-2) - Key Size 8 mm |  |  |
| $20 \times 40$ | 105441 | 10 | 423.61 |
| 50 | 105442 | 10 | 479.14 |
| 60 | 105444 | 10 | 534.64 |
| 70 | 105448 | 10 | 590.17 |
| 80 | 105449 | 10 | 645.68 |
| 90 | 105450 | 10 | 701.21 |
| 100 | 106347 | 10 | 756.71 |
| 120 | 106348 | 10 | 867.75 |


| $24 \mathrm{~mm}(\mathrm{M} 20-2.5)-$ Key Size 12 mm |  |  |  |
| ---: | ---: | ---: | ---: |
| $24 \times 50$ | 401488 | 5 | 828.50 |
| 60 | 401489 | 5 | 906.49 |
| 70 | 401490 | 5 | 984.48 |
| 80 | 401491 | 5 | 1062.49 |
| 90 | 401492 | 5 | 1140.48 |
| 100 | 401493 | 5 | 1218.47 |
| 120 | 401494 | 5 | 1372.80 |

Note:

- Precision ground to h8 Tolerance on the shoulder.
-The Nominal Diameter of a shoulder screw is the diameter of the shoulder and not the thread diameter, but it is recommended that both are quoted when ordering Eg. $16 \mathrm{~mm} \times \mathrm{M} 12 \times 70$



Replaces costly special parts－shafts， pivots，pins，guides，linkages and trunnion mountings．Also standard for tool and die industries．

## Equivalent Standard

ASME B18．3，BS 2470

## Mechanical Properties

Hardness：Rockwell C 39－43；
Shear Strength：108，000 lbf／in ${ }^{2}$
Working temperature：$-50^{\circ}$ to $+300^{\circ} \mathrm{C}$
Thread class：3A
Seating Torques and Strength

| Thread <br> size <br> nom． | seating <br> torque <br> in－lbs． | ult．tensile <br> strength <br> lbs．$(\mathrm{min})$ | single shear <br> strength <br> of body <br> lbs．（min） |
| :--- | ---: | ---: | ---: |
| $1 / 4$ | 45 | 2,220 | 4,710 |
| $5 / 16$ | 112 | 4,160 | 7,360 |
| $3 / 8$ | 230 | 7,060 | 10,500 |
| $1 / 2$ | 388 | 10,600 | 18,850 |
| $5 / 8$ | 990 | 19,810 | 29,450 |
| $3 / 4$ | 1,975 | 31,670 | 42,410 |
| 1 | 3,490 | 47,680 | 75,400 |
| $1-1 / 4$ | 5,610 | 66,230 | 117,800 |
| $1-1 / 2$ | 12,000 | 110,000 | 169,500 |
| $1-3 / 4$ | 16,000 | 141,000 | 231,000 |
| 2 | 30,000 | 205,000 | 301,500 |

## Note

Because of their configuration，these screws cannot be tensile tested．

## Head Marking



Head markings may vary slightly depending on manufacturing practice． UNBRAKO and UNB are recognized identifications for $1 / 4^{\prime \prime}$ diameter \＆larger


Product Dimensions

| Body size nom． | Thread size | Threads per Inch UNRC | Head Diameter A max． | Hex Socket Size W nom | Head <br> Height H max | Socket <br> Depth T min． | Shoulder diameter D |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1／4 | \＃10 | 24 | ． 375 | ． 125 | ． 188 | ． 094 | ． 248 | ． 246 |
| 5／16 | 1／4 | 20 | ． 438 | ． 156 | ． 219 | ． 117 | ． 311 | ． 309 |
| 3／8 | 5／16 | 18 | ． 562 | ． 188 | ． 250 | ． 141 | ． 373 | ． 371 |
| 1／2 | 3／8 | 16 | ． 750 | ． 250 | ． 312 | ． 188 | ． 498 | ． 496 |
| 5／8 | 1／2 | 13 | ． 875 | ． 312 | ． 375 | ． 234 | ． 623 | ． 621 |
| 3／4 | 5／8 | 11 | 1.000 | ． 375 | ． 500 | ． 281 | ． 748 | ． 746 |
| 1 | 3／4 | 10 | 1.312 | ． 500 | ． 625 | ． 375 | ． 998 | ． 996 |
| $11 / 4$ | 7／8 | 9 | 1.750 | ． 625 | ． 750 | ． 469 | 1.248 | 1.246 |
| $11 / 2$ | $11 / 8$ | 7 | 2.125 | ． 875 | 1.000 | ． 656 | 1.498 | 1.496 |
| $13 / 4$ | $11 / 4$ | 7 | 2.375 | 1.000 | 1.125 | ． 750 | 1.748 | 1.746 |
| 2 | $11 / 2$ | 6 | 2.750 | 1.250 | 1.250 | ． 937 | 1.998 | 1.996 |


| Body <br> size <br> nom． | Gax. | K <br> $\min$ | I <br> max | Fax | Thread <br> Length <br> E |
| :--- | :---: | :---: | :---: | :---: | :---: |
| $1 / 4$ | .142 | .227 | .083 | .093 | .375 |
| $5 / 16$ | .193 | .289 | .100 | .093 | .438 |
| $3 / 8$ | .249 | .352 | .111 | .093 | .500 |
| $1 / 2$ | .304 | .477 | .125 | .093 | .625 |
| $5 / 8$ | .414 | .602 | .154 | .093 | .750 |
| $3 / 4$ | .521 | .727 | .182 | .093 | .875 |
| 1 | .638 | .977 | .200 | .125 | 1.000 |
| $1-1 / 4$ | .750 | 1.227 | .222 | .125 | 1.125 |
| $1-1 / 2$ | .964 | 1.478 | .286 | .125 | 1.500 |
| $1-3 / 4$ | 1.089 | 1.728 | .286 | .125 | 1.750 |
| 2 | 1.307 | 1.978 | .333 | .125 | 2.000 |

## NOTES

Concentricity：Head to body－within ． 005 T．I．R．when checked in＂$V$＂block equal to or longer than body length．Pitch diameter to body－within ． 004 T．I．R．when held in threaded bushing and checked at a distance of $3 / 16^{\prime \prime}$ from shoulder at threaded end．

Shoulder must rest against face of shoulder of standard＂GO＂ring gage．
Bearing surface of head－perpendicular to axis of body within $2^{\circ}$ maximum deviation．

Tensile strength based on minimum neck area＂G．＂Shear strength based on shoulder diameter＂D．＂

Screw point chamfer：The point shall be flat or slightly concave，and chamfered．The plane of the point shall be approximately normal to the axis of the screw．The chamfer shall extend slightly below the root of the thread，and the edge between flat and chamfer may be slightly rounded．The included angle of the point should be approximately $90^{\circ}$ ．

| Size | Part No. | lbs. <br> $/ 1000$ |
| ---: | :---: | :---: |
| $1 / 4^{\prime \prime}(\# 10-24)$ |  | UNC - Key Size $1 / 8^{\prime \prime}$ |
| $1 / 4^{\prime \prime} \times 3 / 8$ | 103614 | 25 |
| $1 / 2$ | 115475 | 25 |
| $5 / 8$ | 115729 | 25 |
| $3 / 4$ | 115859 | 25 |
| 1 | 102352 | 25 |
| $11 / 4$ | 111469 | 25 |
| $11 / 2$ | 117980 | 25 |



1/2" (3/8-16) UNC - Key Size 1/4"

| $1 / 2^{\prime \prime} \times 23 / 4$ | 113509 | 25 | 198.37 |
| ---: | ---: | ---: | ---: |
| 3 | 102884 | 25 | 212.17 |
| $31 / 4$ | 111946 | 25 | 225.94 |
| $31 / 2$ | 111978 | 25 | 239.71 |
| $33 / 4$ | 112011 | 25 | 253.51 |
| 4 | 108444 | 25 | 267.28 |
| $41 / 4$ | 108477 | 25 | 281.07 |
| $41 / 2$ | 108510 | 10 | 294.84 |
| $43 / 4$ | 108544 | 10 | 308.62 |
| 5 | 102921 | 10 | 322.41 |
| $51 / 2$ | 116309 | 10 | 349.98 |
| 6 | 116311 | 10 | 377.52 |

5/8" (1/2-13) UNC - Key Size 5/16"

| $5 / 8^{\prime \prime} \times 1$ | 115741 | 25 | 169.47 |
| ---: | ---: | ---: | ---: |
| $11 / 4$ | 102954 | 25 | 191.03 |


| $11 / 2$ | 106331 | 25 | 43.63 |
| ---: | ---: | ---: | ---: |
| $13 / 4$ | 106395 | 25 | 48.97 |
| 2 | 106459 | 25 | 54.34 |

$3 / 8^{\prime \prime}(5 / 16-18)$ UNC - Key Size 3/16"

| $3 / 8^{\prime \prime} \times 3 / 8$ | 106524 | 25 | 33.77 |
| ---: | ---: | ---: | ---: |
| $1 / 2$ | 111791 | 25 | 37.64 |
| $5 / 8$ | 116768 | 25 | 41.49 |
| $3 / 4$ | 116800 | 25 | 45.36 |
| 1 | 110993 | 25 | 53.09 |
| $11 / 4$ | 111025 | 25 | 60.83 |
| $11 / 2$ | 118465 | 25 | 68.55 |
| $13 / 4$ | 114133 | 25 | 76.30 |
| 2 | 114166 | 25 | 84.02 |
| $21 / 4$ | 114200 | 25 | 91.74 |
| $21 / 2$ | 114233 | 25 | 99.48 |
| $23 / 4$ | 119970 | 25 | 107.21 |
| 3 | 120003 | 25 | 114.95 |
| $31 / 4$ | 120036 | 25 | 122.67 |
| $31 / 2$ | 120069 | 25 | 130.39 |
| $33 / 4$ | 120101 | 25 | 138.14 |
| 4 | 118103 | 25 | 145.86 |


| $1 / 2^{\prime \prime}(3 / 8-16)$ UNC - Key Size $1 / 4^{\prime \prime}$ |  |  |  |
| ---: | ---: | ---: | ---: |
| $1 / 2^{\prime \prime} \times 1 / 2$ | 119560 | 25 | 74.36 |
| $5 / 8$ | 107602 | 25 | 81.25 |
| $3 / 4$ | 107634 | 25 | 88.13 |
| 1 | 113288 | 25 | 101.90 |
| $11 / 4$ | 106400 | 25 | 115.70 |
| $11 / 2$ | 106432 | 25 | 129.47 |
| $13 / 4$ | 106465 | 25 | 143.26 |
| 2 | 106497 | 25 | 157.04 |
| $21 / 4$ | 113444 | 25 | 170.81 |
| $21 / 2$ | 113476 | 25 | 184.60 |


| $3 / 4$ (5/8-11) unc-Key size $3 / 8$ |  |  |  |
| ---: | :---: | :---: | ---: |
| $3 / 4^{\prime \prime} \times 3 / 4$ | 102298 | 25 | 241.18 |
| 1 | 102365 | 25 | 272.27 |
| $11 / 4$ | 102397 | 25 | 303.38 |
| $11 / 2$ | 108998 | 10 | 334.47 |
| $13 / 4$ | 125809 | 10 | 365.55 |
| 2 | 113145 | 10 | 396.00 |
| $21 / 4$ | 107658 | 10 | 427.72 |
| $21 / 2$ | 107690 | 10 | 458.83 |
| $23 / 4$ | 107722 | 10 | 489.92 |
| 3 | 113244 | 10 | 521.00 |
| $31 / 4$ | 107461 | 10 | 552.09 |
| $31 / 2$ | 107493 | 10 | 583.18 |

3/4" (5/8-11) UNC - Key Size 3/8"

| $3 / 4^{\prime \prime} \times 33 / 4$ | 107525 | 10 | 614.26 |
| ---: | ---: | ---: | ---: |
| 4 | 107557 | 10 | 645.37 |
| $41 / 4$ | 107590 | 10 | 676.46 |
| $41 / 2$ | 107622 | 10 | 707.54 |
| $43 / 4$ | 113276 | 10 | 738.63 |
| 5 | 113308 | 10 | 769.71 |
| $51 / 2$ | 106420 | 10 | 831.91 |
| 6 | 106452 | 10 | 894.08 |
| $61 / 2$ | 117921 | 10 | 956.25 |
| 7 | 117938 | 10 | 1018.45 |

Note:
The nominal diameter of a shoulder screw is the diameter of the shoulder, and not the thread diameter, but it is recommended that both are quoted when ordering. Eg $1 / 2 \times 5 / 8$ UNC $\times 1$

## FLAT HEAD COUNTERSUNK SOCKET SCREWS



Modern equipment and machinery requires stronger more reliable joints to hold their parts together - and stronger more reliable fasteners.

That's why Unbrako countersunk screws are so widely used for fastening of plates, strips, mouldings, and other thin section parts. Unbrako countersunk screws provide reliable fastening and a smooth, attractive, flush mounting that enhances the appearance of the product on which they are used.

Unbrako countersunk screws provide more clamping force because they are manufactured from high grade alloy steel, and held to exacting tolerances to ensure the highest degree of dimensional uniformity. The closely controlled head angle assures flush seating, and close all-round head contact by initially contacting at the upper portion of the head bearing area in the countersunk hole. Closely controlled threads mean tighter and more secure fits, and stronger assemblies. Deep accurate non-slip sockets provide maximum key engagement for full tightening without marring the surrounding surface.

Unbrako countersunk screws are available with either plain or plated finish. Stainless steel screws are also available.

## FEATURES




Controlled angle under the head ensures maximum flushness and side wall contact. Non-slip Hex socket prevents marring of material.

## Equivalent Standards

ISO 10642, ASME B18.3.5M,
DIN 7991, BS 4168-8

## Mechanical Properties

Material: Unbrako High Grade Alloy Steel
Property Class: 012.9
Heat Treatment: Rc 39-44
Shear Strength: $630 \mathrm{~N} / \mathrm{mm}^{2}$
Min. Elongation: 9\%
Tensile Strength: 1040 Mpa
Shear Strength: 630 Mpa
Yield Strength: 945 Mpa

## Notes

1. Thread Class: ANSI B1.13M, ISO262
2. Working Temperature: $-50^{\circ} \mathrm{C}$ to $+300^{\circ} \mathrm{C}$
3. For sizes up to and including M20 Head Angle shall be $92^{\circ} / 90^{\circ}$, over M20 Head Angle be $62^{\circ} / 60^{\circ}$.
4. Torque calculated in accordance with VDI2230 -"Systematic calculation of high duty bolted joints" with $\sigma 0.2=720 \mathrm{~N} / \mathrm{mm}^{2}$ and $\mu=.125$ for plain finish and $\mu=0.094$ for plated.

Length 'L' Tolerance (mm)

| Screws <br> Over | Up to and <br> including | Tolerance |
| :--- | :---: | :---: |
| - | 50 | $\pm 0.25$ |
| 50 | 80 | $\pm 0.50$ |
| 80 | 120 | $\pm 0.70$ |
| 120 | 250 | $\pm 0.80$ |
| 250 | - | $\pm 1.02$ |

## Head Marking



General Note: Flat, countersunk head cap screws and button head cap screws are designed and recommended for moderate fastening applications: machine guards, hinges, covers, etc. They are not suggested for use in critical high load strength applications where socket head cap screws should be used. Also due to their head configuration they may not meet the minimum ultimate tensile requirements for property class 12.9 as specified in EN ISO 898-1. They are nevertheless required to meet the other material and property requirements for property class 12.9.

## Body and Grip Length Dimensions

- LG is the maximum grip length and is the distance from the bearing surface to the first complete thread.
- LB is the minimum body length and is the length of the unthreaded cylindrical portion of the shank.
- Dimensions for LB and LG are calculated from the following formula:

T Ref $=(2 x$ Nominal Dia) plus 12 mm .
LG max = Nominal length "L" minus " $T$ "
LB min $=$ Nominal length " L " minus ( $\mathrm{T}+5$ pitches)


| Length | M3 |  | M4 |  | M5 |  | M6 |  | M8 |  | M10 |  | M12 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L Nom. | $\begin{gathered} L_{B} \\ (\mathrm{~min}) \end{gathered}$ | $\begin{gathered} L_{G} \\ (\max ) \end{gathered}$ | $\begin{gathered} L_{B} \\ (\mathrm{~min}) \end{gathered}$ | $\begin{gathered} L_{G} \\ (\max ) \end{gathered}$ | $\begin{gathered} L_{B} \\ (\mathrm{~min}) \end{gathered}$ | $\begin{gathered} L_{G} \\ (\max ) \end{gathered}$ | $\begin{gathered} L_{B} \\ (\mathrm{~min}) \end{gathered}$ | $\begin{gathered} L_{G} \\ (\max ) \end{gathered}$ | $\begin{gathered} L_{B} \\ (\mathrm{~min}) \end{gathered}$ | $\begin{gathered} L_{G} \\ (\max ) \end{gathered}$ | $\begin{gathered} L_{B} \\ (\mathrm{~min}) \end{gathered}$ | $\begin{gathered} L_{G} \\ (\max ) \end{gathered}$ | $\begin{gathered} L_{B} \\ (\mathrm{~min}) \end{gathered}$ | $\begin{gathered} L_{G} \\ (\max ) \end{gathered}$ |
| 30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 35 | 14.5 | 17.0 | 11.5 | 15.0 |  |  |  |  |  |  |  |  |  |  |
| 40 | 19.5 | 22.0 | 16.5 | 20.0 | 14.0 | 18.0 |  |  |  |  |  |  |  |  |
| 45 | 24.5 | 27.0 | 21.5 | 25.0 | 19.0 | 23.0 | 16.0 | 21.0 |  |  |  |  |  |  |
| 50 | 29.5 | 32.0 | 26.5 | 30.0 | 24.0 | 28.0 | 21.0 | 26.0 | 15.75 | 22.0 |  |  |  |  |
| 55 | 34.5 | 37.0 | 31.5 | 35.0 | 29.0 | 33.0 | 26.0 | 31.0 | 20.75 | 27.0 |  |  |  |  |
| 60 |  |  | 36.5 | 40.0 | 34.0 | 38.0 | 31.0 | 36.0 | 25.75 | 32.0 | 20.5 | 28.0 |  |  |
| 65 |  |  | 41.5 | 45.0 | 39.0 | 43.0 | 36.0 | 41.0 | 30.75 | 37.0 | 25.5 | 33.0 | 20.2 | 29.0 |
| 70 |  |  | 46.5 | 50.0 | 44.0 | 48.0 | 41.0 | 46.0 | 35.75 | 42.0 | 30.5 | 38.0 | 25.2 | 34.0 |
| 80 |  |  | 56.5 | 60.0 | 54.0 | 58.0 | 51.0 | 56.0 | 45.75 | 52.0 | 40.5 | 48.0 | 35.2 | 44.0 |
| 90 |  |  |  |  | 64.0 | 68.0 | 61.0 | 66.0 | 55.70 | 62.0 | 50.5 | 58.0 | 45.2 | 54.0 |
| 100 |  |  |  |  | 74.0 | 78.0 | 71.0 | 76.0 | 65.70 | 72.0 | 60.5 | 68.0 | 55.2 | 64.0 |
| 110 |  |  |  |  |  |  | 81.0 | 86.0 | 75.70 | 82.0 | 70.5 | 78.0 | 65.2 | 74.0 |
| 120 |  |  |  |  |  |  | 91.0 | 96.0 | 85.70 | 92.0 | 80.5 | 88.0 | 75.2 | 84.0 |
| 130 |  |  |  |  |  |  |  |  | 95.70 | 102.0 | 90.5 | 98.0 | 85.2 | 94.0 |
| 140 |  |  |  |  |  |  |  |  | 105.70 | 112.0 | 100.5 | 108.0 | 95.2 | 104.0 |
| 150 |  |  |  |  |  |  |  |  | 115.70 | 122.0 | 110.5 | 118.0 | 105.2 | 114.0 |


| Length | M14 |  | M16 |  | M18 |  | M20 |  | M22 |  | M24 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L Nom. | $\begin{gathered} L_{B} \\ \text { (Max.) } \end{gathered}$ | $\begin{gathered} L_{G} \\ \text { (Max.) } \end{gathered}$ | $\begin{gathered} L_{B} \\ \text { (Max.) } \end{gathered}$ | $\begin{gathered} L_{G} \\ \text { (Max.) } \end{gathered}$ | $L_{B}$ <br> (Max.) | $\begin{gathered} L_{G} \\ \text { (Max.) } \end{gathered}$ | $\begin{gathered} L_{B} \\ \text { (Max.) } \end{gathered}$ | $\begin{gathered} L_{G} \\ \text { (Max.) } \end{gathered}$ | $\begin{gathered} L_{B} \\ \text { (Max.) } \end{gathered}$ | $\begin{gathered} L_{G} \\ (\text { Max. }) \end{gathered}$ | $\begin{gathered} L_{B} \\ \text { (Max.) } \end{gathered}$ | $\begin{gathered} L_{G} \\ \text { (Max.) } \end{gathered}$ |
| 70 | 20.0 | 30.0 |  |  |  |  |  |  |  |  |  |  |
| 80 | 30.0 | 40.0 | 26.0 | 36.0 |  |  |  |  |  |  |  |  |
| 90 | 40.0 | 50.0 | 36.0 | 46.0 | 29.5 | 42.0 |  |  |  |  |  |  |
| 100 | 50.0 | 60.0 | 46.0 | 56.0 | 39.5 | 52.0 |  |  |  |  |  |  |
| 110 | 60.0 | 70.0 | 56.0 | 66.0 | 49.5 | 62.0 | 45.5 | 58.0 |  |  |  |  |
| 120 | 70.0 | 80.0 | 66.0 | 76.0 | 59.5 | 72.0 | 55.5 | 68.0 | 51.5 | 64.0 |  |  |
| 130 | 80.0 | 90.0 | 76.0 | 86.0 | 69.5 | 82.0 | 65.5 | 78.0 | 61.5 | 74.0 | 55.0 | 70.0 |
| 140 | 90.0 | 100.0 | 86.0 | 96.0 | 79.5 | 92.0 | 75.5 | 88.0 | 71.5 | 84.0 | 65.0 | 80.0 |
| 150 | 100.0 | 110.0 | 96.0 | 106.0 | 89.5 | 102.0 | 85.5 | 98.0 | 81.5 | 94.0 | 75.0 | 90.0 |
| 160 |  |  | 106.0 | 116.0 | 99.5 | 112.0 | 95.5 | 108.0 | 91.5 | 104.0 | 85.0 | 100.0 |
| 180 |  |  | 126.0 | 136.0 | 119.5 | 132.0 | 115.5 | 128.0 | 111.5 | 124.0 | 105.0 | 120.0 |
| 200 |  |  |  |  | 139.5 | 156.0 | 135.5 | 148.0 | 131.5 | 144.0 | 125.0 | 140.0 |
| 220 |  |  |  |  |  |  |  |  | 151.5 | 164.0 | 145.0 | 160.0 |
| 240 |  |  |  |  |  |  |  |  |  |  | 165.0 | 180.0 |


| Size | Part No. | Ibs. <br> $/ 1000$ |  |
| ---: | :---: | :---: | :---: |
| $\mathrm{M} 3(0.5)$ - Key Size 2 mm |  |  |  |
| M3 $\times 6$ | 106283 | 200 | 0.84 |
| 8 | 103303 | 200 | 1.06 |
| 10 | 103304 | 200 | 1.25 |
| 12 | 103305 | 200 | 1.45 |
| 15 | 401672 | 200 | 1.76 |
| 16 | 103306 | 200 | 1.87 |
| 20 | 103308 | 200 | 2.27 |
| 25 | 106284 | 200 | 2.79 |
| 30 | 106285 | 200 | 3.30 |


| Size | Part No. | Ibs. <br> $/ 1000$ |  |
| ---: | :---: | :---: | :---: |
| M6 (1)- Key Size 4mm |  |  |  |
| M6 $\times 30$ | 103333 | 200 | 14.08 |
| 35 | 103334 | 200 | 16.13 |
| 40 | 103335 | 200 | 18.17 |
| 45 | 106295 | 200 | 20.04 |
| 50 | 106296 | 200 | 24.53 |

Size Part No. $\bigoplus$| Ibs. |
| :---: |
| $/ 1000$ |

M12 (1.75) - Key Size 8mm

| M12 $\times 60$ | 106313 | 50 | 115.50 |
| ---: | ---: | ---: | ---: |
| 70 | 106314 | 50 | 143.99 |
| 80 | 106315 | 50 | 163.68 |
| 90 | 106316 | 50 | 184.56 |
| 100 | 106330 | 50 | 204.82 |


| M8 (1.25) - Key Size 5mm |  |  |  |
| ---: | ---: | ---: | ---: |
| M8 $\times 10$ | 103336 | 200 | 11.70 |
| 12 | 103337 | 200 | 13.18 |
| 15 | 401680 | 200 | 15.40 |
| 16 | 103338 | 200 | 16.15 |
| 18 | 401681 | 200 | 17.62 |
| 20 | 103340 | 200 | 19.10 |
| 25 | 103341 | 200 | 22.77 |
| 30 | 103342 | 200 | 26.47 |
| 35 | 103343 | 200 | 30.16 |
| 40 | 103344 | 200 | 33.86 |
| 45 | 106297 | 200 | 37.53 |
| 50 | 106298 | 200 | 44.62 |
| 55 | 106299 | 100 | 49.66 |
| 60 | 106300 | 100 | 53.53 |
| 70 | 106301 | 100 | 62.44 |


| M16 (2) - Key Size 10mm |  |  |  |
| :---: | :---: | :---: | :---: |
| M16 $\times 30$ | 103359 | 50 | 118.60 |
| 35 | 103360 | 50 | 134.05 |
| 40 | 103361 | 50 | 149.47 |
| 45 | 106318 | 50 | 164.91 |
| 50 | 103362 | 50 | 180.36 |
| 55 | 106320 | 25 | 195.78 |
| 60 | 103363 | 25 | 211.22 |
| 70 | 106321 | 25 | 242.09 |
| 80 | 106322 | 25 | 291.87 |


| M20 (2.5) - Key Size 12mm |  |  |  |
| ---: | ---: | ---: | ---: |
| M20 x 35 | 106328 | 25 | 211.97 |
| 40 | 106332 | 25 | 236.10 |
| 45 | 106334 | 25 | 260.22 |
| 50 | 106335 | 25 | 284.35 |
| 60 | 106337 | 25 | 332.60 |
| 70 | 106338 | 25 | 380.82 |
| 80 | 106339 | 25 | 429.07 |
| 100 | 106342 | 25 | 525.56 |
| 120 | 401685 | 10 | 676.37 |
| 140 | 401686 | 10 | 788.83 |
| 160 | 401687 | 10 | 901.30 |
| M24 (3) - Key Size 14mm |  |  |  |
| M24 x 50 | 220032 | 10 | 407.00 |
| 100 | 401693 | 10 | 721.60 |
| 120 | 183179 | 10 | 857.34 |

Sizes above the bold line are threaded to head.


Controlled angle under the head ensures maximum flushness and side wall contact. Non-slip Hex socket prevents marring of material.

Equivalent Standards
BS 2470, ANSI B18.3
Mechanical Properties
Material: ASTM F835
Hardness: Rc 39-43
Tensile Strength: $96,000 \mathrm{lbf} / \mathrm{in}^{2} \mathrm{~min}$.

| Length Tolerance |  |  |  |
| :---: | :---: | :---: | :---: |
| Diameter | to $1^{\prime \prime}$ | to $21 / 2^{\prime \prime}$ | to |
| \#0 to 3/8" incl. | -. 03 | -. 04 | -. 06 |
| $7 / 16$ to $3 / 4^{\prime \prime}$ incl. | -. 03 | -. 06 | -. 08 |
| $7 / 8$ to 1 "incl. | -. 05 | -. 10 | -. 14 |

## Application Data

| Thread size nom. | Maximum Tightening Torques |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Unplated |  | Plated |  |
|  | UNC | UNF | UNC | UNF |
| \#0 | - | 1.6 | - | 1.2 |
| \#1 | 2.6 | 2.9 | 1.9 | 2.1 |
| \#2 | 4.4 | 4.8 | 3.3 | 3.6 |
| \#3 | 6.7 | 8.5 | 5.0 | 6.3 |
| \#4 | 8.9 | 10.0 | 6.6 | 7.5 |
| \#5 | 13.0 | 14.0 | 9.0 | 10.0 |
| \#6 | 16.0 | 19.0 | 12.0 | 14.0 |
| \#8 | 30.0 | 32.0 | 22.0 | 24.0 |
| \#10 | 44.0 | 51.0 | 33.0 | 38.0 |
| 1/4 | 100.0 | 120.0 | 75.0 | 90.0 |
| 5/16 | 210.0 | 240.0 | 157.0 | 180.0 |
| 3/8 | 380.0 | 430.0 | 285.0 | 322.0 |
| 7/16 | 600.0 | 680.0 | 450.0 | 510.0 |
| 1/2 | 930.0 | 1,050.0 | 697.0 | 787.0 |
| 5/8 | 1,800.0 | 2,000.0 | 1,350.0 | 1,500.0 |
| 3/4 | 3,200.0 | 3,560.0 | 2,400.0 | 2,670.0 |
| 7/8 | 5,400.0 | 6,000.0 | 4,050.0 | 4,500.0 |
| 1 | 8,200.0 | 8,900.0 | 6,150.0 | 6,675.0 |

## Head Marking



Head markings may vary slightly
depending on manufacturing practice.
UNBRAKO, and UNB are recognized identifications for \#10 diameter \& larger.



* maximum - to theoretical sharp corners
**minimum - absolute with A flat

| Thread size | thd-to-hd max | Body Diameter B | Protrusion gage diameter G | Tensile Load lbf |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| nom. | ref | max min | max min | UNC | UNF |
| \#0 | . 500 | . 060.0568 | . 078.077 |  | 265 |
| \#1 | . 750 | . 073.0695 | . 101.100 | 390 | 390 |
| \#2 | . 750 | . 086.0822 | . 124.123 | 555 | 555 |
| \#3 | . 750 | . 099.0949 | . 148.147 | 725 | 725 |
| \#4 | . 875 | . 112.1075 | . 172.171 | 960 | 1,040 |
| \#5 | . 875 | . 125.1202 | . 196.195 | 1,260 | 1,310 |
| \#6 | . 875 | . 138.1329 | . 220.219 | 1,440 | 1,620 |
| \#8 | 1.000 | . 164.1585 | . 267.266 | 2,220 | 2,240 |
| \#10 | 1.250 | . 190.1840 | . 313.312 | 2,780 | 3,180 |
| 1/4 | 1.250 | . 250.2435 | . 424.423 | 5,070 | 5,790 |
| 5/16 | 1.500 | . 3125.3053 | . 539.538 | 8,350 | 9,250 |
| 3/8 | 1.750 | . 375.3678 | . 653.652 | 12,400 | 14,000 |
| 7/16 | 2.000 | . 4375.4294 | . 690.689 | 16,900 | 18,900 |
| 1/2 | 2.250 | . 500.4919 | . 739.738 | 22,800 | 25,600 |
| 5/8 | 2.500 | . 625.6163 | . 962.961 | 36,000 | 40,800 |
| 3/4 | 3.000 | . 750.7406 | 1.1861 .185 | 53,200 | 59,300 |
| 7/8 | 3.250 | . 875.8647 | 1.4111 .410 | 73,500 | 81,000 |
| 1 | 3.750 | 1.000 .9886 | 1.6351 .634 | 96,300 | 106,000 |

GENERAL NOTE: Flat, countersunk head cap screws and button head cap screws are designed and recommended for moderate fastening applications: machine guards, hinges, covers, etc. They are not suggested for use in critical high load strength applications where socket head cap screws should be used.

## Maximum Lengths

- LG is the maximum grip length and is the distance from the bearing surface to the first complete thread.


| Thread <br> Size | $3 / 4$ | $7 / 8$ | 1 | $11 / 4$ | $11 / 2$ | $13 / 4$ | 2 | $21 / 4$ | $21 / 2$ | $23 / 4$ | 3 | $31 / 4$ | $31 / 2$ | $33 / 4$ | 4 |  | $41 / 4$ | $41 / 2$ | $43 / 4$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | 0.25 | 0.25 | 0.50 | 0.75 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| Size | Part No. | lbs. <br> $/ 1000$ |  |
| ---: | :---: | :---: | :---: |
| $\# 4-40$ UNC - Key Size $1 / 16^{\prime \prime}$ |  |  |  |
| $\# 4 \times 1 / 4$ | 104414 | 100 | 0.84 |
| $3 / 8$ | 104447 | 100 | 1.10 |
| $1 / 2$ | 104480 | 100 | 1.36 |
| $5 / 8$ | 103424 | 100 | 1.61 |
| $3 / 4$ | 103457 | 100 | 1.89 |

\#5-40 UNC - Key Size 5/64"

| $\# 5 \times 1 / 4$ | 121026 | 100 | 1.06 |
| ---: | ---: | ---: | ---: |
| $3 / 8$ | 107506 | 100 | 1.39 |
| $1 / 2$ | 107615 | 100 | 1.74 |
| $5 / 8$ | 113269 | 100 | 1.94 |
| $3 / 4$ | 119592 | 100 | 2.40 |


| \#6-32 UNC - Key Size 5/64" |  |  |  |
| ---: | ---: | ---: | ---: |
| \#6 x 1/4 | 119626 | 100 | 1.32 |
| $3 / 8$ | 119658 | 100 | 1.72 |
| $1 / 2$ | 119691 | 100 | 2.13 |
| $5 / 8$ | 119725 | 100 | 2.51 |
| $3 / 4$ | 119759 | 100 | 2.93 |
| 1 | 105351 | 100 | 3.37 |


| \#8-32 UNC - Key Size 3/32" |  |  |  |
| ---: | ---: | ---: | ---: |
| $\# 8 \times 3 / 8$ | 106645 | 100 | 2.60 |
| $1 / 2$ | 106677 | 100 | 3.19 |
| $5 / 8$ | 106709 | 100 | 3.78 |
| $3 / 4$ | 106741 | 100 | 4.38 |
| 1 | 106773 | 100 | 5.59 |


| $\# 10-24$ UNC - Key Size $1 / 8^{\prime \prime}$ |  |  |  |
| ---: | :---: | :---: | ---: |
| $\# 10 \times 3 / 8$ | 106805 | 100 | 3.43 |
| $1 / 2$ | 113654 | 100 | 4.20 |
| $5 / 8$ | 113687 | 100 | 4.97 |
| $3 / 4$ | 113719 | 100 | 5.74 |
| 1 | 120686 | 100 | 7.26 |
| $11 / 4$ | 118712 | 100 | 8.80 |
| $11 / 2$ | 108955 | 100 | 11.62 |
| $\# 10-32$ UNF- Key Size $1 / 8^{\prime \prime}$ |  |  |  |
| $\# 10 \times 3 / 8$ | 111890 | 100 | 3.59 |
| $1 / 2$ | 111889 | 100 | 4.42 |
| $5 / 8$ | 113158 | 100 | 5.26 |
| $3 / 4$ | 107655 | 100 | 6.09 |
| 1 | 107671 | 100 | 7.77 |
| $11 / 4$ | 107687 | 100 | 9.44 |
| $11 / 2$ | 111818 | 100 | 12.03 |


| 1/4-20 UNC - Key Size 5/32" |  |  |  | $21 / 4$ | 109890 | 50 | 73.17 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $1 / 4 \times 3 / 8$ | 105257 | 100 | 6.93 | $21 / 2$ | 103706 | 50 | 80.61 |
| 1/2 | 105289 | 100 | 8.32 | 3 | 104929 | 50 | 96.73 |
| 5/8 | 105321 | 100 | 9.70 |  |  |  |  |


| Size | Part No. | lbs. <br> /1000 |  |
| ---: | :---: | :---: | :---: |
| $1 / 4-20$ UNC - Key Size $5 / 32^{\prime \prime}$ |  |  |  |
| $1 / 4 \times 3 / 4$ | 105352 | 100 | 11.09 |
| 1 | 118658 | 100 | 13.86 |
| $11 / 4$ | 120514 | 100 | 16.63 |
| $11 / 2$ | 120581 | 100 | 19.40 |
| $13 / 4$ | 120645 | 100 | 23.21 |
| 2 | 118672 | 100 | 27.26 |

1/4-28 UNF - Key Size 5/32"

| $1 / 4 \times 3 / 8$ | 111834 | 100 | 7.19 |
| ---: | ---: | ---: | ---: |
| $1 / 2$ | 108107 | 100 | 8.71 |
| $5 / 8$ | 104289 | 100 | 10.21 |
| $3 / 4$ | 104322 | 100 | 11.73 |
| 1 | 104356 | 100 | 14.72 |
| $11 / 4$ | 115174 | 100 | 17.73 |
| $11 / 2$ | 107581 | 100 | 20.75 |


| $5 / 16-18$ UNC - Key Size 3/16" |  |  |  |
| ---: | ---: | :--- | ---: |
| $5 / 16 \times 1 / 2$ | 120341 | 100 | 14.23 |
| $5 / 8$ | 119485 | 100 | 16.41 |
| $3 / 4$ | 119517 | 100 | 18.59 |
| $7 / 8$ | 106770 | 100 | 19.51 |
| 1 | 105918 | 100 | 22.95 |
| $11 / 4$ | 105951 | 100 | 27.32 |
| $11 / 2$ | 105983 | 100 | 31.68 |
| $13 / 4$ | 106015 | 100 | 36.04 |
| 2 | 106046 | 100 | 44.73 |
| $21 / 4$ | 106079 | 100 | 47.76 |
| $21 / 2$ | 117115 | 100 | 50.80 |

5/16-24 UNF - Key Size 3/16"

| $5 / 16 \times 1 / 2$ | 114970 | 100 | 14.83 |
| ---: | ---: | ---: | ---: |
| $5 / 8$ | 103930 | 100 | 17.20 |
| $3 / 4$ | 103326 | 100 | 18.59 |
| 1 | 115218 | 100 | 24.35 |
| $11 / 4$ | 115282 | 100 | 29.13 |
| $11 / 2$ | 115345 | 100 | 33.90 |

3/8-16 UNC - Key Size 7/32"

| $3 / 8 \times 1 / 2$ | 117147 | 100 | 22.40 |
| ---: | ---: | ---: | ---: |
| $5 / 8$ | 117179 | 100 | 23.85 |


| $3 / 4$ | 107104 | 100 | 28.91 |
| :--- | :--- | :--- | :--- |
| $7 / 8$ | 118253 | 100 | 32.12 |


| $7 / 8$ | 118253 | 100 | 32.12 |
| ---: | ---: | ---: | ---: |
| 1 | 107136 | 100 | 35.40 |


| $11 / 4$ | 104272 | 100 | 41.80 |
| ---: | ---: | ---: | ---: |
| $11 / 2$ | 104338 | 100 | 48.38 |
| $13 / 4$ | 110464 | 100 | 54.87 |
| 2 | 108160 | 100 | 65.74 |
| $21 / 4$ | 109890 | 50 | 73.17 |
| $21 / 2$ | 103706 | 50 | 80.61 |
| 3 | 104929 | 50 | 96.73 |

Size Part No. $\quad$| lbs. |
| :---: |
| $/ 1000$ |

| $3 / 8-24$ UNF - Key Size 7/32" |  |  |  |
| ---: | ---: | ---: | ---: |
| $3 / 8 \times 5 / 8$ | 115416 | 100 | 23.85 |
| $3 / 4$ | 103388 | 100 | 30.32 |
| 1 | 103420 | 100 | 37.40 |
| $11 / 4$ | 106866 | 100 | 44.48 |
| $11 / 2$ | 106896 | 100 | 51.57 |

7/16-14 UNC - Key Size 7/32"

| $7 / 16 \times 3 / 4$ | 104993 | 100 | 35.22 |
| ---: | ---: | ---: | ---: |
| 1 | 116833 | 100 | 43.63 |
| $11 / 4$ | 116897 | 50 | 35.42 |
| $11 / 2$ | 102033 | 50 | 63.40 |
| $13 / 4$ | 105097 | 50 | 68.86 |
| 2 | 116228 | 50 | 72.47 |

1/2-13 UNC- Key Size 5/16"

| $1 / 2 \times 3 / 4$ | 115671 | 100 | 45.06 |
| ---: | ---: | ---: | ---: |
| 1 | 102630 | 100 | 60.85 |
| $11 / 4$ | 107321 | 50 | 72.71 |
| $11 / 2$ | 107353 | 50 | 84.57 |
| $13 / 4$ | 120801 | 50 | 96.40 |
| 2 | 106977 | 50 | 108.26 |
| $21 / 4$ | 106992 | 50 | 112.11 |
| $21 / 2$ | 107007 | 25 | 142.16 |
| 3 | 107038 | 25 | 165.88 |
| $1 / 2-20$ UNF- Key Size $5 / 16^{\prime \prime}$ |  |  |  |
| $1 / 2 \times 3 / 4$ | 106925 | 100 | 51.19 |
| 1 | 106955 | 100 | 64.00 |
| $11 / 4$ | 106985 | 50 | 76.78 |
| $11 / 2$ | 107015 | 50 | 89.58 |
| $13 / 4$ | 107046 | 50 | 102.37 |
| 2 | 107076 | 50 | 115.17 |


| $5 / 8-11$ UNC - Key Size 3/8" |  |  |  |
| ---: | ---: | ---: | ---: |
| $5 / 8 \times 11 / 4$ | 107053 | 25 | 122.94 |
| $11 / 2$ | 107923 | 25 | 141.70 |
| $13 / 4$ | 120818 | 25 | 160.45 |
| 2 | 107955 | 25 | 179.21 |
| $21 / 4$ | 107971 | 25 | 197.96 |
| $21 / 2$ | 107989 | 25 | 208.53 |
| 3 | 120848 | 25 | 254.21 |
| $3 / 4-10$ UNC - Key Size 1/2" |  |  |  |
| $3 / 4 \times 11 / 4$ | 102419 | 25 | 262.37 |
| $11 / 2$ | 102436 | 25 | 219.14 |
| $13 / 4$ | 102453 | 25 | 226.03 |
| 2 | 102469 | 25 | 251.50 |
| $21 / 4$ | 102486 | 25 | 283.49 |
| $21 / 2$ | 102502 | 25 | 329.01 |
| 3 | 102535 | 25 | 383.94 |
| 4 | 701531 | 25 | 475.20 |



## BUTITON HEAD CAP SCREWS

Unbrako button head screws are ideally suited for use in materials too thin to countersink and in non-critical loading applications. Their low head profile gives them smooth, aesthetic appearance, and their deep accurate sockets ensure non-slip wrench engagement to prevent marring of the surface in which they are installed.

Unbrako button head screws are made from high grade alloy steel and every manufacturing operation is closely controlled. Heads are forged for greater strength and full formed radius-root rolled threads assure close tolerances, maximum strength and superior fatigue resistance. Deep accurate sockets allow full tightening, and customized heat treatment of each heat of steel ensures maximum strength and hardness without brittleness.

## FEATURES \& BENEFITS



## GENERAL NOTE

Flat, countersunk head cap screws and button head cap screws are designed and recommended for moderate fastening applications: machine guards, hinges, covers, etc. These are not suggested for use in critical high strength applications where socket head cap screws should be used.


Low head streamline design. Use them in materials too thin to countersink; also for non-critical loading requiring heat treated screws

## Equivalent Standards

ISO 7380, ASME B18.3.4M, BS 4168-4

## Mechanical Properties

1. Material: ASTM F835M, EN ISO 898-1
2. Dimensions: B18.3.4M
3. Property Class: 12.9
4. Hardness: Rc 39-44
5. Tensile Stress: 1040 MPa
6. Shear Stress: 630 Mpa
7. Yield Stress: 945 Mpa
8. Working temperature: $-50^{\circ} \mathrm{C}$ to $+300^{\circ} \mathrm{C}$
9. Bearing surface: To be square with body within $2^{\circ}$.
10. Thread Class: 4 g 6 g
11. Min Elongation 9\%
12. Length Tolrence $+/-0.25 \mathrm{MM}$
13. Torques Calculated In Accordance With VDI 2230

## Head Marking



Head markings may vary slightly depending on manufacturing practice. UNBRAKO, and UNB are recognized identifications for M5 diameter \& larger.


Product Dimensions


| Recommended Tightening Torque |  |  |  | Tensile Load kN |
| :---: | :---: | :---: | :---: | :---: |
| Unplated |  | Plated |  |  |
| Nm | Ibf.in | Nm | Ibf.in |  |
| 1.4 | 12 | 1.1 | 9 | 5.28 |
| 3.4 | 30 | 2.6 | 22 | 9.22 |
| 6.8 | 60 | 5.1 | 45 | 14.90 |
| 11.0 | 97 | 8.3 | 73 | 21.10 |
| 28.0 | 248 | 21.0 | 186 | 38.40 |
| 55.0 | 486 | 41.0 | 363 | 60.90 |
| 95.0 | 840 | 71.0 | 630 | 88.50 |

General Note: Flat, countersunk head cap screws and button head cap screws are designed and recommended for moderate fastening applications: machine guards, hinges, covers, etc. They are not suggested for use in critical high strength applications where socket head cap screws should be used. Also due to their head configuration they may not meet the minimum ultimate tensile requirements for property class 12.9 as specified in EN ISO 898-1. They are nevertheless required to meet the other material and property requirements for property class 12.9.

## Black / Plain

| Size | Part No. | $\checkmark$ | $\begin{aligned} & \text { lbs. } \\ & \text { /1000 } \end{aligned}$ | Size | Part No. | $\square$ | $\begin{aligned} & \text { lbs. } \\ & \text { /1000 } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M3 (0.5) - Key Size 2mm |  |  |  | M8 (1.25) - Key Size 5mm |  |  |  |
| M3 $\times 5$ | 180248 | 200 | 0.97 | M8 $\times 30$ | 106386 | 200 | 28.73 |
| 6 | 106353 | 200 | 1.06 | 35 | 106389 | 200 | 32.23 |
| 8 | 106354 | 200 | 1.25 | 40 | 106390 | 200 | 35.73 |
| 10 | 106357 | 200 | 1.45 |  |  |  |  |
| 12 | 106358 | 200 | 1.65 | M10 (1.5) - Key Size 6mm |  |  |  |
| 16 | 106359 | 200 | 2.02 | M10 $\times 16$ | 106392 | 200 | 32.82 |
|  |  |  |  | 20 | 106393 | 200 | 37.25 |
| M4 (0.7) - Key Size 2.5 mm |  |  |  | 25 | 106396 | 200 | 42.75 |
| M4 $\times 6$ | 180200 | 200 | 2.16 | 30 | 106399 | 200 | 48.27 |
| 8 | 106360 | 200 | 2.49 | 35 | 106401 | 200 | 53.79 |
| 10 | 106361 | 200 | 2.84 | 40 | 106402 | 100 | 59.29 |
| 12 | 106363 | 200 | 3.17 |  |  |  |  |
| 15 | 401218 | 200 | 3.67 | M12 (1.75) - Key Size 8mm |  |  |  |
| 16 | 106364 | 200 | 3.85 | M12 $\times 16$ | 106403 | 100 | 52.47 |
|  |  |  |  | 20 | 106404 | 100 | 58.85 |
| M5 (0.8) - Key Size 3mm |  |  |  | 25 | 106405 | 100 | 66.84 |
| M5 x 6 | 180398 | 200 | 3.83 | 30 | 106406 | 100 | 74.84 |
| 8 | 180175 | 200 | 4.38 | 35 | 106407 | 100 | 82.83 |
| 10 | 106365 | 200 | 4.93 | 40 | 106408 | 50 | 84.66 |
| 12 | 106366 | 200 | 5.48 | 50 | 106413 | 50 | 106.79 |
| 15 | 401219 | 200 | 6.29 | Note: <br> - All button head socket screws are supplied with full thread. |  |  |  |
| 16 | 106367 | 200 | 6.56 |  |  |  |  |
| 18 | 406269 | 200 | 7.11 |  |  |  |  |
| 20 | 106368 | 200 | 7.63 |  |  |  |  |
| 22 | 401220 | 200 | 8.18 |  |  |  |  |
| 25 | 106369 | 200 | 9.00 |  |  |  |  |
| 30 | 106370 | 200 | 10.36 |  |  |  |  |


| M6 (1) - Key Size 4mm |  |  |  |
| ---: | :---: | :---: | ---: |
| M6 x 8 | 180249 | 200 | 5.74 |
| 10 | 106372 | 200 | 7.15 |
| 12 | 106373 | 200 | 7.92 |
| 15 | 401222 | 200 | 9.09 |
| 16 | 106374 | 200 | 9.48 |
| 18 | 401223 | 200 | 10.25 |
| 20 | 106375 | 200 | 11.02 |
| 25 | 106376 | 200 | 12.96 |
| 30 | 106378 | 200 | 14.92 |


| M8 (1.25) |  |  |  |
| ---: | :---: | :---: | :---: |
| Mey Size 5mm |  |  |  |
| M8 $\times 10$ | 106379 | 200 | 14.74 |
| 12 | 106380 | 200 | 16.13 |
| 15 | 401226 | 200 | 18.24 |
| 16 | 106382 | 200 | 18.94 |
| 20 | 106384 | 200 | 21.74 |
| 25 | 106385 | 200 | 25.23 |



Low heads streamline design. Use them in materials too thin to countersink; also for non-critical loading requiring heat treated screws

Equivalent Standard
ASME B18.3, BS 2470
Mechanical Properties
Material: Unbrako High Grade Alloy Steel Thread Class: 3A
Max working temperature: $-50^{\circ} \mathrm{C}$ to $+300^{\circ} \mathrm{C}$
Heat Treatment: Rc 39-44
Shear Strength: 96,000 Ibf/in2
Min. Elongation: 9\%

## Length Tolerance

| Diameter | to 1" <br> Incl. | over 1" <br> to 2" Incl. |
| :--- | :---: | :---: |
| To 1"incl. | -.03 | -.04 |
| Over 1"to 2" | -.03 | -.06 |

## Maximum Tightening Torques

Thread size Unplated Plated

| nom. | UNF | UNC | UNF | UNC |
| :---: | :---: | :---: | :---: | :---: |
|  | Maximum Tightening Torques (lbf. in.) |  |  |  |
| \#4 | 8.9 | 10 | 6.6 | 7.5 |
| \#5 | 13.0 | 14 | 9.7 | 10.0 |
| \#6 | 16.0 | 19 | 12.0 | 14.0 |
| \#8 | 30.0 | 32 | 22.0 | 24.0 |
| \#10 | 44.0 | 51 | 33.0 | 38.0 |
| 1/4 | 100.0 | 120 | 75.0 | 90.0 |
| 5/16 | 210.0 | 240 | 157.0 | 180.0 |
|  | Maximum Tightening Torques (lbf. ft.) |  |  |  |
| 3/8 | 380.0 | 430 | 285.0 | 322.0 |
| 7/16 | 600.0 | 680 | 450.0 | 510.0 |
| 1/2 | 930.0 | 1050 | 697.0 | 787.0 |
| 5/8 | 1800.0 | 2000 | 1350.0 | 1500.0 |
| 3/4 | 3200.0 | 3560 | 240 | 670.0 |

Head Marking


Head markings may vary slightly depending on manufacturing practice. UNBRAKO and UNB are recognized identifications for \#10 diameter \& larger.

Product Dimensions

| Thread size nom. | Threads per Inch |  | Head Diameter A |  | Hex Socket Size W min. | Head Height H |  | Socket <br> Depth T min |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | UNC | UNF | max | min |  | max | min |  |
| \#0 | - | 80 | . 114 | . 104 | . 035 | . 032 | . 026 | . 020 |
| \#1 | 64 | 72 | . 139 | . 129 | . 050 | . 039 | . 033 | . 028 |
| \#2 | 56 | 64 | . 164 | . 154 | . 050 | . 046 | . 038 | . 028 |
| \#3 | 48 | 56 | . 188 | . 176 | . 0625 | . 052 | . 044 | . 035 |
| \#4 | 40 | 48 | . 213 | . 201 | . 0625 | . 059 | . 051 | . 035 |
| \#5 | 40 | 44 | . 238 | . 226 | . 0781 | . 066 | . 058 | . 044 |
| \#6 | 32 | 40 | . 262 | . 250 | . 0781 | . 073 | . 063 | . 044 |
| \#8 | 32 | 36 | . 312 | . 298 | . 0937 | . 087 | . 077 | . 052 |
| \#10 | 24 | 32 | . 361 | . 347 | . 1250 | . 101 | . 091 | . 070 |
| 1/4 | 20 | 28 | . 437 | . 419 | . 1562 | . 132 | . 122 | . 087 |
| 5/16 | 18 | 24 | . 547 | . 527 | . 1875 | . 166 | . 152 | . 105 |
| 3/8 | 16 | 24 | . 656 | . 636 | . 2187 | . 199 | . 185 | . 122 |
| 7/16 | 14 | 20 | . 750 | . 730 | . 2500 | . 232 | . 212 | . 138 |
| 1/2 | 13 | 20 | . 875 | . 851 | . 3125 | . 265 | . 245 | . 175 |
| 5/8 | 11 | 18 | 1.000 | . 970 | . 3750 | . 331 | . 311 | . 210 |
| 3/4 | 10 | 16 | 1.218 | 1.198 | . 5000 | . 398 | . 378 | . 272 |


| Thread size nom. | thd. to hd max ref | Body Dia B |  | Transition Dia. |  |  | Tensile Load lbs. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | max | min | max | max | ref | UNC | UNF |
| \#0 | . 500 | . 060 | . 0568 | . 010 | . 080 | . 070 |  |  |
| \#1 | . 500 | . 073 | . 0695 | . 010 | . 093 | . 080 |  |  |
| \#2 | . 500 | . 086 | . 0822 | . 010 | . 106 | . 099 |  |  |
| \#3 | . 500 | . 099 | . 0949 | . 010 | . 119 | . 110 |  |  |
| \#4 | . 500 | . 112 | . 1075 | . 015 | . 132 | . 135 | 960 | 1,040 |
| \#5 | . 500 | . 125 | . 1202 | . 015 | . 145 | . 141 | 1,260 | 1,310 |
| \#6 | . 625 | . 138 | . 1329 | . 015 | . 158 | . 158 | 1,440 | 1,620 |
| \#8 | . 750 | . 164 | . 1585 | . 015 | . 194 | . 185 | 2,220 | 2,240 |
| \#10 | 1.000 | . 190 | . 1840 | . 020 | . 220 | . 213 | 2,780 | 3,180 |
| 1/4 | 1.000 | . 250 | . 2435 | . 031 | . 290 | . 249 | 5,070 | 5,790 |
| 5/16 | 1.000 | . 3125 | . 3053 | . 031 | . 353 | . 309 | 8,350 | 9,250 |
| 3/8 | 1.250 | . 375 | . 3678 | . 031 | . 415 | . 368 | 12,400 | 14,000 |
| 7/16 | 1.500 | . 437 | . 4294 | 0.31 | . 478 | . 417 | 16,900 | 18,900 |
| 1/2 | 2.000 | . 500 | . 4919 | . 046 | . 560 | . 481 | 22,800 | 25,600 |
| 5/8 | 2.000 | . 625 | . 6163 | . 062 | . 685 | . 523 | 36,000 | 40,800 |
| 3/4 | 2.000 | . 750 | . 7406 | 0.78 | . 810 | . 670 | 53,200 | 59,300 |

N.B. Because of their head configurations, Button head screw tensile loads,
are based on $160,000 \mathrm{lbf} / \mathrm{in} 2$.

| Size | Part No. | Ibs. <br> /1000 |  |
| ---: | :---: | :---: | :---: |
| \#4-40 UNC - Key Size $1 / 16^{\prime \prime}$ |  |  |  |
| \#4× $1 / 4$ | 104704 | 100 |  |
| $5 / 16$ | 107146 | 100 |  |
| $3 / 8$ | 104720 | 100 |  |
| $1 / 2$ | 104736 | 100 |  |
| \#6-32 UNC - Key Size $5 / 64^{\prime \prime}$ |  |  |  |
| \#6 x 1/4 | 104752 | 100 |  |
| $5 / 16$ | 105496 | 100 |  |
| $3 / 8$ | 104768 | 100 |  |
| $1 / 2$ | 104784 | 100 |  |
| $5 / 8$ | 104800 | 100 |  |
| 1 | 106565 | 100 |  |


| Size | Part No. | 5 | $\begin{aligned} & \text { lbs. } \\ & \text { /1000 } \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| 1/4-28 UNF - Key Size 5/32" |  |  |  |
| $1 / 4 \times 1 / 4$ | 114974 | 100 | 5.96 |
| 3/8 | 118664 | 100 | 7.37 |
| 1/2 | 120494 | 100 | 8.78 |
| 5/8 | 120527 | 100 | 10.19 |
| 3/4 | 120561 | 100 | 11.59 |
| 7/8 | 120593 | 100 | 13.00 |
| 1 | 120625 | 100 | 14.41 |


| Size | Part No. | Ibs. <br> $/ 1000$ |
| :---: | :---: | :---: | :---: |


| $1 / 2-20$ UNF - Key Size 5/16" |  |  |  |
| ---: | :---: | :---: | :---: |
| $1 / 2 \times 1$ | 108196 | 100 | 73.83 |
| $5 / 8-11$ |  |  |  |
| $5 / 8 \times 1$ | $1 / 4$ | 111802 | 25 |
| $11 / 2$ | 111819 | 25 | 148.83 |
| 2 | 111906 | 25 | 184.25 |

## Note:

- All button head socket screws are supplied with full thread.

| \#8-32 UNC - Key Size 3/32" |  |  |  |
| ---: | ---: | ---: | ---: |
| \#8 x 1/4 | 116546 | 100 | 2.44 |
| $3 / 8$ | 116562 | 100 | 2.99 |
| $1 / 2$ | 116579 | 100 | 3.56 |
| $5 / 8$ | 116595 | 100 | 4.00 |
| $3 / 4$ | 116611 | 100 | 4.69 |


| \#10-24 UNC - Key Size 1/8" |  |  |  |
| ---: | ---: | ---: | ---: |
| $\# 10 \times 1 / 4$ | 116932 | 100 | 3.34 |
| $3 / 8$ | 116948 | 100 | 3.89 |
| $1 / 2$ | 116964 | 100 | 4.80 |
| $5 / 8$ | 109705 | 100 | 5.50 |
| $3 / 4$ | 109722 | 100 | 6.25 |
| $7 / 8$ | 103523 | 100 | 6.84 |
| 1 | 103539 | 100 | 7.72 |


| \#10-32 UNF - Key Size 1/8" |  |  |  |
| ---: | :---: | :---: | :---: |
| $\# 10 \times 1 / 4$ | 105400 | 100 | 3.48 |
| $3 / 8$ | 102042 | 100 | 4.27 |
| $1 / 2$ | 102058 | 100 | 5.06 |
| $5 / 8$ | 120709 | 100 | 5.85 |
| $3 / 4$ | 120725 | 100 | 6.47 |
| $7 / 8$ | 120741 | 100 | 7.22 |
| 1 | 118647 | 100 | 8.23 |


| $3 / 8-16$ UNC - Key Size 7/32" |  |  |  |
| ---: | ---: | ---: | ---: |
| $3 / 8 \times 1 / 2$ | 104056 | 100 | 23.41 |
| $5 / 8$ | 104072 | 100 | 26.49 |
| $3 / 4$ | 108180 | 100 | 29.57 |
| $7 / 8$ | 108197 | 100 | 32.65 |
| 1 | 108213 | 100 | 35.73 |
| $11 / 4$ | 108229 | 100 | 41.91 |
| $11 / 2$ | 113752 | 100 | 48.07 |
| 2 | 701845 | 100 | 60.41 |


| 3/8-24 UNF - Key Size 7/32" |  |  |  |
| ---: | ---: | ---: | ---: |
| $3 / 8 \times 1 / 2$ | 120353 | 100 | 24.42 |
| $3 / 4$ | 119491 | 100 | 31.06 |
| 1 | 119523 | 100 | 37.73 |
| $11 / 4$ | 183934 | 100 | 41.91 |


| $1 / 4 \times 3 / 8$ | 103556 | 100 | 7.04 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/2 | 110416 | 100 | 8.34 | 1/2-13 UNC - Key Size 5/16" |  |  |  |
| 5/8 | 104174 | 100 | 9.64 | 1/2 $\times 3 / 4$ | 106017 | 100 | 59.20 |
| 3/4 | 104191 | 100 | 10.93 | 1 | 111721 | 50 | 70.38 |
| 7/8 | 104209 | 100 | 12.25 | $11 / 4$ | 111737 | 50 | 81.55 |
| 1 | 103943 | 100 | 13.55 | $11 / 2$ | 111753 | 50 | 92.40 |
| $11 / 4$ | 120415 | 100 | 16.15 | 2 | 111769 | 50 | 115.08 |

## FLANGE <br> BUTTON HEAD CAP SCREWS

Unbrako flange button head screws allow the covering of large diameter holes in sheet metal. As the large under head surface pressure by area is low, this fastener can also be used with softer materials without harm or damage. Flange button heads are ideal to fix strips, cover plates and sheet metal housings.

The radius on the button head presents a streamlined profile, virtually eliminating the sharp edges which could occur with a bolt and washer assembly.

Unbrako flange button head screws are available with metric threads and are made from high grade alloy steel.


## FEATURES \& BENEFITS

Precision forged head for continuous grain flow and maximum strength

Deep, accurate socket for uniform wrenching power and high maximum torques.

Heat treated in a controlled atmosphere for maximum uniform strength and surface integrity without brittleness or decarburisation



Allow covering of large diameter holes in sheet metal. Ideal to fix strips, cover plates and sheet metal housings.

## Mechanical Properties

Material: Unbrako High Grade Alloy Steel Heat Treatment: Rc 39-44

## Notes

1. Thread Class: 4 g 6 g
2. Full thread length to within $21 / 2$ pitches of head.
3. Working Temperature: $-50^{\circ} \mathrm{C}+300^{\circ} \mathrm{C}$
4. Length tolerance $= \pm 0.25 \mathrm{~mm}$.
5. Torques calculated in accordance with VDI 2230 "Systematic calculation of high duty bolted joints with $\sigma 0.2=720 \mathrm{~N} / \mathrm{mm}^{2}$ and $\mu=0.125$ for plain finish.

## Length Tolerance

|  |  |  |
| :---: | :---: | :---: |
| Screws Over | Up to and <br> including | Tolerance |
| - | $1^{\prime \prime}$ | $\pm 0.16^{\prime \prime}$ |
| $1^{\prime \prime}$ | $2^{\prime \prime}$ | $+0.031 "-0.016^{\prime \prime}$ |
| $2^{\prime \prime}$ | $6^{\prime \prime}$ | $\pm 0.031^{\prime \prime}$ |
| $6^{\prime \prime}$ | - | $\pm 0.062^{\prime \prime}$ |



Product Dimensions


| Thread Size nom. | Recommended |  |  |
| :---: | :---: | :---: | :---: |
|  | Tightening Torques Unplated |  | Tensile Loads kN |
|  |  |  |  |
|  | N-m | Ibf.in |  |
| M3 | 1.96 | 18 | 5.23 |
| M4 | 4.52 | 40 | 9.13 |
| M5 | 9.08 | 80 | 14.77 |
| M6 | 15.40 | 138 | 20.90 |
| M8 | 36.80 | 330 | 38.06 |
| M10 | 72.30 | 650 | 60.32 |
| M12 | 126.00 | 1134 | 87.67 |

Unorako


Allow covering of large diameter holes in sheet metal. Ideal to fix strips, cover plates and sheet metal housings.

\section*{Mechanical Properties <br> Heat Treatment: 40-43 HRC <br> Thread Class: 3A <br> Length Tolerance <br> | Up to 1" | -0.03 |
| :--- | :--- |
| Over 1" to 2 1/2" | -0.04 |
| Over 2 1/2" | -0.06 |}

## Notes

*Thread Length: Screw lengths equal to or shorter than listed in column 'L' will be threaded to head

## Head Marking



Head markings may vary slightly depending on manufacturing practice. UNBRAKO and UNB are recognized identifications for $1 / 4^{\prime \prime}$ diameter \& larger.


Product Dimensions

| Thread <br> Size | Threads <br> per Inch | Head <br> Diameter | Hex <br> Socket Size <br> W | Head <br> Height <br> H | Socket <br> Depth |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| nom. | UNC UNF |  |  |  |  |  |  |  |  | max | max | min | max | min. |
| $\# 4$ | 40 | 48 | 0.240 | 0.0635 | 0.0625 | 0.059 | 0.035 |  |  |  |  |  |  |  |
| $\# 6$ | 32 | 40 | 0.292 | 0.0791 | 0.0781 | 0.073 | 0.044 |  |  |  |  |  |  |  |
| $\# 8$ | 32 | 36 | 0.357 | 0.0952 | 0.0937 | 0.087 | 0.052 |  |  |  |  |  |  |  |
| $\# 10$ | 24 | 32 | 0.407 | 0.1270 | 0.1250 | 0.101 | 0.070 |  |  |  |  |  |  |  |
| $1 / 4$ | 20 | 28 | 0.560 | 0.1587 | 0.1562 | 0.132 | 0.087 |  |  |  |  |  |  |  |
| $5 / 16$ | 18 | 24 | 0.680 | 0.1900 | 0.1875 | 0.166 | 0.105 |  |  |  |  |  |  |  |
| $3 / 8$ | 16 | 24 | 0.810 | 0.2217 | 0.2187 | 0.199 | 0.122 |  |  |  |  |  |  |  |
| $1 / 2$ | 13 | 20 | 1.070 | 0.3160 | 0.3125 | 0.265 | 0.175 |  |  |  |  |  |  |  |


| Thread Size | Bearing Face |  |  | Fillet Extension | Thread Length* |
| :---: | :---: | :---: | :---: | :---: | :---: |
| nom. | D $\min$ | $\underset{\max }{\mathrm{Q}}$ | R nom | $\underset{\max }{S}$ | L min |
| \#4 | 0.203 | 0.025 | 0.140 | 0.010 | 0.500 |
| \#6 | 0.252 | 0.028 | 0.163 | 0.010 | 0.625 |
| \#8 | 0.312 | 0.031 | 0.190 | 0.015 | 0.750 |
| \#10 | 0.357 | 0.036 | 0.218 | 0.015 | 1.000 |
| 1/4 | 0.496 | 0.046 | 0.254 | 0.020 | 1.000 |
| 5/16 | 0.603 | 0.058 | 0.314 | 0.020 | 1.000 |
| 3/8 | 0.721 | 0.069 | 0.373 | 0.020 | 1.250 |
| 1/2 | 0.960 | 0.094 | 0.486 | 0.030 | 2.000 |


| Size | Part No. | $\square$ | $\begin{aligned} & \text { lbs } \\ & \text { /1000 } \end{aligned}$ | Size | Part No. | $\square$ | $\begin{gathered} \text { lbs } \\ \text { /1000 } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M3 (0.5) - Key Size 2mm |  |  |  | M6 (1) - Key Size 4mm |  |  |  |
| M $3 \times 6$ | 404977 | 200 | 1.23 | M6 x 25 | 405003 | 200 | 14.17 |
|  |  |  |  | 30 | 405004 | 200 | 16.13 |
| M4 (0.7) - Key Size 2.5mm |  |  |  |  |  |  |  |
| M $4 \times 8$ | 404982 | 200 | 2.79 | M8 (1.25) - Key Size 5mm |  |  |  |
| 10 | 404983 | 200 | 3.15 | M8× 10 | 405005 | 200 | 16.37 |
| 12 | 404984 | 200 | 3.48 | 12 | 405007 | 200 | 17.78 |
| 16 | 404986 | 200 | 4.16 | 16 | 405009 | 200 | 20.57 |
|  |  |  |  | 20 | 405011 | 200 | 23.36 |
| M5 (0.8) - Key Size 3mm |  |  |  | 25 | 405012 | 200 | 26.86 |
| M5 $\times 10$ | 404988 | 200 | 5.41 | 30 | 405013 | 200 | 30.36 |
| 12 | 404989 | 200 | 5.96 | 40 | 405015 | 200 | 37.36 |
| 16 | 404991 | 200 | 7.04 |  |  |  |  |
| 20 | 404992 | 200 | 8.12 | M10 (1.5) - Key Size 6mm |  |  |  |
| 25 | 404994 | 200 | 9.48 | M10 $\times 16$ | 405016 | 200 | 35.82 |
|  |  |  |  | 20 | 405017 | 200 | 40.24 |
| M6 (1) - Key Size 4mm |  |  |  | 25 | 405018 | 200 | 45.76 |
| M6 $\times 10$ | 180079 | 200 | 8.36 | 30 | 405019 | 200 | 51.26 |
| 12 | 404997 | 200 | 9.13 |  |  |  |  |
| 16 | 404999 | 200 | 10.69 |  |  |  |  |
| 20 | 405001 | 200 | 12.23 |  |  |  |  |

## Flange Button Head Socket Screw - Inch

(0)

| Size | Part No. | $\$$ | $\begin{aligned} & \text { lbs } \\ & \text { /1000 } \end{aligned}$ | Size | Part No. | $\square$ | $\begin{aligned} & \text { lbs } \\ & \text { /1000 } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \#8-32 UNC - Key Size 3/32" |  |  |  | 1/4-20 UNC - Key Size 5/32" |  |  |  |
| \#8 x 1/4 | 116376 | 100 | 3.04 | $1 / 4^{\prime \prime} \times 3 / 8$ | 116406 | 100 | 9.46 |
| 3/8 | 116379 | 100 | 3.61 | 1/2 | 116408 | 100 | 10.76 |
| 1/2 | 116381 | 100 | 4.18 | 3/4 | 116413 | 100 | 13.35 |
|  |  |  |  | 1 | 116418 | 100 | 15.97 |
| \#10-24 UNC - Key Size 1/8" |  |  |  |  |  |  |  |
| \#10 x 3/8 | 116391 | 100 | 4.86 | 5/16-18 UNC - Key Size 3/16" |  |  |  |
| 1/2 | 116393 | 100 | 5.59 | 5/16" $\times 3 / 8$ | 116421 | 100 | 17.91 |
| 5/8 | 116395 | 100 | 6.34 | 1/2 | 116423 | 100 | 20.02 |
| 3/4 | 116398 | 100 | 7.06 | 5/8 | 116425 | 100 | 22.11 |
|  |  |  |  | 3/4 | 116427 | 100 | 24.22 |
| \#10-32 UNF - Key Size 1/8" |  |  |  | 1 | 116432 | 100 | 28.42 |
| \#10 x 3/8 | 116392 | 100 | 4.86 |  |  |  |  |
| 1/2 | 116394 | 100 | 5.59 | 3/8-16 UNC - Key Size 7/32" |  |  |  |
| 3/4 | 116400 | 100 | 7.06 | $3 / 8^{\prime \prime} \times 1 / 2$ | 116434 | 100 | 31.68 |
|  |  |  |  | 3/4 | 116439 | 100 | 37.84 |
|  |  |  |  | 1 | 116444 | 100 | 44.00 |
|  |  |  |  | $11 / 4$ | 116446 | 100 | 50.16 |

All flange button head socket screws are supplied with full thread

## Untrak

NABL ISO/IEC 17025:2005

## PREGISION in Every Fastener

Unbrako Lab is equipped state-of-the-art equipment for testing of both physical and metallurgical aspects of fasteners for the most demanding industries:

\author{

- Tensile testing <br> - Hardness testing <br> - Salt spray testing
}
- Digital profile analysis
- X-ray analysis of coating thickness
- Impact Testing
- Chemical composition analysis (Spectrometer)
- Metallurgical Microscope with Image Analyzer
- Dynamic fatigue testing
- Torque tension and friction testing
- Eddy current Testing
- MCD Testing


## SOCKET

 SET SCREWSIf you know set screws, you know that the tighter you can tighten them, the better they hold and the more they resist loosening from vibration. But there's a limit to how much you can tighten the average socket set screw. If you're not care-ful, you can ream or crack the socket, and in some cases, even strip the threads. So you're never quite sure whether or not it will actually stay tight. With UNBRAKO set screws it's a different story. A unique combination of design and carefully controlled manufacturing and heat treating gives these screws extra strength that permits you to tighten them appreciably tighter than ordinary screws with minimal fear of reaming or cracking the socket. this extra strength represents a substantial bonus of extra holding power and the additional safety and reliability that goes with it.

Design - Deeper UNBRAKO sockets give more key engagement to let you seat the screws tighter. Corners are radiused to safeguard against reaming or cracking the socket when the extra tightening torque is applied. The sharp corners of other set screws create high stress
concentrations and can cause can cause cracking, even at lower tightening torques. By eliminating the corners, the radii distribute tightening stresses to reduce the chance of splitting to a minimum.

Controlled Manufacturing - The fully-formed threads of UNBRAKO set screws are rolled under extreme pressure to minimize stripping and handle the higher tightening torques. Also, with rolled threads, tolerances can be more closely maintained. Unbrako set screws
have Class 3A threads, closest interchangeable fit, giving maximum cross-section with smooth assembly. The thread form itself has the radiused root that increases the strength of the threads and resistance to shear.

Controlled Heat Treatment - This is the third element of the combination. Too little carbon in the furnace atmosphere (decarburization) makes screws soft, causing reamed sockets, stripped threads and sheared points when screws are tightened. Too much carbon (carburization) makes screws brittle and liable to crack or fracture. The heat treatment is literally tailored to each "heat" of UNBRAKO screws, maintaining the necessary controlled Rc 45-53 hardness for maximum strength. Finally, point style affects holding power. As much as $15 \%$ more can contributed, depending on the depth of penetration. The cone point (when used without a spotting hole in the shaft) gives greatest increase because of its greater penetration. The plain cup point by far the most commonly used, because of the wide range of applications to which it is adaptable.

However, there is one cup point that can give you both a maximum holding power and of resistance to vibration. It is the exclusive UNBRAKO knurled cup point, whose locking knurls bite into the shaft and resist the tendency of the screw to back out of the tapped hole. The chart on this page shows clearly how much better the UNBRAKO set screws resist vibration in comparison with plain cup point set screws. UNBRAKO knurled cup point self-locking set screws give you excellent performance under conditions of extreme vibration.

## SOCKET

## SET SCREWS

In contrast to other types of fasteners, set screws are primarily used in compression. They must hold fast against three types of forces, torsional (rotational), axial (lateral movement) and vibrational. To be effective, socket set screws should produce a strong clamping action which resists the relative motion between the assembled parts, because of the compression developed by tightening the set screw. Since holding power is proportional to seating torque, the tighter you can seat the screw, the higher the compression force will be.

But there is a limit to how much you can tighten the average set screw. If you're not careful, you'll ream or crack the socket, or strip the threads. So you're never sure if the screw is tight enough, and whether it will stay tight.

But you can be sure that Unbrako set screws will 'stay put' because you can tighten them until the key twists off, with no damage to the screws. Unbrako recommend tightening torques as much as $40 \%$ higher than other set screws, giving you extra holding power and additional safety and reliability. Unbrako socket set screws hold tighter because
they are stronger than other set screws. The superior strength and dimensional uniformity of Unbrako set screws permit use of consistently higher seating torques than with other set screws. Consequently you can often save money because you can reduce the size or the number of set screws you require in your assembly.

Here are some of the reasons why Unbrako set screws are so strong and stay tight. Unbrako set screws are made of high grade alloy steel and heat treated to a minimum hardness of Rc 45 . Deep accurate sockets give more key engagement for extra wrenching areas. Radiused socket corners minimize points of weakness where cracks may start. Distribute stresses. Fully formed rolled threads provide greater strength and resistance to stripping. Controlled heat treatment assures uniform hardness without brittleness.

Unbrako socket set screws are available in knurled cup, cone, half dog, flat and plain cup point styles in plain or plated finishes. Stainless steel set screws are available in plain cup points only.

Fully formed threads - are rolled, not cut or ground. Metal is compressed, making it extra strong. Threads resist shearing, withstand higher tightening torques Class 3A threads Formed with closest interchangeable fit for maximum cross section with smooth assembly. Assure better mating of parts

Radiused socket corners -
Rounded corners resist cracking and allow UNBRAKO set screws to withstand high tightening torques

Counterbored knurled cup
point - Exclusive UNBRAKO self-
locking point provides 5 times greater vibrational holding power than other knurled points

Deep socket - Key fits deeply into socket to provide extra wrenching area for tighter tightening without reaming the socket or rounding off corners of key


Continuous grain flow - Flow
lines of rolled threads follow closely the contour of the screw

Balanced heat treatment It's customized to individual lots of screws for uniform hardness, assuring maximum strength without brittleness

## SOCKET

 SET SCREWS
## Point Selection According To Application

Point selection is normally determined by the nature of the application - materials, their relative hardness, frequency of assembly and re-assembly and other factors. Reviewed here are standard point types, their general features and most frequent areas of application of each type.

## KNURLED CUP

For quick and permanent location of gears, collars, pulleys or knobs on shafts. Exclusive counterclockwise locking knurls resist screw loosening, even in poorly tapped holes. Resists most severe vibration.

## PLAIN CUP

Use against hardened shafts, in zinc, die castings and other soft materials where high tightening torques are impractical.

## Torsional And Axial Holding Power

Size selection of socket set screws

The user of a set-screw-fastened assembly is primarily buying static holding power. The data in this chart offers a simplified means for selecting diameter and seating torque of a set screw on a given dia-meter shaft. Torsional holding power in inch-pounds and axial holding power in pounds are tabulated for various cup point socket screws, seated at recommended installation torques. Shafting used was hardened to Rockwell C15. Test involved Class 3A screw threads in Class 2B tapped holes. Data was determined experimentally in a long series of tests in which holding power was defined as the minimum load to produce 0.010 inch relative movement of shaft and collar. From this basic chart, values can be modified by percentage factors to yield suitable design data for almost any standard set screw application.

## CONE POINT

For permanent location of parts. Deep penetration gives highest axial and holding power. In material over Rockwell C15 point is spotted to half its length to develop shear strength across point. Used for pivots and fine adjustment.

## HALF DOG POINT

Used for permanent location of one part to another. Point is spotted in hole drilled in shaft or against flat (milled). Often replaces dowel pins. Works well against hardened members or hollow tubing.

## FLAT POINT

Use where parts must be frequently re-set, as it causes little or no damage to part it bears against. Can be used against hardened shafts (usually with ground flat for better contact) and as adjusting screw. Preferred for thin wall thickness and on soft plugs.




KNURLED CUP


PLAIN CUP

Fasten collars, sheaves, gears, knobs on shafts. Locate machine parts. Self-locking knurled cup point is standard. Special Points like Flat, Dog, Cone \& Plain Cup are also available.

## Mechanical Properties

Unbrako High Grade Alloy Steel
Hardness: Rc 45 Minimum

Notes

1. Corner of recess must have fillets to minimise stress concentrations.
2. Thread Class: 6 g
3. Working Temperature: $-50^{\circ} \mathrm{C}$ to $+300^{\circ} \mathrm{C}$
4. Angle: The cup angle is 135 max for screw lengths equal to or smaller than screw diameter. For longer lengths, the cup angle will be 124 max.
5. Torques calculated at $75 \%$ of the torsional shear strength of the respective Unbrako wrenches.

Maximum Tightening Torque
Thread

| size | Nm | Ibf.in. |
| :--- | :---: | :---: |
| M3 | 0.87 | 7.7 |
| M4 | 2.20 | 19.5 |
| M5 | 4.60 | 41.0 |
| M6 | 7.80 | 69.0 |
| M8 | 18.00 | 160.0 |
| M10 | 36.00 | 320.0 |
| M12 | 62.00 | 550.0 |
| (M14) | 62.00 | 550.0 |
| M16 | 150.00 | 1330.0 |
| (M18) | 290.00 | 2570.0 |
| M20 | 290.00 | 2570.0 |
| (M22) | 475.00 | 4200.0 |
| M24 | 475.00 | 4200.0 |

Length Tolerance

| Screws Over | Up to and <br> including <br> Screw Dia | Tolerance <br> - <br> Screw Dia |
| :---: | :---: | :---: |
| 50 | $\pm 0.25-0.00$ |  |
| 50 | 80 | $\pm 0.50$ |
| 80 | 120 | $\pm 0.70$ |
| 120 | 250 | $\pm 0.80$ |

Unorado


Fasten collars, sheaves, gears, knobs on shafts. Locate machine parts. Self-locking knurled cup point is standard. Special Points like Flat, Dog, Cone \& Plain Cup are also available.

Equivalent Standards

|  | BS 4168, ASME B18.3.6M |
| :--- | :---: |
| Flat Point | DIN 913, ISO 4026 |
| Cone Point | DIN 914, ISO 4027 |
| Dog Point | DIN 915, ISO 4028 |
| Plain Cup | DIN 916, ISO 4028 |
|  | ISO 898-5 |

Mechanical Properties
Unbrako High Grade Alloy Steel
Hardness: Rc 45 Minimum

## Notes

1. Corner of recess must have fillets to minimise stress concentrations.
2. Thread Class: 6 g
3. Working Temperature: $-50^{\circ} \mathrm{C}$ to $+300^{\circ} \mathrm{C}$
4. Screws with lengths $L$ or smaller will have half dog point $H$. Screws with lengths larger than $L$ will have full dog point HL.
5. Torques calculated at $75 \%$ of the torsional shear strength of the respective Unbrako wrenches.

## Length Tolerance

|  | Up to and <br> including | Tolerance |
| :---: | :---: | :---: |
| Screws Over | Screw Dia | $+0.25-0.00$ |
| - | 50 | $\pm 0.25$ |
| Screw Dia | 80 | $\pm 0.50$ |
| 50 | 120 | $\pm 0.70$ |
| 80 | 250 | $\pm 0.80$ |




FULL DOG


HALF DOG

Product Dimensions

| Thread |  |  | Dog Point |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| size | Pitch | Socket Size |  | H-Full |  |  |
| AL-Half |  |  |  |  |  |  |
| A |  | W | L (See | Dog | Dog | V |
| nom. |  | nom. | Note 4) | max | max | max |
| M3 | 0.50 | 1.5 | 5.00 | 1.75 | 1.00 | 2.00 |
| M4 | 0.70 | 2.0 | 6.00 | 2.25 | 1.25 | 2.50 |
| M5 | 0.80 | 2.5 | 6.00 | 2.75 | 1.50 | 3.50 |
| M6 | 1.00 | 3.0 | 8.00 | 3.25 | 1.75 | 4.00 |
| M8 | 1.25 | 4.0 | 10.00 | 4.30 | 2.25 | 5.50 |
| M10 | 1.50 | 5.0 | 12.00 | 5.30 | 2.75 | 7.00 |
| M12 | 1.75 | 6.0 | 16.00 | 6.30 | 3.25 | 8.50 |
| (M14) | 2.00 | 6.0 | 20.00 | 7.36 | 3.80 | 10.00 |
| M16 | 2.00 | 8.0 | 20.00 | 8.36 | 4.30 | 12.00 |
| (M18) | 2.50 | 10.0 | 25.00 | 9.36 | 4.80 | 13.00 |
| M20 | 2.50 | 10.0 | 25.00 | 10.36 | 5.30 | 15.00 |
| (M22) | 2.50 | 12.0 | 30.00 | 11.43 | 5.80 | 17.00 |
| M24 | 3.00 | 12.0 | 30.00 | 12.43 | 6.30 | 18.00 |

Application Data

|  | Maximum <br> Thread <br> size <br> M3$c$ <br> Tightening Torque <br> Nm |  |
| :--- | ---: | ---: |
| Ibf.in. |  |  |
| M4 | 0.87 | 7.7 |
| M5 | 4.20 | 19.5 |
| M6 | 7.80 | 41.0 |
| M8 | 18.00 | 160.0 |
| M10 | 36.00 | 320.0 |
| M12 | 62.00 | 550.0 |
| (M14) | 62.00 | 550.0 |
| M16 | 150.00 | $1,330.0$ |
| (M18) | 290.00 | $2,570.0$ |
| M20 | 290.00 | $2,570.0$ |
| (M22) | 475.00 | $4,200.0$ |
| M24 | 475.00 | $4,200.0$ |

Sizes in brackets are non-preferred standards.

## Torsional and axial holding power

Tabulated axial and torsional holding powers are typical strengths and should be used accordingly, with specific safety factors appropriate to the given application and load conditions.

| Thread | Seating |  | Shaft diameter (shaft hardness Rc 15 to Rc 35) Torsional holding power Nm |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Size | Torque <br> Nm | Holding <br> Power (kN) | 1.4 | 1.6 | 1.8 | 2.0 | 3.0 | 4.0 | 5.0 | 6.0 | 8.0 | 10 | 12 | 14 |
| M1.4 | . 10 | . 19 | . 13 | . 15 | . 17 | . 19 | . 29 | . 38 | . 48 |  |  |  |  |  |
| M1.6 | . 10 | . 22 | . 15 | . 18 | . 20 | . 22 | . 33 | . 44 | . 55 | . 66 |  |  |  |  |
| M1.8 | . 10 | . 25 | . 18 | . 20 | . 23 | . 25 | . 38 | . 50 | . 63 | . 75 | 1.0 |  |  |  |
| M2.0 | . 21 | . 29 | . 20 | . 23 | . 26 | . 29 | . 44 | . 58 | . 73 | . 87 | 1.2 | 1.5 |  |  |
| M2.5 | . 60 | . 53 |  | . 42 | . 48 | . 53 | . 80 | 1.10 | 1.30 | 1.60 | 2.1 | 2.7 | 3.2 |  |
| M2.6 | . 60 | . 56 |  |  | . 50 | . 56 | . 84 | 1.10 | 1.40 | 1.70 | 2.2 | 2.8 | 3.4 | 3.9 |
| M3 | . 87 | . 71 |  |  |  | . 71 | 1.07 | 1.40 | 1.80 | 2.10 | 2.8 | 3.6 | 4.3 | 5.0 |
| M4 | 2.20 | 1.70 |  |  |  | 1.70 | 2.60 | 3.40 | 4.30 | 5.10 | 6.8 | 8.5 | 10.0 | 12.0 |
| M5 | 4.60 | 2.50 |  |  |  |  | 3.80 | 5.00 | 6.30 | 7.50 | 10.0 | 13.0 | 15.0 | 18.0 |
| M6 | 7.80 | 4.20 |  |  |  |  |  |  | 11.00 | 13.00 | 17.0 | 21.0 | 25.0 | 29.0 |
| M8 | 18.00 | 6.70 |  |  |  |  |  |  |  | 20.00 | 27.0 | 34.0 | 40.0 | 47.0 |
| M10 | 36.00 | 9.30 |  |  |  |  |  |  |  |  | 37.0 | 47.0 | 56.0 | 65.0 |
| M12 | 62.00 | 12.00 |  |  |  |  |  |  |  |  |  | 60.0 | 72.0 | 84.0 |
| M14 | 62.00 | 15.00 |  |  |  |  |  |  |  |  |  |  | 90.0 | 105.0 |
| M16 | 150.00 | 18.00 |  |  |  |  |  |  |  |  |  |  |  | 126.0 |
| Thread | Seating | Axial | Shaft diameter (shaft hardness Rc 15 to Rc 35) Torsional holding power Nm |  |  |  |  |  |  |  |  |  |  |  |
| Size | Torque <br> Nm | Holding <br> Power (kN) | 16 | 18 | 20 | 25 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 |
| M2.6 | . 60 | . 56 | 4.5 |  |  |  |  |  |  |  |  |  |  |  |
| M3 | . 87 | . 71 | 5.7 | 6.4 | 7.1 |  |  |  |  |  |  |  |  |  |
| M4 | 2.20 | 1.70 | 14.0 | 15.0 | 17.0 | 21 |  |  |  |  |  |  |  |  |
| M5 | 4.60 | 2.50 | 20.0 | 23.0 | 25.0 | 31 | 38 |  |  |  |  |  |  |  |
| M6 | 7.80 | 4.20 | 34.0 | 38.0 | 42.0 | 53 | 63 | 84 |  |  |  |  |  |  |
| M8 | 18.00 | 6.70 | 54.0 | 60.0 | 67.0 | 84 | 101 | 134 | 168 | 201 |  |  |  |  |
| M10 | 36.00 | 9.30 | 74.0 | 84.0 | 93.0 | 116 | 140 | 186 | 233 | 279 |  |  |  |  |
| M12 | 62.00 | 12.00 | 96.0 | 108.0 | 120.0 | 150 | 180 | 240 | 300 | 360 | 420 |  |  |  |
| M14 | 62.00 | 15.00 | 120.0 | 135.0 | 150.0 | 188 | 225 | 300 | 375 | 450 | 525 | 600 |  |  |
| M16 | 150.00 | 18.00 | 144.0 | 162.0 | 180.0 | 225 | 270 | 360 | 450 | 540 | 630 | 720 | 810 |  |
| M18 | 290.00 | 21.00 | 168.0 | 189.0 | 210.0 | 263 | 315 | 420 | 525 | 630 | 735 | 840 | 945 | 1050 |
| M20 | 290.00 | 23.00 |  | 207.0 | 230.0 | 288 | 345 | 460 | 575 | 690 | 805 | 920 | 1040 | 1150 |
| M22 | 475.00 | 26.00 |  |  | 260.0 | 325 | 390 | 520 | 650 | 780 | 910 | 1040 | 1170 | 1300 |
| M24 | 475.00 | 29.00 |  |  |  | 363 | 435 | 580 | 725 | 870 | 1020 | 1160 | 1310 | 1450 |


| Knurled Cup Point |  |  |  |
| :---: | :---: | :---: | :---: |
| Size | Part No. | $6$ | $\begin{aligned} & \text { lbs } \\ & / 1000 \end{aligned}$ |
| M3(0.5) - Key Size 1.5 mm |  |  |  |
| M $3 \times 3$ | 104076 | 200 | 0.18 |
| 4 | 103172 | 200 | 0.24 |
| 5 | 103175 | 200 | 0.29 |
| 6 | 103176 | 200 | 0.40 |
| 8 | 103177 | 200 | 0.57 |
| 10 | 103178 | 200 | 0.73 |
| 12 | 103179 | 200 | 0.90 |
| 16 | 103180 | 200 | 1.30 |


| Size | Part No. | lbs |  |
| ---: | ---: | ---: | ---: |
|  | M8 (1.25) - Key Size 4 mm |  |  |
|  |  |  |  |
| M8 x 8 | 103224 | 200 | 3.92 |
| 10 | 103227 | 200 | 4.82 |
| 12 | 103228 | 200 | 6.23 |
| 15 | 401091 | 200 | 7.70 |
| 16 | 103229 | 200 | 8.43 |
| 20 | 103230 | 200 | 10.85 |
| 25 | 103231 | 200 | 13.86 |
| 30 | 103235 | 200 | 16.85 |
| 35 | 103236 | 200 | 19.87 |
| 40 | 103237 | 200 | 25.34 |
| 50 | 103240 | 200 | 28.91 |


| Size | Part No. | 9 | $\begin{aligned} & \text { lbs } \\ & / 1000 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| M20 (2.5) - Key Size 10mm |  |  |  |
| M20 $\times 25$ | 103286 | 50 | 79.64 |
| 30 | 103287 | 50 | 99.57 |
| 35 | 103288 | 25 | 119.53 |
| 40 | 103289 | 25 | 139.48 |
| 50 | 103292 | 25 | 179.37 |
| 60 | 103294 | 25 | 219.25 |
| Flat P |  |  | - |


| M4 (0.7) - Key Size 2mm |  |  |  |
| ---: | :---: | :---: | :---: |
| M4 x 4 | 103182 | 200 | 0.44 |
| 5 | 103185 | 200 | 0.55 |
| 6 | 103186 | 200 | 0.84 |
| 8 | 103187 | 200 | 1.01 |
| 10 | 103188 | 200 | 1.28 |
| 12 | 103189 | 200 | 1.56 |
| 15 | 401084 | 200 | 2.00 |
| 16 | 103191 | 200 | 2.13 |
| 20 | 103193 | 200 | 2.73 |


| M5 (0.8) - Key Size 2.5mm |  |  |  |
| ---: | :---: | :---: | :---: |
| M5 x 5 | 103194 | 200 | 0.88 |
| 6 | 103195 | 200 | 1.03 |
| 8 | 103196 | 200 | 1.54 |
| 10 | 103197 | 200 | 2.00 |
| 12 | 103198 | 200 | 2.46 |
| 15 | 401099 | 200 | 3.17 |
| 16 | 103199 | 200 | 3.39 |
| 20 | 103202 | 200 | 4.31 |
| 25 | 103203 | 200 | 5.48 |
| 30 | 103204 | 200 | 6.64 |


| M10 (1.5) - Key Size 5mm |  |  |  |
| ---: | ---: | ---: | ---: |
| M10 x 10 | 103241 | 200 | 7.41 |
| 12 | 103244 | 200 | 9.04 |
| 15 | 401094 | 200 | 11.90 |
| 16 | 103245 | 200 | 12.85 |
| 20 | 103246 | 200 | 16.65 |
| 25 | 103247 | 200 | 21.41 |
| 30 | 103249 | 200 | 26.16 |
| 35 | 103251 | 200 | 34.54 |
| 40 | 103252 | 200 | 35.68 |
| 45 | 103253 | 100 | 40.44 |
| 50 | 103254 | 100 | 45.19 |


| Size | Part No. | $\theta$ | $\begin{aligned} & \text { lbs } \\ & \text { /1000 } \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| M3 (0.5) - Key Size 1.5mm |  |  |  |
| M3 x 3 | 120000 | 200 | 0.22 |
| 4 | 120001 | 200 | 0.22 |
| 5 | 104024 | 200 | 0.33 |
| 6 | 108106 | 200 | 0.44 |
| 8 | 108108 | 200 | 0.66 |
| 10 | 108109 | 200 | 0.66 |
| 12 | 104025 | 200 | 0.88 |
| 16 | 120004 | 200 | 1.32 |


| M12 (1.75) - Key Size 6mm |  |  |  |
| ---: | ---: | ---: | ---: |
| M12 x 12 | 103256 | 100 | 12.25 |
| 16 | 103258 | 100 | 17.78 |
| 20 | 103259 | 100 | 23.32 |
| 25 | 103260 | 100 | 30.25 |
| 30 | 103261 | 100 | 37.16 |
| 35 | 103262 | 100 | 44.09 |
| 40 | 103263 | 50 | 51.00 |
| 45 | 103269 | 50 | 57.93 |
| 50 | 103270 | 50 | 64.83 |
| 60 | 103272 | 50 | 78.67 |


| M4 x 4 | 121084 | 200 | 0.44 |
| ---: | :---: | :---: | :---: |
| 5 | 104027 | 200 | 0.59 |
| 6 | 111691 | 200 | 0.66 |
| 8 | 108110 | 200 | 0.88 |
| 10 | 104028 | 200 | 1.32 |
| 12 | 104029 | 200 | 1.76 |
| 16 | 108101 | 200 | 2.42 |
| 20 | 120005 | 200 | 2.64 |
| M5 (0.8)-Key Size 2.5 mm |  |  |  |
| $\mathbf{M 5 \times 5}$ | 121109 | 200 | 0.88 |
| 6 | 104031 | 200 | 1.10 |
| 8 | 104033 | 200 | 1.54 |
| 10 | 104034 | 200 | 2.20 |
| 12 | 104035 | 200 | 2.64 |
| 16 | 122408 | 200 | 3.74 |
| 20 | 104038 | 200 | 4.62 |
| 25 | 120006 | 200 | 5.94 |


| M6 (1) - Key Size 3mm |  |  |  |
| ---: | :---: | :---: | :---: |
| M6 x 6 | 105476 | 200 | 1.54 |
| 8 | 108095 | 200 | 2.20 |
| 10 | 108111 | 200 | 2.86 |
| 12 | 122395 | 200 | 3.74 |

[^1]| Flat Point |  |  | -1] |
| :---: | :---: | :---: | :---: |
| Size | Part No. | $6$ | $\begin{aligned} & \text { lbs } \\ & / 1000 \end{aligned}$ |
| M6 (1) - Key Size 3mm |  |  |  |
| M6 $\times 15$ | 401089 | 200 | 4.84 |
| 16 | 104041 | 200 | 5.28 |
| 20 | 108096 | 200 | 6.82 |
| 25 | 104042 | 200 | 8.80 |
| 30 | 104043 | 200 | 10.56 |
| 40 | 120009 | 200 | 14.52 |
| M8 (1.25) - Key Size 4mm |  |  |  |
| M8x 8 | 120861 | 200 | 3.74 |
| 10 | 108227 | 200 | 4.40 |
| 12 | 104044 | 200 | 6.93 |
| 16 | 120012 | 200 | 8.43 |
| 20 | 120013 | 200 | 13.64 |
| 25 | 106340 | 200 | 14.96 |
| 30 | 120014 | 200 | 16.85 |
| 35 | 120016 | 200 | 28.60 |
| 40 | 120017 | 200 | 25.34 |
| 50 | 120020 | 200 | 29.72 |

M10 (1.5) - Key Size 5mm

| M10 X 10 | 107993 | 200 | 6.38 |
| ---: | ---: | ---: | ---: |
| 12 | 108257 | 200 | 7.92 |
| 16 | 110881 | 200 | 14.30 |
| 20 | 110897 | 200 | 17.14 |
| 25 | 120022 | 200 | 23.76 |
| 30 | 120023 | 200 | 28.60 |
| 40 | 120025 | 200 | 39.82 |
| 50 | 120027 | 100 | 48.40 |


| M12 (1.75) - Key Size 6 mm |  |  |  |
| ---: | ---: | ---: | ---: |
| M12 X 12 | 120028 | 100 | 13.86 |
| 16 | 120029 | 100 | 19.80 |
| 20 | 107985 | 100 | 26.18 |
| 25 | 125795 | 100 | 35.20 |
| 40 | 120032 | 50 | 55.88 |
| 50 | 120033 | 50 | 70.62 |
| 60 | 120037 | 50 | 83.60 |


| M8 (1.25) - Key Size 4mm |  |  |  |
| ---: | :---: | :---: | ---: |
| M8 x 8* | 120222 | 200 | 3.74 |
| 10 | 107983 | 200 | 4.40 |
| 12 | 120226 | 200 | 5.06 |
| 16 | 120227 | 200 | 9.02 |
| 20 | 121121 | 200 | 13.64 |
| 25 | 120228 | 200 | 14.96 |
| 30 | 108188 | 200 | 24.20 |
| 40 | 108146 | 200 | 33.00 |


| $M 3(0.5)-$ Key Size 1.5 mm |  |  |  |
| ---: | :---: | :---: | :---: |
| M3 x 5 | 120071 | 200 | 0.31 |
| 6 | 108208 | 200 | 0.44 |
| 8 | 120072 | 200 | 0.66 |
| $M 4(0.7)-$ Key Size 2 mm |  |  |  |
| M4 x 5 | 120076 | 200 | 0.55 |
| 6 | 108143 | 200 | 0.66 |
| 8 | 108249 | 200 | 0.88 |
| 10 | 120077 | 200 | 1.32 |
| 12 | 120078 | 200 | 1.76 |



| Size | Part No. | $\theta$ | $\begin{aligned} & \text { lbs } \\ & \text { /1000 } \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| M10 (1.5) - Key Size 5mm |  |  |  |
| M10 x 10* | 108207 | 200 | 6.38 |
| 16 | 108191 | 200 | 14.30 |
| 20 | 108113 | 200 | 18.48 |
| 25 | 108085 | 200 | 23.76 |
| 30 | 108098 | 200 | 34.98 |
| 45 | 120238 | 100 | 44.22 |
| 50 | 120240 | 100 | 48.62 |


| M12 (1.75) - Key Size 6mm |  |  |  |
| ---: | ---: | ---: | ---: |
| M12 $\times 12^{*}$ | 120242 | 100 | 14.30 |
| 20 | 120243 | 100 | 26.18 |
| 25 | 120244 | 100 | 33.66 |
| 40 | 107982 | 50 | 55.88 |
| 50 | 120248 | 50 | 70.62 |


| M16 (2) - Key Size 8mm |  |  |  |
| ---: | :---: | :---: | ---: |
| M16 $\times 30$ | 107984 | 50 | 65.78 |
| 40 | 108039 | 50 | 94.38 |
| 50 | 120259 | 50 | 122.76 |
| 60 | 120261 | 25 | 151.14 |

M20 (2.5) - Key Size 10mm

| $\mathrm{M} 20 \times 50$ | 120270 | 25 | 210.10 |
| ---: | ---: | ---: | ---: |
| 60 | 120275 | 25 | 242.95 |

Cone Point


| Size | Part No. | lbs |  |
| ---: | :---: | :---: | :---: |
| M5 (0.8) - Key |  |  |  |
| Size 2.5 mm |  |  |  |
| M5 x 6 | 120085 | 200 | 1.10 |
| 8 | 120086 | 200 | 1.54 |
| 10 | 113532 | 200 | 2.20 |
| 12 | 108144 | 200 | 2.64 |
| 16 | 120088 | 200 | 3.74 |

Size Part No. $\quad$| lbs |
| :---: |
| $/ 1000$ |

| Size | Part No. | lbs |  |
| ---: | :---: | :---: | :---: |
| M10 (1.5) - Key Size 5 mm |  |  |  |
| M10 $\times 16$ | 104073 | 200 | 13.24 |
| 20 | 104074 | 200 | 17.14 |
| 25 | 122205 | 200 | 22.02 |


| $\mathrm{M} 2.5 \times 3$ | 104173 | 200 | 0.13 |
| ---: | ---: | ---: | ---: |
| 6 | 104115 | 200 | 0.31 |
| 8 | 104116 | 200 | 0.42 |
| 10 | 104117 | 200 | 0.53 |


| M12 (1.75) - Key Size 6 mm |  |  |  |
| ---: | ---: | ---: | ---: |
| M12 x 12 | 108056 | 100 | 12.61 |
| 20 | 108053 | 100 | 23.89 |



Fasten collars, sheaves, gears, knobs on shafts. Locate machine parts. Self-locking knurled cup point is standard. Special Points like Flat, Dog, Cone \& Plain Cup are also available.

## Equivalent Standards

ASME B18.3, BS 2470

## Mechanical Properties

Material : ASTM F912
Dimensions : ASME/ANSI B18.3
Hardness : Rc 45-53
Thread: 3A

## Length Tolerance

|  | .63 and | over .63 <br> Diameter 2" <br> under | over 2" <br> to 6" | over 6" |
| :---: | :---: | :---: | :---: | :---: |
| All | $\pm .01$ | $\pm .02$ | $\pm .03$ | $\pm .06$ |

## NOTE

1. Knurled Cup Point: When length equals nominal dia or less, included angle is $130^{\circ}$. 2. Cone Cup Point: When length equals nominal diameter or less, included angle is $118^{\circ}$. ( $\# 4 \times 1 / 8$ and $\# 8 \times 3 / 16$ also have $118^{\circ}$ angle)
*CAUTION: Values shown in column T are for minimum stock length cup point screws. Screws shorter than nominal minimum length shown do not have sockets deep enough to utilize full key capability which can result in failure of socket, key or mating threads.

[^2]

Fasten collars, sheaves, gears, knobs on shafts. Locate machine parts. Self-locking knurled cup point is standard. Special Points like Flat, Dog, Cone \& Plain Cup are also available.

## Equivalent Standards

ASME B18.3, BS 2470

## Mechanical Properties

Material : ASTM F912 - alloy steel Dimensions : ASME/ANSI B18.3
Hardness: Rc 45-53 (alloy steel only),
Thread: 3A
Length Tolerance

|  | .63 and <br> Diameter <br> under | over .63 <br> to 2" | over 2" <br> to 6" | over 6" |
| :---: | :---: | :---: | :---: | :---: |
| All | $\pm .01$ | $\pm .02$ | $\pm .03$ | $\pm .06$ |

## NOTE

1. Cone Cup Point: When length equals nominal diameter or less, included angle is $118^{\circ}$. ( $\# 4 \times 1 / 8$ and $\# 8 \times 3 / 16$ also have $118^{\circ}$ angle)
2. Knurled Cup Point: When length equals nominal dia or less, included angle is $130^{\circ}$.


Product Dimensions

| nom. | Thread per inch. | Head Diameter A |  |  | Hex Socket Size W F nom | C $\max \min$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| size | UNRC UNRF | max | UNRC | UNRF |  |  |  |
| 1/4 | 2028 | . 2500 | . 2419 | . 2435 | 5 . 125 | . 132 | . 118 |
| 5/16 | $18 \quad 24$ | . 3125 | . 3038 | . 3053 | 3 . 1562 | . 172 | . 156 |
| 3/8 | 1624 | . 3750 | . 3656 | . 3678 | 8 . 1875 | . 212 | . 194 |
| 7/16 | 1420 | . 4375 | . 4272 | . 4294 | 4 . 2187 | . 252 | . 232 |
| 1/2 | 1320 | . 5000 | . 4891 | . 4919 | 9 . 250 | . 291 | . 270 |
| 9/16 | 1218 | . 5625 | . 5511 | . 5538 | 8 . 250 | . 332 | . 309 |
| 5/8 | 1118 | . 6250 | . 6129 | . 6163 | 3 . 3125 | . 371 | . 347 |
| 3/4 | 1016 | . 7500 | . 7371 | . 7406 | 6 . 375 | . 450 | . 425 |
| 7/8 | 914 | . 8750 | . 8611 | . 8647 | 7 . 500 | . 530 | . 502 |
| 1 | 812 | 1.0000 | . 9850 | . 9886 | 6 . 5625 | . 609 | . 579 |
| $11 / 8$ | 712 | 1.1250 | 1.1086 | 1.1136 | 6 . 5625 | . 689 | . 655 |
| $11 / 4$ | 712 | 1.2500 | 1.2336 | 1.2386 | 6 . 625 | . 767 | . 733 |
| $13 / 8$ | 612 | 1.3750 | 1.3568 | 1.3636 | 6 . 625 | . 848 | . 808 |
| $11 / 2$ | 612 | 1.5000 | 1.4818 | 1.4886 | 6 . 750 | . 926 | . 886 |
| nom. size | Q max min | $\begin{aligned} & \mathrm{T}^{*} \\ & \mathrm{~min} \end{aligned}$ | max | P min | Recommended * seating torque In-lbs |  | screw length nom. |
| 1/4 | . 067.059 | . 105 | . 156 | . 149 | 87 |  | 5/16 |
| 5/16 | . 082.074 | . 140 | . 203 | . 195 | 165 |  | 3/8 |
| 3/8 | . 099.089 | . 140 | . 250 | . 241 | 290 |  | 7/16 |
| 7/16 | . 114.104 | . 190 | . 297 | . 287 | 430 |  | 1/2 |
| 1/2 | . 130.120 | . 210 | . 344 | . 334 | 620 |  | 9/16 |
| 9/16 | . 146.136 | . 265 | . 390 | . 379 | 620 |  | 5/8 |
| 5/8 | . 164.148 | . 265 | . 469 | . 456 | 1,325 |  | 11/16 |
| 3/4 | . 196.180 | . 330 | . 562 | . 549 | 2,400 |  | 3/4 |
| 7/8 | . 227.211 | . 450 | . 656 | . 642 | 3,600 |  | 3/4 |
| 1 | . 260.240 | . 550 | . 750 | . 734 | 5,000 |  | 7/8 |
| $11 / 8$ | . 291.271 | . 650 | . 844 | . 826 | 7,200 |  | 1 |
| $11 / 4$ | . 323.303 | . 700 | . 938 | . 920 | 9,600 |  | $11 / 8$ |
| $13 / 8$ | . 354.334 | . 700 | 1.031 | 1.011 | 9,600 |  | $11 / 4$ |
| $11 / 2$ | . 385.365 | . 750 | 1.125 | 1.105 | 11,320 |  | $11 / 4$ |

*CAUTION: Values shown in column T are for minimum stock length cup point screws. Screws shorter than nominal minimum length shown do not have sockets deep enough to utilize full key capability which can result in failure of socket, key or mating threads.

[^3]
## Torsional and axial holding power

(Based on Recommended Seating Torques - Inch-Lbs.)
Tabulated axial and torsional holding powers are typical strengths and should be used accordingly, with specific safety factors appropriate to the given application and load conditions.

| Thread Size | Seating <br> Torque <br> Ibf.in. | Axial Holding Power (lbf.) | Shaft diameter (shaft hardness Rc 15 to Rc 35) Torsional Holding Power Ibf.in. |  |  |  |  |  |  |  | 3/8 | 7/16 | 1/2 | 9/16 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1/16 | 3/32 | 1/8 | 5/32 | 3/16 | 7/32 | 1/4 | 5/16 |  |  |  |  |
| \#0 | 1.0 | 50 | 1.5 | 2.3 | 3.1 | 3.9 | 4.7 | 5.4 | 6.2 |  |  |  |  |  |
| \#1 | 1.8 | 65 | 2.0 | 3.0 | 4.0 | 5.0 | 6.1 | 7.1 | 8.1 | 10.0 |  |  |  |  |
| \#2 | 1.8 | 85 | 2.6 | 4.0 | 5.3 | 6.6 | 8.0 | 9.3 | 10.6 | 13.2 | 16.0 |  |  |  |
| \#3 | 5.0 | 120 | 3.2 | 5.6 | 7.5 | 9.3 | 11.3 | 13.0 | 15.0 | 18.7 | 22.5 | 26.3 |  |  |
| \#4 | 5.0 | 160 |  | 7.5 | 10.0 | 12.5 | 15.0 | 17.5 | 20.0 | 25.0 | 30.0 | 35.0 | 40.0 |  |
| \#5 | 10.0 | 200 |  |  | 12.5 | 15.6 | 18.7 | 21.8 | 25.0 | 31.2 | 37.5 | 43.7 | 50.0 | 56.2 |
| \#6 | 10.0 | 250 |  |  |  | 19.0 | 23.0 | 27.0 | 31.0 | 39.0 | 47.0 | 55.0 | 62.0 | 70.0 |
| \#8 | 20.0 | 385 |  |  |  | 30.0 | 36.0 | 42.0 | 48.0 | 60.0 | 72.0 | 84.0 | 96.0 | 108.0 |
| \#10 | 36.0 | 540 |  |  |  |  | 51.0 | 59.0 | 68.0 | 84.0 | 101.0 | 118.0 | 135.0 | 152.0 |
| 1/4 | 87.0 | 1,000 |  |  |  |  |  |  | 125.0 | 156.0 | 187.0 | 218.0 | 250.0 | 281.0 |
| 5/16 | 165.0 | 1,500 |  |  |  |  |  |  |  | 234.0 | 280.0 | 327.0 | 375.0 | 421.0 |
| 3/8 | 290.0 | 2,000 |  |  |  |  |  |  |  |  | 375.0 | 437.0 | 500.0 | 562.0 |
| 7/16 | 430.0 | 2,500 |  |  |  |  |  |  |  |  |  | 545.0 | 625.0 | 702.0 |
| 1/2 | 620.0 | 3,000 |  |  |  |  |  |  |  |  |  |  | 750.0 | 843.0 |
| 9/16 | 620.0 | 3,500 |  |  |  |  |  |  |  |  |  |  |  | 985.0 |


| Thread Size | Seating Torque Ibf.in. | Axial Holding Power (lbf) | Shaft diameter (shaft hardness Rc 15 to Rc 35) Torsional Holding Power Ibfin. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 5/8 | 3/4 | 7/8 | 1 | $11 / 4$ | $11 / 2$ | 13/4 | 2 | $21 / 2$ | 3 | $31 / 2$ | 4 |
| \#5 | 10.0 | 200 | 62 |  |  |  |  |  |  |  |  |  |  |  |
| \#6 | 10.0 | 250 | 78 | 94 | 109 |  |  |  |  |  |  |  |  |  |
| \#8 | 20.0 | 385 | 120 | 144 | 168 | 192 |  |  |  |  |  |  |  |  |
| \#10 | 36.0 | 540 | 169 | 202 | 236 | 270 | 338 |  |  |  |  |  |  |  |
| 1/4 | 87.0 | 1,000 | 312 | 375 | 437 | 500 | 625 | 750 |  |  |  |  |  |  |
| 5/16 | 165.0 | 1,500 | 468 | 562 | 656 | 750 | 937 | 1125 | 1310 | 1500 |  |  |  |  |
| 3/8 | 290.0 | 2,000 | 625 | 750 | 875 | 1000 | 1250 | 1500 | 1750 | 2000 |  |  |  |  |
| 7/16 | 430.0 | 2,500 | 780 | 937 | 1095 | 1250 | 1560 | 1875 | 2210 | 2500 | 3125 |  |  |  |
| 1/2 | 620.0 | 3,000 | 937 | 1125 | 1310 | 1500 | 1875 | 2250 | 2620 | 3000 | 3750 | 4500 |  |  |
| 9/16 | 620.0 | 3,500 | 1090 | 1310 | 1530 | 1750 | 2190 | 2620 | 3030 | 3500 | 4370 | 5250 | 6120 |  |
| 5/8 | 1,325.0 | 4,000 | 1250 | 1500 | 1750 | 2000 | 2500 | 3000 | 3750 | 4000 | 5000 | 6000 | 7000 | 8000 |
| 3/4 | 2,400.0 | 5,000 |  | 1875 | 2190 | 2500 | 3125 | 3750 | 4500 | 5000 | 6250 | 7500 | 8750 | 10000 |
| 7/8 | 5,200.0 | 6,000 |  |  | 2620 | 3000 | 3750 | 4500 | 5250 | 6000 | 7500 | 9000 | 10500 | 12000 |
| 1 | 7,200.0 | 7,000 |  |  |  | 3500 | 4375 | 5250 | 6120 | 7000 | 8750 | 10500 | 12250 | 14000 |


| Knurled Point |  |  | 四 |
| :---: | :---: | :---: | :---: |
| Size | Part No. | $\square$ | $\begin{gathered} \text { lbs } \\ / 1000 \end{gathered}$ |
| \#4-40 UNC - Key Size 0.05" |  |  |  |
| \# $4 \times 1 / 8$ | 107218 | 100 | 0.18 |
| 3/16 | 107235 | 100 | 0.29 |
| 1/4 | 117866 | 100 | 0.40 |
| 1/2 | 117933 | 100 | 0.81 |
| \#4-48 UNF - Key Size 0.05" |  |  |  |
| \#4 x 1/8 | 107829 | 100 | 0.18 |
| 3/16 | 107846 | 100 | 0.31 |
| 3/8 | 107894 | 100 | 0.64 |
| \#5-40 UNC - Key Size 1/16" |  |  |  |
| \#5 x 1/8 | 117965 | 100 | 0.22 |
| 3/16 | 117981 | 100 | 0.33 |
| 1/4 | 117997 | 100 | 0.48 |
| 1/2 | 118063 | 100 | 1.03 |
| 5/8 | 114014 | 100 | 1.32 |

\#5-44 UNF - Key Size 1/16"

| $\# 5 \times 1 / 8$ | 107912 | 100 | 0.20 |
| ---: | ---: | ---: | ---: |
| \#6-32 UNC - Key Size 1/16" |  |  |  |
| $\# 6 \times 1 / 8$ | 102949 | 100 | 0.24 |
| $3 / 16$ | 102967 | 100 | 0.42 |
| $1 / 4$ | 102983 | 100 | 0.57 |
| $5 / 16$ | 108396 | 100 | 0.75 |
| $3 / 8$ | 121651 | 100 | 0.90 |
| $7 / 16$ | 102767 | 100 | 1.17 |
| $1 / 2$ | 121751 | 100 | 1.23 |
| $3 / 4$ | 102866 | 100 | 1.89 |
| $7 / 8$ | 115033 | 100 | 2.22 |


| \#8-32 UNC - Key Size 5/64" |  |  |  |
| ---: | ---: | ---: | ---: |
| $\# 8 \times 1 / 8$ | 113100 | 100 | 0.33 |
| $3 / 16$ | 105233 | 100 | 0.57 |
| $1 / 4$ | 114173 | 100 | 0.81 |
| $5 / 16$ | 102972 | 100 | 1.06 |
| $3 / 8$ | 103005 | 100 | 1.32 |
| $1 / 2$ | 103071 | 100 | 1.80 |
| $5 / 8$ | 108566 | 100 | 2.29 |
| $3 / 4$ | 113228 | 100 | 2.79 |
| 1 | 111282 | 100 | 3.76 |

\#8-36 UNF - Key Size 5/64"
$\begin{array}{llll}\# 8 \times 1 / 8 & 119355 & 100 & 0.35\end{array}$

Pieces per Box

| Knurled Point |  |  |  |
| :---: | :---: | :---: | :---: |
| Size | Part No. |  |  |



| Size | Part No. | Ibs <br> $/ 1000$ |  |
| ---: | :---: | :---: | :---: |
| \#6-32 UNC - Key | Size $1 / 16^{\prime \prime}$ |  |  |
| \#6 x 1/8 | 113057 | 100 | 0.24 |
| $3 / 16$ | 113073 | 100 | 0.42 |
| $1 / 4$ | 109399 | 100 | 0.59 |
| $5 / 16$ | 109417 | 100 | 0.75 |
| $3 / 8$ | 109433 | 100 | 0.92 |
| $1 / 2$ | 109465 | 100 | 1.25 |
| $5 / 8$ | 109481 | 100 | 1.58 |
| $3 / 4$ | 109498 | 100 | 1.94 |
| 1 | 109531 | 100 | 2.60 |

\#1-64 UNF - Key Size 0.035"

| $\# 1 \times 1 / 16$ | 107275 | 100 | 0.04 |
| ---: | :---: | :---: | :---: |
| $3 / 32$ | 119983 | 100 | 0.06 |
| $1 / 8$ | 118176 | 100 | 0.08 |
| $\# 2-56$ UNC - Key Size $0.035^{\prime \prime}$ |  |  |  |
| $\# 2 \times 1 / 16$ | 106816 | 100 | 0.06 |
| $3 / 32$ | 113649 | 100 | 0.09 |
| $1 / 8$ | 113665 | 100 | 0.11 |
| $3 / 16$ | 113698 | 100 | 0.18 |
| $1 / 4$ | 113714 | 100 | 0.24 |


| \#6-40 UNF - Key Size 1/16" |  |  |  |
| :---: | :---: | :---: | :---: |
| \#6 x 1/8 | 119216 | 100 | 0.26 |
| $3 / 16$ | 119232 | 100 | 0.46 |
| $1 / 4$ | 119249 | 100 | 0.64 |
| $3 / 8$ | 119282 | 100 | 0.99 |


| $\# 3-48$ UNC - Key Size 0.050" |  |  |  |
| ---: | ---: | ---: | ---: |
| $\# 3 \times 3 / 32$ | 113730 | 100 | 0.09 |
| $1 / 8$ | 113747 | 100 | 0.11 |
| $3 / 16$ | 102978 | 100 | 0.26 |
| $1 / 4$ | 102995 | 100 | 0.37 |


| \#8-32 UNC - Key Size 5/64" |  |  |  |
| ---: | ---: | ---: | ---: |
| $\# 8 \times 1 / 8$ | 114993 | 100 | 0.33 |
| $3 / 16$ | 115009 | 100 | 0.59 |
| $1 / 4$ | 108241 | 100 | 0.84 |
| $5 / 16$ | 108256 | 100 | 1.10 |
| $3 / 8$ | 108273 | 100 | 1.34 |
| $1 / 2$ | 118841 | 100 | 1.85 |
| $5 / 8$ | 118857 | 100 | 2.33 |
| $3 / 4$ | 118873 | 100 | 2.84 |
| 1 | 118905 | 100 | 3.85 |
|  |  |  |  |

\#10-24 UNC - Key Size 3/32"

| $5 / 8-11$ UNC - Key Size 5/16" |  |  |  |
| ---: | ---: | ---: | ---: |
| $5 / 8^{\prime \prime} \times 1 / 2$ | 111417 | 100 | 22.57 |
| $5 / 8$ | 111449 | 50 | 30.34 |
| $7 / 8$ | 117842 | 50 | 45.89 |
| 1 | 117875 | 50 | 53.68 |
| $1-1 / 4$ | 117909 | 25 | 69.23 |
| $1-1 / 2$ | 111467 | 25 | 84.79 |
| $1-3 / 4$ | 111499 | 25 | 100.32 |


| $5 / 8-18$ UNF - Key Size 5/16" |  |  |  |
| ---: | ---: | :---: | ---: |
| $5 / 8^{\prime \prime} \times 5 / 8$ | 119273 | 50 | 33.51 |
| 1 | 119289 | 50 | 58.72 |


| \#4-40 UNC - Key Size 0.050" |  |  |  |
| ---: | ---: | ---: | ---: |
| $\# 4 \times 1 / 8$ | 103011 | 100 | 0.18 |
| $3 / 16$ | 103027 | 100 | 0.29 |
| $1 / 4$ | 103043 | 100 | 0.40 |
| $5 / 16$ | 103061 | 100 | 0.51 |
| $3 / 8$ | 103078 | 100 | 0.62 |
| $1 / 2$ | 108572 | 100 | 0.84 |
| $5 / 8$ | 108589 | 100 | 1.08 |


| $\# 10 \times 3 / 16$ | 118921 | 100 | 0.73 |
| ---: | ---: | ---: | ---: |
| $1 / 4$ | 118937 | 100 | 1.03 |
| $5 / 16$ | 118953 | 100 | 1.36 |
| $3 / 8$ | 118970 | 100 | 1.67 |
| $1 / 2$ | 111770 | 100 | 2.33 |


| $\# 10-32$ UNF - Key Size 3/32" |  |  |  |
| ---: | :---: | :---: | :---: |
| $\# 10 \times 3 / 16$ | 119397 | 100 | 0.84 |
| $1 / 4$ | 119413 | 100 | 1.19 |
| $5 / 16$ | 119429 | 100 | 1.50 |
| $3 / 8$ | 120397 | 100 | 1.85 |
| $1 / 2$ | 107300 | 100 | 2.55 |
| $5 / 8$ | 107316 | 100 | 3.26 |
| $3 / 4$ | 107332 | 100 | 3.94 |
| 1 | 117212 | 100 | 5.35 |
| $11 / 4$ | 117228 | 100 | 6.73 |
|  |  |  |  |
| $1 / 4-20$ UNC - Key Size $1 / 8^{\prime \prime}$ |  |  |  |
| $1 / 4^{\prime \prime} \times 1 / 4$ | 106510 | 100 | 1.78 |
| $5 / 16$ | 113489 | 100 | 2.38 |

Unbrako

| Size | Part No. | lbs |  |
| ---: | :---: | :---: | ---: |
| $1 / 4-20$ UNC - Key Size $1 / 8^{\prime \prime}$ |  |  |  |
| $1 / 4^{\prime \prime} \times 3 / 8$ | 113554 | 100 | 3.39 |
| $1 / 2$ | 106569 | 100 | 4.11 |
| $5 / 8$ | 119558 | 100 | 5.28 |
| $3 / 4$ | 117296 | 100 | 6.42 |
| 1 | 117427 | 100 | 8.76 |
| $11 / 4$ | 117492 | 100 | 11.07 |
| $11 / 2$ | 112469 | 100 | 13.40 |
| $13 / 4$ | 103102 | 100 | 15.71 |
| 2 | 103135 | 100 | 18.04 |


| $\# 1 / 4-28$ UNF - Key Size $1 / 8^{\prime \prime}$ |  |  |  |
| ---: | ---: | ---: | ---: |
| $1 / 4^{\prime \prime} \times 1 / 4$ | 117260 | 100 | 1.94 |
| $5 / 16$ | 117277 | 100 | 2.66 |
| $3 / 8$ | 117293 | 100 | 3.26 |
| $1 / 2$ | 107183 | 100 | 4.51 |
| $5 / 8$ | 107199 | 100 | 5.79 |
| $3 / 4$ | 116503 | 100 | 7.04 |
| 1 | 104560 | 100 | 9.57 |
| $11 / 4$ | 104592 | 100 | 12.08 |


| 3/8-24 UNF - Key Size 3/16" |  |  |  | 5/8-18 UNF - Key Size 5/16" |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $3 / 81$ " $1 / 4$ | 115994 | 100 | 4.66 | 5/8"x 5/8 | 115480 | 50 | 33.59 |
| 5/16 | 116026 | 100 | 5.65 | 1 | 115497 | 50 | 58.85 |
| 3/8 | 115083 | 100 | 7.15 |  |  |  |  |
| 1/2 | 115149 | 100 | 10.60 |  |  |  |  |
| 5/8 | 115181 | 100 | 13.09 |  |  |  |  |
| 3/4 | 114813 | 100 | 16.06 |  |  |  |  |
| 1 | 114845 | 100 | 22.00 |  |  |  |  |
| $11 / 4$ | 114880 | 100 | 27.94 |  |  |  |  |
| $11 / 2$ | 114912 | 100 | 33.88 |  |  |  |  |


| $\# 5 / 16-18$ UNC - Key Size 5/32" |  |  |  |
| ---: | ---: | ---: | ---: |
| $5 / 16^{\prime \prime} \times 1 / 4$ | 103169 | 100 | 2.77 |
| $5 / 16$ | 103201 | 100 | 3.70 |
| $3 / 8$ | 112503 | 100 | 4.64 |
| $1 / 2$ | 112568 | 100 | 6.51 |
| $5 / 8$ | 103243 | 100 | 8.38 |
| $3 / 4$ | 105227 | 100 | 10.25 |
| 1 | 113079 | 100 | 14.01 |
| $11 / 4$ | 109423 | 100 | 17.75 |
| $11 / 2$ | 109455 | 100 | 21.49 |
| $13 / 4$ | 109487 | 100 | 25.26 |
| 2 | 109521 | 100 | 30.98 |


| $7 / 16-14$ UNC - Key Size 7/32" |  |  |  |
| ---: | ---: | ---: | ---: |
| $7 / 16^{\prime \prime} \times 3 / 8$ | 114169 | 100 | 8.80 |
| $1 / 2$ | 103001 | 100 | 12.28 |
| $3 / 4$ | 103067 | 100 | 19.80 |
| 1 | 108595 | 100 | 27.30 |


| $7 / 16-20$ UNF - Key Size 7/32" |  |  |  |
| ---: | ---: | ---: | ---: |
| $7 / 16^{\prime \prime} \times 3 / 8$ | 103568 | 100 | 9.35 |
| $1 / 2$ | 103602 | 100 | 13.38 |


| $1 / 2-13$ UNC - Key Size $1 / 4^{\prime \prime}$ |  |  |  |
| ---: | ---: | ---: | ---: |
| $1 / 2^{\prime \prime} \times 3 / 8$ | 114340 | 100 | 10.82 |
| $1 / 2$ | 108519 | 100 | 15.77 |
| $5 / 8$ | 108535 | 100 | 20.75 |
| $3 / 4$ | 102895 | 100 | 25.72 |
| $7 / 8$ | 102911 | 100 | 30.69 |
| 1 | 104078 | 100 | 35.66 |
| $11 / 4$ | 104095 | 100 | 45.58 |
| $11 / 2$ | 104112 | 100 | 55.53 |
| $13 / 4$ | 104128 | 50 | 65.45 |
| 2 | 104144 | 50 | 75.39 |
| $21 / 2$ | 104160 | 50 | 95.26 |


| \#3/8-16 UNC - Key Size 3/16" |  |  |  | 1/2-20 UNF - Key Size 1/4" |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $3 / 8^{\prime \prime} \times 1 / 4$ | 114999 | 100 | 4.38 | 1/2" $\times 1 / 2$ | 103619 | 100 | 17.36 |
| 5/16 | 108247 | 100 | 4.99 | 5/8 | 103635 | 100 | 22.73 |
| 3/8 | 118815 | 100 | 6.40 | 3/4 | 115447 | 100 | 28.07 |
| 1/2 | 118879 | 100 | 9.13 | 1 | 115463 | 100 | 38.81 |
| 5/8 | 118911 | 100 | 11.86 |  |  |  |  |

Pieces per Box

# TAPER PRESSURE PLUGS 

# LEVL SEAL ${ }^{\circledR}$ TYPE Dryseal Thread Form with 7/8-inch per foot 

Precision hex socket with maximum depth for positive wrenching at higher seating torques
Dryseal Type With 3/4-inch Taper per Foot
Heat treated alloy steel for strength Rounded
closely controlled for better sealing

High pressure is developed through a deliberate difference of taper between the plug and the tapped hole having standard $3 / 4^{\prime \prime}$ taper

Flush seating is achieved through closer control of thread forms, sizes and taper-improves safety and appearance Fully formed PTF dryseal threads for better sealing without the use of a compound
Controlled chamfer for faster starting
Controlled chamfer for faster starting

Pressure plugs are not pipe plugs. Pipe plugs (plumber's fittings) are limited to pressures of 600 psi, are sealed with a compound, and are made of cast iron with cut threads and protruding square drive.

Pressure plugs are made to closer tolerances, are generally of higher quality, and almost all have taper threads. Properly made and used, they will seal at pressures to 5000 psi and without a sealing compound (pressure tests are usually at 20,000 psi.) they are often used in hydraulic and pneumatic designs.

## Performance Requirements

Pressure plugs used in industrial applications should:

- not leak at pressures to 5000 psi
- need no sealing compounds
- be reusable without seizure
- give a good seal when reused - seal low viscosity fluids
- require minimum seating torque
- require minimum re-tooling or special tools.

For a satisfactory seal, the threads of the plug and those in the mating hole must not gall or seize up to maximum possible tightening
torque. Galling and seizure are caused by metal pickup on the mating surfaces and are directly related to force on the surface, material hardness, lubrication used, and thread finish.

## How Pressure Plugs Seal

Sealing is achieved by crushing the crest of one thread against the root of the mating thread. If too much of compressive force is required to torque the plug, it will tend to gall in the hole. Too little force will not deform the crest of threads enough to produce a seal. Increasing the hardness of the material will reduce galling but will also increase the required sealing force. Generally a hardness range of Rc 30 to 40 will meet most requirements. The tightening force must be low enough to cause no galling in this range.

## Cost Considerations

Dryseal plugs are more frequently used, especially where reuse is frequent. Reason: more threads are engaged and they therefore resist leakage better. They are also preferred in soft metals to reduce of over-torquing.

## TYPES OF PRESSURE PLUG THREADS

Three thread forms are commonly used for pipe plugs and pressure plugs:

NPT: National Pipe thread, Tapered. This is the thread form commonly used for commercial pipe and fittings for low pressure applications. A lubricant and sealer are generally used.

ANPT: Aeronautical National Pipe thread, Tapered. Covered by MIL-S7105, this thread form was developed for aircraft use. It is basically the same as the NPT thread except that tolerances have been reduced about 50 percent. Plugs made with this thread should be used with lubricants and sealers. They are not to be used for hydraulic applications.

NPTF: National Pipe thread, Tapered, Fuel. This is the standard thread for pressure plugs. They make pressuretight joints without a sealant. Tolerances are about $1 / 4$ those for NPT threads. The standard which applies is ANSI B1.20.3. Applicable for fluid power applications.

## TAPER

## PRESSURE PLUGS

Deliberate difference in taper between the plug and the tapped hole. Ideal for use in assemblies where clearance is limited and in hydraulic lines near moving parts. Designed for use in hard materials and in thick-walled sections as well as for normal plug applications.


High pressure seal-Achieved through metal-to-metal contact at the large end of the plug. High load placed on the few mating threads near the top of the hole.


Flush seating—Design of LEVL-SEAL plug permits seating within half a pitch in a normally tapped hole. Conventional plugs have the greater tolerance of a full pitch and usually protrude above the surface.

## PTFE/TEFLON Coated LEVL-SEAL Type

Typical thickness is 0.0005 -inch LEVLSEAL precision coated with tough, corrosion-resistant PTFE/TEFLON.

Installation of the new plugs is faster with the coating of PTFE/TEFLON which acts as a lubricant as well as seal. Power equipment can be used to install the smaller sizes instead of the manual wrenching required by higher torques of un-coated plugs. Suited for in assembly line production.

Higher hydraulic and pneumatic working pressures can be effectively sealed. Seal is effective without use
of tapes or sealing compounds, even with liquids of very low viscosity. Unbrako Laboratories have tested these plugs with surges up to 13,500 psi 8 times in 5 minutes, then held peak pressure for 6 full hours without traceof leakage.

Flush seating improves appearance and adds safety. LEVL-SEAL plugs seat flush because of a combination of (1) gaging procedures, and (2) a deliberate difference in taper between the plug and a normally tapped NPTF hole. (The taper of the plug is $7 / 8^{\prime \prime}$ per foot, while that of the hole is $3 / 4^{\prime \prime}$ per foot.)

PTFE/TEFLON was selected for the coating material because of its


PTF fully formed Dryseal threads designed to achieve seal in tapped holes without need for sealing compounds.
combination of extra hardness and abrasion resistance which permit reuse up to 5 times without appre ciable loss of seal.

The coating is serviceable to $+450^{\circ} \mathrm{F}$ without deterioration.

Temperatures lower than $-100^{\circ} \mathrm{F}$ require the use of stainless steel plugs. These are available in the same range of sizes as the alloy steel plugs.

With no tape or sealing compound involved, there is no danger of foreign matter entering and contaminating the system or equipment. The coating reduces any tendency of the plug to "freeze" in the hole because of rust or corrosion.


## DIN 906



Precision thread for positive seal without sealing compound; controlled chamfer for faster starting.

## Mechanical Properties

Thread shall conform to DIN 158
Heat Treatment: 35-40 HRC
Product Dimensions

| Nom Dia | Pitch | Head Diameter A |  | $\begin{gathered} \text { Hex } \\ \text { Socket Size } \\ \text { W } \end{gathered}$ |  | Length |  | Socket Depth |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | max | min | max | min | max | min | min | Drill Size |
| M8 | 1 | 6.66 | 6.41 | 4.07 | 4.02 | 8.25 | 7.75 | 4.00 | 4.14 |
| M10 | 1 | 8.66 | 8.41 | 5.08 | 5.02 | 8.25 | 7.75 | 4.00 | 5.15 |
| M12 | 1.5 | 10.09 | 9.84 | 6.09 | 6.02 | 10.25 | 9.75 | 5.00 | 6.17 |
| M14 | 1.5 | 12.09 | 11.84 | 7.11 | 7.03 | 10.25 | 9.75 | 5.00 | 7.20 |
| M16 | 1.5 | 14.09 | 13.84 | 8.11 | 8.03 | 10.25 | 9.75 | 5.00 | 8.20 |
| M18 | 1.5 | 16.09 | 15.84 | 8.11 | 8.03 | 10.25 | 9.75 | 5.00 | 8.20 |
| M20 | 1.5 | 18.09 | 17.84 | 10.12 | 10.03 | 10.25 | 9.75 | 5.00 | 10.23 |
| M22 | 1.5 | 20.09 | 19.84 | 10.12 | 10.03 | 10.25 | 9.75 | 5.00 | 10.23 |
| M24 | 1.5 | 22.22 | 21.97 | 12.13 | 12.04 | 12.25 | 11.75 | 6.00 | 12.28 |
| M26 | 1.5 | 24.22 | 23.97 | 12.13 | 12.04 | 12.25 | 11.75 | 6.00 | 12.28 |
| M30 | 1.5 | 28.22 | 27.97 | 17.15 | 17.05 | 12.25 | 11.75 | 6.00 | 17.30 |



Features 3/4" taper. Precision thread for positive seal without sealing compound; controlled chamfer for faster starting.

Mechanical Properties
Heat Treatment: 35-40 HRC


Product Dimensions

| Plug Size | Threads per Inch | Head Diameter A |  | Hex <br> Socket Size W nom | Socket <br> Depth F min | Length |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | max | min |  |  | max | min |
| 1/8 | 28 | 0.329 | 0.319 | 0.1875 | 0.183 | 0.385 | 0.365 |
| 1/4 | 19 | 0.438 | 0.428 | 0.2500 | 0.245 | 0.510 | 0.490 |
| 3/8 | 19 | 0.578 | 0.568 | 0.3125 | 0.276 | 0.573 | 0.553 |
| 1/2 | 14 | 0.731 | 0.721 | 0.3750 | 0.339 | 0.698 | 0.678 |
| 5/8 | 14 | 0.808 | 0.798 | 0.5000 | 0.370 | 0.760 | 0.740 |
| 3/4 | 14 | 0.946 | 0.936 | 0.5625 | 0.370 | 0.823 | 0.803 |
| 7/8 | 14 | 1.098 | 1.088 | 0.5625 | 0.442 | 0.885 | 0.865 |
| 1 | 11 | 1.181 | 1.171 | 0.6250 | 0.558 | 1.010 | 0.990 |
| $11 / 4$ | 11 | 1.530 | 1.520 | 0.7500 | 0.677 | 1.260 | 1.240 |
| $11 / 2$ | 11 | 1.754 | 1.744 | 0.7500 | 0.677 | 1.260 | 1.240 |


| Plug <br> Size | $E$ <br> min | Socket <br> Drill <br> Size |
| ---: | :---: | :---: |
| $1 / 8$ | 0.076 | 0.1923 |
| $1 / 4$ | 0.107 | 0.2564 |
| $3 / 8$ | 0.139 | 0.3205 |
| $1 / 2$ | 0.170 | 0.3847 |
| $5 / 8$ | 0.170 | 0.5129 |
| $3 / 4$ | 0.232 | 0.5770 |
| $7 / 8$ | 0.232 | 0.5770 |
| 1 | 0.232 | 0.6400 |
| $11 / 4$ | 0.300 | 0.7680 |
| $11 / 2$ | 0.300 | 0.7680 |



Features $3 / 4^{\prime \prime}$ and $7 / 8^{\prime \prime}$ tapers. Dryseal thread for positive seal without sealing compound; controlled chamfer for faster starting

## Application Data

Unbrako recommends using a tapered reamer with corresponding size tap drill

## Notes

+With use of reamer (taper thread).
++ Without use of tapered reamer.
*Recommended torques for alloy steel only. Multiply by .65 for stainless steel and .50 for brass. NPTF fully formed Dryseal threads achieve seal in tapped holes without need for sealing compounds.

Product Dimensions

| Thread | Thread | Head Diameter | Hex <br> Socket Size |  | Length $( \pm .010)$ | Socket Depth |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| size <br> nom | per <br> Inch | A <br> ref | W nom | E $\min$ | $\stackrel{L}{\max }$ | F min |
| 1/16 | 27 | . 318 | . 156 | . 062 | . 312 | . 140 |
| 1/8 | 27 | . 411 | . 188 | . 062 | . 312 | . 140 |
| 1/4 | 18 | . 545 | . 250 | . 073 | . 437 | . 218 |
| 3/8 | 18 | . 684 | . 312 | . 084 | . 500 | . 250 |
| 1/2 | 14 | . 847 | . 375 | . 095 | . 562 | . 312 |
| 3/4 | 14 | 1.061 | . 562 | . 125 | . 625 | . 312 |
| 1 | 11 1/2 | 1.333 | . 625 | . 125 | . 750 | . 375 |
| $11 / 4$ | 11 1/2 | 1.679 | . 750 | . 126 | . 812 | . 437 |
| $11 / 2$ | 11 1/2 | 1.918 | 1.000 | . 156 | . 812 | . 437 |
| 2 | 11 1/2 | 2.395 | 1.000 | . 156 | . 875 | . 437 |


| Thread <br> size <br> nom | Tap <br> Drill <br> Size+ | Tap <br> Drill <br> Size++ | recommended <br> torque <br> in.-lbs* |
| ---: | ---: | ---: | :---: |
| $1 / 16$ | $15 / 64$ | $1 / 4$ | 150 |
| $1 / 8$ | $21 / 64$ | $11 / 32$ | 250 |
| $1 / 4$ | $27 / 64$ | $7 / 16$ | 600 |
| $3 / 8$ | $9 / 16$ | $37 / 64$ | 1200 |
| $1 / 2$ | $11 / 16$ | $23 / 32$ | 1800 |
| $3 / 4$ | $57 / 64$ | $59 / 64$ | 3000 |
| 1 | $11 / 8$ | $15 / 32$ | 4200 |
| $11 / 4$ | 37.5 mm | - | 5400 |
| $11 / 2$ | 43.5 mm | - | 6900 |
| 2 | $23 / 16$ | - | 8500 |



Levl-seal features: controlled $7 / 8^{\prime \prime}$ taper in $3 / 4^{\prime \prime}$ taper hole seats plug level, flush with surface within $1 / 2$ pitch.

## Mechanical Properties

1. Material: ASTM A574 alloy steel, austenitic stainless steel or brass.
2. Hardness: Rc 35-40 for steel.
3. DRY-SEAL and LEVL-SEAL: Small end of plug to be flush with face of standard NPTF ring gages within one thread (L1, L2 and tapered ring). Large end of plug to be flush with face of special 7/8 taper ring gages within one-half thread.
4. Undercut in socket at mfrs. option
5. Six equally spaced identification grooves
(1/16-27 plug to have 3 identification grooves)
on alloy steel plugs. (LEVL-SEAL)
6. Dimensions apply before plating and/or coating.

## Notes

* for taper thread (using tapered reamer)
** Maximum for PTFE / Teflon-coated but can be reduced as much as $60 \%$ in most applications.

Size Part No. $\bigoplus$| Ibs |
| :---: |
| $/ 1000$ |

DIN906.22 - Grade 5.8

| M8 (1.0) | 402218 | 100 | 4.40 |
| ---: | ---: | ---: | ---: |
| M10 (1.0) | 402219 | 100 | 7.48 |
| M12 (1.5) | 402220 | 100 | 14.08 |
| M16 (1.5) | 402221 | 100 | 24.20 |
| M18 (1.5) | 402222 | 100 | 35.20 |
| M20 (1.5) | 402223 | 100 | 38.72 |
| M22 (1.5) | 402224 | 100 | 46.20 |

## Taper Pressure Plugs - Inch



| Size | Part No. | 5 | $\begin{aligned} & \text { lbs } \\ & / 1000 \end{aligned}$ | Size | Part No. | $\theta$ | $\begin{gathered} \text { lbs } \\ / 1000 \end{gathered}$ | Size | Part No. | 4 | $\begin{aligned} & \text { lbs } \\ & / 1000 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BSPT 3/4"Taper Alloy Steel |  |  |  | NPTF 3/4"Taper / Dryseal Brass |  |  |  | NPTF 7/8"Taper / LEVL - SEAL Teflon Coated |  |  |  |
| 1/8-28 | 402208 | 200 | 9.31 | 1/16-27 | 102940 | 100 | 3.96 | 1/16-27 | 796087 | 100 | 3.08 |
| 1/4-19 | 402209 | 200 | 22.33 | 1/8-27 | 103266 | 100 | 9.90 | 1/8-27 | 138240 | 100 | 5.94 |
| 3/8-19 | 402210 | 100 | 41.51 | 1/4-18 | 103164 | 100 | 18.92 | 1/4-18 | 138241 | 100 | 18.33 |
| 1/2-14 | 402211 | 100 | 75.90 | 3/8-18 | 103072 | 100 | 37.84 | 3/8-18 | 796086 | 100 | 29.04 |
| 5/8-14 | 402212 | 50 | 99.51 |  |  |  |  | 1/2-14 | 138243 | 50 | 53.68 |
| 3/4-14 | 402213 | 50 | 150.15 | NPTF 3/4"Taper / Dryseal Stainless 304 |  |  |  | 3/4-14 | 796088 | 50 | 72.60 |
| 1-11 | 402214 | 25 | 294.47 | 1/16-27 | 102262 | 100 | 3.96 | 1-11.5 | 796089 | 25 | 88.00 |
| 1 1/4-11 | 402215 | 25 | 598.40 | 1/8-27 | 102182 | 100 | 10.12 | 11/4-11.5 | 796090 | 25 | 110.00 |
| $11 / 2-11$ | 402216 | 25 | 756.80 | 1/4-18 | 102076 | 100 | 18.92 |  |  |  |  |
|  |  |  |  | 3/8-18 | 110890 | 100 | 59.84 | NPTF 7/8"Taper / LEVL - SEAL Brass |  |  |  |
| NPTF 3/4"Taper / Dryseal Alloy Steel |  |  |  | 1/2-14 | 110779 | 50 | 84.04 | 1/16-27 | 134502 | 100 | 3.08 |
| 1/16-27 | 117052 | 100 | 4.40 |  |  |  |  | 1/8-27 | 134503 | 100 | 5.94 |
| 1/8-27 | 117068 | 100 | 11.00 | NPTF 7/8"Taper / LEVL - SEAL Alloy Steel |  |  |  | 1/4-18 | 134504 | 100 | 15.84 |
| 1/4-18 | 117084 | 100 | 19.18 | 1/16-27 | 107577 | 100 | 3.08 | 3/8-18 | 134505 | 100 | 28.82 |
| 3/8-18 | 118963 | 100 | 37.40 | 1/8-27 | 107593 | 100 | 5.94 | 1/2-14 | 134506 | 50 | 57.64 |
| 1/2-14 | 103846 | 50 | 61.60 | 1/4-18 | 105766 | 100 | 16.28 |  |  |  |  |
| 3/4-14 | 103747 | 50 | 101.64 | 3/8-18 | 105782 | 100 | 29.04 | NPTF 7/8" Taper / LEVL- SEAL Stainless 304 |  |  |  |
| 1-11.5 | 103644 | 25 | 202.40 | 1/2-14 | 112286 | 50 | 53.68 | 1/8-27 | 183840 | 100 | 5.94 |
| 1 1/4-11.5 | 103588 | 25 | 360.80 | 3/4-14 | 109168 | 50 | 85.80 | 1/4-18 | 183538 | 100 | 15.84 |
|  |  |  |  | 1-11.5 | 109184 | 50 | 167.20 |  |  |  |  |
|  |  |  |  | $11 / 4-11.5$ | 109201 | 50 | 286.00 |  |  |  |  |

## Pins

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## Its about

## Time

# \& Money... 

whether you're an engineer or purchase manager,
Unbrako has fastening solutions to save you time \& help increase revenue.

## DOWEL

Surface hardness: Rockwell "C" 60 minimum
Surface finish: 8 micro inch maximum Core hardness: Rockwell "C" 50-58 Case depth: .020-inch minimum Shear strength: 150,000 psi (calculated based on conversion from hardness)
Heat treated alloy steel for strength and toughness Held to precise tolerance by automatic gaging and electronic feed-back equipment
Material, Heat Treatment, Dimensions: ASME B18.8.2 .0002 - inch oversize typically used for first installation. . 0010 - inch oversize typically used after hole enlarges.


## Installation Warning -

 Do not strike. Use safety shield or glasses when pressing chamfered end in first.

Continuous grain flow resists
chipping of ends. Precision heat treated for greater strength and surface hardness.
Chamfered end provides easier insertion in hole. Surface finish to 8 microinch maximum.


Formed ends, controlled heat treat; close tolerances; standard for die work; also used as bearings, gages, precision parts, etc.

## Mechanical Properties

Specifications: ANSI B18.8.5M, ISO
8734 or DIN 6325.
Material: ANSI B18.85-alloy steel
Hardness: Rockwell C60 minimum (surface)
Rockwell C 50-58 (core)
Shear Stress: Calculated values based on 1050 MPa.
Surface Finish: 0.2 micrometer maximum

## Application Data

calculated
single shear Recommended Nominal strength

| Nominal | strength |  |  | hole size |  |
| :---: | ---: | ---: | :--- | :--- | :--- |
| Size |  | kN | lbs |  | max |
| Sonnn | min |  |  |  |  |
| 3 | 7.4 | 1,670 |  | 3.000 | 2.987 |
| 4 | 13.2 | 2,965 |  | 4.000 | 3.987 |
| 5 | 20.6 | 4,635 |  | 5.000 | 4.987 |
| 6 | 29.7 | 6,650 |  | 6.000 | 5.987 |
| 8 | 52.5 | 11,850 |  | 8.000 | 7.987 |
| 10 | 82.5 | 18,550 |  | 10.000 | 9.987 |
| 12 | 119.0 | 26,700 |  | 12.000 | 11.985 |
| 16 | 211.0 | 47,450 |  | 16.000 | 15.985 |
| 20 | 330.0 | 74,000 |  | 20.000 | 19.983 |
| 25 | 515.0 | 116,000 |  | 25.000 | 24.983 |

## Warning

Installation warning: Dowel pins should not be installed by striking or hammering.
Wear safety glasses or shield when pressing chamfered point end first.


Product Dimensions

| Size <br> nom | Pin diameter |  | Point diameter |  | Crown height C max | Crown radius R min |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | max | A min | max | min |  |  |
| 3 | 3.008 | 3.003 | 2.9 | 2.6 | 0.8 | 0.3 |
| 4 | 4.009 | 4.004 | 3.9 | 3.6 | 0.9 | 0.4 |
| 5 | 5.009 | 5.004 | 4.9 | 4.6 | 1.0 | 0.4 |
| 6 | 6.010 | 6.004 | 5.8 | 5.4 | 1.1 | 0.4 |
| 8 | 8.012 | 8.006 | 7.8 | 7.4 | 1.3 | 0.5 |
| 10 | 10.012 | 10.006 | 9.8 | 9.4 | 1.4 | 0.6 |
| 12 | 12.013 | 12.007 | 11.8 | 11.4 | 1.6 | 0.6 |
| 16 | 16.013 | 16.007 | 15.8 | 15.3 | 1.8 | 0.8 |
| 20 | 20.014 | 20.008 | 19.8 | 19.3 | 2.0 | 0.8 |
| 25 | 25.014 | 25.008 | 24.8 | 24.3 | 2.3 | 1.0 |


| Size | Part No. | $6$ | $\begin{gathered} \text { lbs } \\ / 1000 \end{gathered}$ | Size | Part No. | $8$ | $\begin{aligned} & \text { lbs } \\ & / 1000 \end{aligned}$ | Size | Part No. | $\theta$ | $\begin{aligned} & \text { lbs } \\ & \text { /1000 } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 mm |  |  |  | 6 mm |  |  |  | 16 mm |  |  |  |
| $2 \times 8$ | 407831 | 40 | 0.43 | $6 \times 18$ | 402143 | 40 | 8.79 | $16 \times 32$ | 406218 | 20 | 110.00 |
| 10 | 407832 | 40 | 0.54 | 20 | 115034 | 40 | 9.77 | 40 | 406220 | 20 | 138.89 |
| 12 | 407833 | 40 | 0.65 | 24 | 115037 | 40 | 11.72 | 70 | 406225 | 20 | 243.06 |
| 16 | 407835 | 40 | 0.87 | 28 | 402145 | 40 | 13.67 | 80 | 406226 | 20 | 277.79 |
| 18 | 407836 | 40 | 0.98 | 30 | 115038 | 40 | 14.65 | 90 | 406227 | 20 | 312.51 |
| 20 | 407837 | 40 | 1.08 | 32 | 402146 | 40 | 15.63 | Note: <br> - Unbrako Dowel Pins are through hardened a precision ground from nominal to 0.0002 " ov size on Inch sizes and a surface finish of 0.15 micrometers max, on both Metric and Inch products. <br> - CAUTION: Unbrako advises that correct tools should be used for the application. <br> - Safety goggles should be worn for your security and protection. |  |  |  |
|  |  |  |  | 36 | 406348 | 40 | 17.58 |  |  |  |  |
|  | 3 m |  |  | 40 | 115043 | 40 | 19.53 |  |  |  |  |
| $3 \times 10$ | 115001 | 40 | 1.22 | 45 | 115044 | 40 | 21.97 |  |  |  |  |
| 12 | 115002 | 40 | 1.47 | 50 | 115046 | 40 | 24.42 |  |  |  |  |
| 16 | 115003 | 40 | 1.95 | 60 | 115047 | 40 | 29.30 |  |  |  |  |
| 18 | 402118 | 40 | 2.20 |  |  |  |  |  |  |  |  |
| 20 | 115004 | 40 | 2.44 | 8 mm |  |  |  |  |  |  |  |
| 28 | 402120 | 40 | 3.42 | $8 \times 20$ | 115049 | 40 | 17.36 |  |  |  |  |
| 30 | 115007 | 40 | 3.66 | 24 | 406349 | 40 | 20.83 |  |  |  |  |
| 32 | 402121 | 40 | 3.91 | 28 | 402150 | 40 | 24.31 |  |  |  |  |
| 36 | 406345 | 40 | 4.40 | 30 | 115053 | 40 | 26.04 |  |  |  |  |
| 40 | 402124 | 40 | 4.89 | 32 | 402151 | 40 | 27.78 |  |  |  |  |
|  |  |  |  | 36 | 406350 | 40 | 31.25 |  |  |  |  |
| 4 mm |  |  |  | 40 | 115055 | 40 | 34.72 |  |  |  |  |
| $4 \times 10$ | 115010 | 40 | 2.17 | 45 | 115056 | 40 | 39.06 |  |  |  |  |
| 12 | 115011 | 40 | 2.60 | 50 | 115057 | 40 | 43.40 |  |  |  |  |
| 16 | 115012 | 40 | 3.47 | 55 | 402153 | 40 | 47.74 |  |  |  |  |
| 20 | 115015 | 40 | 4.34 | 60 | 115058 | 40 | 52.09 |  |  |  |  |
| 24 | 407127 | 40 | 5.21 |  |  |  |  |  |  |  |  |
| 25 | 115016 | 40 | 5.43 | 10 mm |  |  |  |  |  |  |  |
| 28 | 402128 | 40 | 6.05 | $10 \times 20$ | 115063 | 40 | 27.13 |  |  |  |  |
| 30 | 115017 | 40 | 6.51 | 24 | 406351 | 40 | 32.55 |  |  |  |  |
| 50 | 402132 | 40 | 10.85 | 30 | 115066 | 40 | 40.69 |  |  |  |  |
|  |  |  |  | 36 | 406352 | 40 | 48.83 |  |  |  |  |
| 5 mm |  |  |  | 40 | 115070 | 40 | 54.26 |  |  |  |  |
| $5 \times 10$ | 402133 | 40 | 3.39 | 45 | 115071 | 40 | 61.04 |  |  |  |  |
| 12 | 115021 | 40 | 4.07 | 50 | 402161 | 40 | 67.82 |  |  |  |  |
| 14 | 402134 | 40 | 4.75 | 60 | 402163 | 40 | 81.38 |  |  |  |  |
| 16 | 115022 | 40 | 5.43 | 70 | 402164 | 40 | 94.60 |  |  |  |  |
| 20 | 115024 | 40 | 6.78 | 90 | 402167 | 40 | 122.07 |  |  |  |  |
| 24 | 407128 | 40 | 8.14 | 100 | 402169 | 40 | 135.64 |  |  |  |  |
| 25 | 115025 | 40 | 8.48 |  |  |  |  |  |  |  |  |
| 28 | 402137 | 40 | 9.50 | 12 mm |  |  |  |  |  |  |  |
| 30 | 115026 | 40 | 10.17 | $12 \times 24$ | 406353 | 40 | 46.88 |  |  |  |  |
| 32 | 402138 | 40 | 10.85 | 30 | 402174 | 40 | 58.59 |  |  |  |  |
| 36 | 406347 | 40 | 12.21 | 36 | 406354 | 40 | 70.31 |  |  |  |  |
| 40 | 115028 | 40 | 13.56 | 40 | 402178 | 40 | 78.13 |  |  |  |  |
| 45 | 115029 | 40 | 15.26 | 50 | 402180 | 40 | 97.66 |  |  |  |  |
| 50 | 115031 | 40 | 16.96 | 60 | 402182 | 40 | 117.19 |  |  |  |  |
|  |  |  |  | 70 | 402183 | 40 | 136.72 |  |  |  |  |
| 6 mm |  |  |  | 80 | 402184 | 40 | 156.26 |  |  |  |  |
| $6 \times 12$ | 402141 | 40 | 5.86 | 90 | 402185 | 40 | 175.79 |  |  |  |  |
| 16 | 115032 | 40 | 7.81 | 100 | 402186 | 40 | 195.32 |  |  |  |  |



Formed ends, controlled heat treat; close tolerances; standard for die work; also used as bearings, gages, precision parts, etc.

Mechanical Properties
Material: ASME B18.8.2
Shear Hardness: 150,000 psi
Surface Hardness: 60 HRC
Core Hardness: 50-58 HRC
Shear Strength and
Recommended hole Size

| Nominal | calculated single shear strength | Recommendedhole size(.0002 over nom.) |  |
| :---: | :---: | :---: | :---: |
| Size | (pounds) | max | min |
| 1/16 | 465 | . 0625 | . 0620 |
| 3/32 | 1,035 | . 0937 | . 0932 |
| 1/8 | 1,845 | . 1250 | . 1245 |
| 5/32 | 2,880 | . 1562 | . 1557 |
| 3/16 | 4,140 | . 1875 | . 1870 |
| 1/4 | 7,370 | . 2500 | . 2495 |
| 5/16 | 11,500 | . 3125 | . 3120 |
| 3/8 | 16,580 | . 3750 | . 3745 |
| 7/16 | 22,540 | . 4375 | . 4370 |
| 1/2 | 29,460 | . 5000 | . 4995 |
| 9/16 | 37,270 | . 5625 | . 5620 |
| 5/8 | 46,020 | . 6250 | . 6245 |
| 3/4 | 66,270 | . 7500 | . 7495 |
| 7/8 | 90,190 | . 8750 | . 8745 |
| 1 | 117,810 | 1.0000 | . 9995 |

## Warning

Installation warning: Do not strike.
Use safety shield or glasses when pressing chamfered end in first.


Product Dimensions

| Size nom | Pin diameter A |  | Point diameter B max | Q |  | Crown radius R min |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} .0002 \text { o } \\ \max \end{gathered}$ | ver nom. min |  | max | $Q_{\text {min }}$ |  |
| 1/16 | . 0628 | . 0626 | 0.056 | 0.056 | 0.019 | 0.010 |
| 3/32 | . 0941 | . 0939 | 0.084 | 0.074 | 0.028 | 0.026 |
| 1/8 | . 1253 | . 1251 | 0.116 | 0.070 | 0.026 | 0.043 |
| 5/32 | . 1565 | . 1563 | 0.147 | 0.071 | 0.026 | 0.043 |
| 3/16 | . 1878 | . 1876 | 0.178 | 0.073 | 0.027 | 0.043 |
| 1/4 | . 2503 | . 2501 | 0.237 | 0.093 | 0.037 | 0.058 |
| 5/16 | . 3128 | . 3126 | 0.298 | 0.102 | 0.041 | 0.058 |
| 3/8 | . 3753 | . 3751 | 0.359 | 0.110 | 0.046 | 0.073 |
| 7/16 | . 4378 | . 4376 | 0.417 | 0.136 | 0.058 | 0.089 |
| 1/2 | . 5003 | . 5001 | 0.480 | 0.133 | 0.057 | 0.104 |
| 9/16 | . 5628 | . 5626 | 0.542 | 0.136 | 0.058 | 0.120 |
| 5/8 | . 6253 | . 6251 | 0.605 | 0.133 | 0.057 | 0.120 |
| 3/4 | . 7503 | . 7501 | 0.725 | 0.161 | 0.071 | 0.120 |
| 7/8 | . 8753 | . 8751 | 0.850 | 0.161 | 0.071 | 0.120 |
| 1 | 1.0003 | 1.0001 | 0.975 | 0.161 | 0.071 | 0.120 |


| Size | Part No. | $5$ | $\begin{aligned} & \text { lbs } \\ & / 1000 \end{aligned}$ | Size | Part No. | $8$ | $\begin{aligned} & \text { lbs } \\ & / 1000 \end{aligned}$ | Size | Part No. | $8$ | $\begin{aligned} & \text { lbs } \\ & / 1000 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/8" |  |  |  | 3/8" |  |  |  | $3 / 4^{\prime \prime}$ |  |  |  |
| 1/8" $\times 3 / 8$ | 116081 | 40 | 1.67 | $3 / 8^{\prime \prime} \times 1 / 2$ | 117593 | 40 | 19.80 | $3 / 4 \prime \times 2$ | 106412 | 10 | 250.05 |
| 1/2 | 116097 | 40 | 1.74 | 5/8 | 109422 | 40 | 22.55 | $21 / 2$ | 106444 | 10 | 334.40 |
| 5/8 | 116113 | 40 | 2.17 | 3/4 | 109454 | 40 | 31.26 | 3 | 106477 | 10 | 375.08 |
| 3/4 | 116129 | 40 | 2.60 | 7/8 | 109486 | 40 | 32.45 | $31 / 2$ | 106509 | 10 | 462.00 |
| 7/8 | 116146 | 40 | 4.95 | 1 | 109520 | 40 | 35.20 | 4 | 113456 | 10 | 500.11 |
| 1 | 116162 | 40 | 3.47 | $11 / 4$ | 114998 | 40 | 39.07 | 5 | 113521 | 10 | 625.14 |
| $11 / 4$ | 116179 | 40 | 4.34 | $11 / 2$ | 115030 | 40 | 46.89 | 6 | 111925 | 10 | 770.00 |
| $11 / 2$ | 116195 | 40 | 4.95 | $13 / 4$ | 115062 | 40 | 54.70 |  |  |  |  |
| $13 / 4$ | 110261 | 40 | 10.45 | 2 | 113097 | 40 | 62.51 | 7/8" |  |  |  |
| 2 | 110277 | 40 | 12.65 | $21 / 4$ | 109028 | 40 | 75.90 | 7/8" $\times 2$ | 111958 | 10 | 374.00 |
|  |  |  |  | $21 / 2$ | 111888 | 40 | 84.70 | 3 | 108424 | 10 | 539.00 |
| 3/16" |  |  |  | 3 | 107654 | 40 | 93.77 | 4 | 108490 | 10 | 704.00 |
| $3 / 16^{\prime \prime} \times 1 / 2$ | 110293 | 40 | 3.91 |  |  |  |  | 5 | 102900 | 10 | 858.00 |
| 5/8 | 110310 | 40 | 4.88 | 7/16" |  |  |  |  |  |  |  |
| 3/4 | 110327 | 40 | 5.86 | 7/16" $\times 1$ | 107686 | 20 | 49.50 | $1 "$ |  |  |  |
| 7/8 | 110344 | 40 | 7.70 | $11 / 4$ | 107718 | 20 | 59.40 | 1"x 2 | 102968 | 10 | 444.54 |
| 1 | 110360 | 40 | 7.81 | $11 / 2$ | 113240 | 20 | 70.40 | $21 / 2$ | 107094 | 10 | 552.00 |
| $11 / 4$ | 110376 | 40 | 9.90 | $13 / 4$ | 107457 | 20 | 84.70 | 3 | 107126 | 10 | 710.60 |
| $11 / 2$ | 110393 | 40 | 12.65 | 2 | 107489 | 20 | 94.60 | $31 / 2$ | 104251 | 10 | 777.95 |
| $13 / 4$ | 110410 | 40 | 14.85 | $21 / 2$ | 107521 | 20 | 114.40 | 4 | 104317 | 10 | 924.00 |
| 2 | 110426 | 40 | 17.60 | 3 | 107553 | 20 | 134.20 | 5 | 108138 | 10 | 1067.00 |


| 1/4" |  |  |  | 1/2" |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/4" $\times 1 / 2$ | 104185 | 40 | 10.42 | 1/2" $\times 3 / 4$ | 117073 | 20 | 41.68 |
| 5/8 | 115069 | 40 | 9.90 | 1 | 119158 | 20 | 55.57 |
| 3/4 | 113104 | 40 | 10.42 | $11 / 4$ | 114656 | 20 | 80.30 |
| 7/8 | 105237 | 40 | 13.75 | $11 / 2$ | 114721 | 20 | 90.20 |
| 1 | 108942 | 40 | 13.89 | $13 / 4$ | 117103 | 20 | 104.50 |
| $11 / 4$ | 108974 | 40 | 17.36 | 2 | 106609 | 20 | 111.14 |
| $11 / 2$ | 105277 | 40 | 20.84 | $21 / 4$ | 119565 | 20 | 134.20 |
| $13 / 4$ | 105309 | 40 | 23.96 | $21 / 2$ | 119597 | 20 | 138.92 |
| 2 | 105341 | 40 | 24.31 | 3 | 119631 | 20 | 174.90 |
| $21 / 4$ | 118645 | 40 | 33.00 | $31 / 2$ | 109023 | 20 | 194.49 |
| $21 / 2$ | 120490 | 40 | 37.40 | 4 | 111884 | 20 | 222.27 |

Note:

- Unbrako Dowel Pins are through hardened and precision ground from nominal to 0.0002 " over size on Inch sizes and a surface finish of 0.15 micrometers max, on both Metric and Inch products.
- CAUTION: Unbrako advises that correct tools should be used for the application.
- Safety goggles should be worn for your security and protection.

| 5/16" |  |  |  | 5/8" |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $5 / 16^{\prime \prime} \times 1 / 2$ | 120557 | 40 | 12.65 | 5/8" $\times 1$ | 107650 | 10 | 86.83 |
| 5/8 | 120621 | 40 | 14.85 | $11 / 4$ | 107682 | 10 | 110.00 |
| 3/4 | 117265 | 40 | 16.28 | 11/2 | 107714 | 10 | 173.65 |
| 7/8 | 117298 | 40 | 18.99 | $13 / 4$ | 121862 | 10 | 160.70 |
| 1 | 117331 | 40 | 21.71 | 2 | 107453 | 10 | 189.20 |
| $11 / 4$ | 117363 | 40 | 29.70 | $21 / 4$ | 107485 | 10 | 209.00 |
| $11 / 2$ | 117397 | 40 | 35.20 | $21 / 2$ | 107517 | 10 | 217.06 |
| $13 / 4$ | 117429 | 40 | 42.35 | 3 | 107549 | 10 | 268.40 |
| 2 | 117462 | 40 | 43.41 | $31 / 2$ | 107582 | 10 | 310.20 |
| $21 / 4$ | 117494 | 40 | 48.84 | 4 | 107614 | 10 | 358.60 |
| $21 / 2$ | 117527 | 40 | 59.95 | $41 / 2$ | 113268 | 10 | 409.20 |
| 3 | 117561 | 40 | 69.85 | 5 | 113300 | 10 | 440.00 |

## PULL-OUT DOWEL PINS

## 5 WAYS TO SAVE <br> UNBRAKO Pull-Out Dowel Pins are easier, more accurate and more economical than "do-it-your-self" modifications of standard dowels. They save you money FIVE ways:

## 1. YOU SAVE COST OF SEPARATE KNOCK-OUT HOLES IN BLIND HOLES WHERE PINS MUST BE REMOVED.

UNBRAKO pull-out pins are easy to install in blind holes, easy to remove. Exclusive spiral grooves release trapped air for insertion or removal without danger of holescoring.


#### Abstract

4. YOU SAVE MODIFICATIONS COSTS, YOU AVOID HEADACHES AND YOU SAVE YOUR SKILLED PEOPLE FOR PROFITABLE WORK. UNBRAKO pull-out dowel pins have tapped holes and relief grooves built in. Time-consuming "do-it-yourself" modification of standard pin eliminated. No need for annealing (to make pins soft enough to drill and tap) and re-hardening, which can result in damage to finish, and in inaccuracies and distortion.


5. YOU SAVE TIME AND MONEY BECAUSE OF THIS QUALITY "REPEATABILITY". NO SPECIAL PREPARATION OF INDIVIDUAL HOLES NEEDED-

## 2. YOU MUST SAVE COST OF NEW PINS EACH TIME DIE IS SERVICED OR DISMANTLED.

 UNBRAKO pull-out dowel pins are reusable. The hole tapped in one end for a removal screw or threaded "puller" makes it easy and fast to remove the pin without damage to pin or hole, permits repeated re-use.
## 3. YOU SAVE MONEY IN REDUCED DOWNTIME AND LOSS OF PRODUCTION

UNBRAKO pull-out dowel pins speed up die servicing and reworking. You can remove
them without turning the die over, and you can take out individual sections of the die for rework or service without removing entire die assembly from the press. .

YOU CAN BE SURE OF ACCURATE FIT EVERY TIME.

UNBRAKO pull-out dowel pins are identical and interchangeable with standard UNBRAKO dowels. They have the same physical, finish, accuracy and tolerances. And they are consistently uniform. Their exclusive spiral relief grooves provide more uniform grooves provide more uniform
relief than other types of removable pins, assuring more uniform pull-out values. pull


You don't need any special tools to remove UNBRAKO pull-out dowels-just an ordinary die hook and a socket head cap or button head socket screw.

## FEATURES

Formed ends resist chipping

Exclusive spiral grooves afford uniform relief for insertion and removal, reduce chances of hole-scoring

Surface hardness-Rockwell C60 minimum Surface finish-8 micro inch maximum Core hardness-Rockwell C 50-58

Shear strength: 150,000 psi (calculated based on conversion from hardness)

Heat treated alloy steel for strength and toughness

Held to precise tolerance


For use in blind holes. Easily removed without special tools. Reusable, Saves money. No need for knock-out holes. Same physicals \& finish as standard Unbrako dowel pins.

Mechanical Properties
Material and Heat Treatment: ASME B18.8.2
Length equal to shorter than 'p' max values may be drilled through

Shear Strength and
Recommended hole Size

| Nominal | Single Shear <br> Strength (lbs) |  | Recommended <br> hole diameter <br> Size |  | ref. |
| ---: | :---: | :---: | :---: | :---: | :---: |
| $1 / 4$ | 7,370 | .2500 | .2495 |  |  |
| $5 / 16$ | 11,500 | .3125 | .3120 |  |  |
| $3 / 8$ | 16,580 | .3750 | .3745 |  |  |
| $7 / 16$ | 22,540 | .4370 | .4315 |  |  |
| $1 / 2$ | 29,460 | .5000 | .4995 |  |  |
| $5 / 8$ | 46,020 | .6250 | .6245 |  |  |
| $3 / 4$ | 66,270 | .7500 | .7495 |  |  |
| $7 / 8$ | 90,190 | .8750 | .8745 |  |  |
| 1 | 117,810 | 1.0000 | .9995 |  |  |


| Size | Part No. | lbs |
| ---: | ---: | ---: |
|  | $1 / 4^{\prime \prime}(\# 8-32$ | UNC) |
| $1 / 4^{\prime \prime} \times 3 / 4$ | 138431 | 40 |
| 1 | 138433 | 40 |
| $11 / 4$ | 138434 | 40 |
| $11 / 2$ | 138436 | 40 |
| $13 / 4$ | 138437 | 40 |
| 2 | 138438 | 40 |
| $21 / 2$ | 138440 | 40 |


| Size | Part No. | lbs <br> $/ 1000$ |
| ---: | :--- | :---: |
|  | $5 / 8^{\prime \prime}(1 / 4-20$ |  |
| $5 / 8^{\prime \prime} \times 11 / 2$ | 138469 | 20 |
| 2 | 138471 | 20 |
| $21 / 4$ | 138472 | 10 |
| $21 / 2$ | 138473 | 10 |
| 3 | 138474 | 10 |
| 4 | 138476 | 10 |


| $5 / 16^{\prime \prime}(\# 10-32$ UNF) |  |  |  |
| ---: | :---: | :---: | :---: |
| $5 / 16^{\prime \prime} \times 3 / 4$ | 138441 | 40 | 17.60 |
| 1 | 138443 | 40 | 24.75 |
| $11 / 4$ | 138444 | 40 | 29.70 |
| $11 / 2$ | 138445 | 40 | 35.20 |
| 2 | 138447 | 40 | 47.30 |
| $21 / 4$ | 138448 | 40 | 51.15 |
| $21 / 2$ | 138449 | 40 | 59.95 |


| $3 / 4^{\prime \prime} \times 2$ | 138477 | 10 | 268.4 |
| ---: | :---: | :---: | :---: |
| $21 / 2$ | 138478 | 10 | 334.4 |
| 3 | 138479 | 10 | 398.2 |
| 4 | 138480 | 10 | 528.0 |
|  |  |  |  |
| $1^{\prime \prime}(3 / 8-16$ UNC) |  |  |  |
| $1 " \times$ | 2 | 138481 | 10 |
| $21 / 2$ | 138482 | 10 | 579.6 |
| 3 | 138483 | 10 | 710.6 |
| 4 | 138485 | 10 | 850.7 |



With up to 9 months inventory cover for standard products More than 3,000 categories of High Tensile Alloy and Stainless Steel Industrial Fasteners are just a call away!

# Unbrako 

## Wrenches \& Tools

Page Contents
92 Hexagon Wrenches - Metric
94 Hexagon Wrenches - Inch

## Its abo Safety

 \& Reliability...Using unbrako tools says a lot:
You're proud,
You're professional, You don't cut corners.

## HEXAGON WRENCHES

Square cut end engages the socket full depth for better tightening of screw ANSI B18．3


Accurately sized across flats and corners to insure snug fit and full wall contact

Heat treated alloy steel－key is hard，tough and ductile clear through for longer life and retention of dimensional accuracy


## Why Unbrako wrenches are Safer ？

An UNBRAKO key is not an ordinary hexagon key－it is a precision inter－ nal wrenching tool of great strength and ductility．With an UNBRAKO key， far more tightening torque than is needed can be applied without damaging the screw or the key，and it can be done safely．This is an important feature，especially true of the smaller sizes（ $5 / 32^{\prime \prime}$ and under） which are normally held in the hand．

Photographs of a destruction test show what we mean．Under exces－ sive torque a 5／64＂UNBRAKO key twists but does not shear until a torque has been reached that is approximately $20 \%$ greater than can be applied with an ordinary key．At his point it shears off clean，flush with the top of the socket，leaving no jagged edge to gash a hand．

Still the UNBRAKO screw has not been harmed．The broken piece of the key is not wedged into the socket．It can be lifted out with a small magnet，convincing proof that the socket has not been reamed or otherwise damaged．

NOTE：The use of an extension in these illustrations is for demon－ stration purposes only．The manu－ facturer does not recommend the use of extensions with any hex key product under normal conditions．


The socket hasn＇t been reamed or damaged．Broken section can be lifted out with a magnet．


Tough, ductile, for high torqueing; accurate fit in all types of socket screws; size marked for quick identity

## Mechanical Properties

1. Material: ASME B18.3.2.M Alloy Steel
2. Dimensions: B18.3.2M
3. Similar Standards: ISO 2936 AND BS4168
4. Unbrako Long arm similar to ISO extra long
5. Please specify standard required at time of purchase.


Product Dimensions

| Size <br> nom. | Width Across Flats W |  | A |  | Unbrako / ASME Short B |  | Unbrako Long B |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | max. | min. | max. | min. | max. | min. | max. | min. |
| 0.71 | 0.711 | 0.698 | 5.5 |  | 31 |  |  |  |
| 0.89 | 0.889 | 0.876 | 9 |  | 31 |  |  |  |
| 1.27 | 1.270 | 1.244 | 13.5 |  | 42 |  |  |  |
| 1.5 | 1.500 | 1.470 | 14 | 13 | 45 | 43 | 90 | 88 |
| 2.0 | 2.000 | 1.970 | 16 | 15 | 50 | 48 | 100 | 98 |
| 2.5 | 2.500 | 2.470 | 18 | 17 | 56 | 53 | 112 | 109 |
| 3.0 | 3.000 | 2.955 | 20 | 19 | 63 | 60 | 126 | 123 |
| 4.0 | 4.000 | 3.955 | 25 | 24 | 70 | 66 | 142 | 138 |
| 5.0 | 5.000 | 4.955 | 28 | 27 | 80 | 76 | 160 | 156 |
| 6.0 | 6.000 | 5.955 | 32 | 30 | 90 | 86 | 180 | 176 |
| 8.0 | 8.000 | 7.955 | 36 | 34 | 100 | 95 | 200 | 195 |
| 10.0 | 10.000 | 9.955 | 40 | 38 | 112 | 106 | 224 | 218 |
| 12.0 | 12.000 | 11.955 | 45 | 43 | 125 | 119 | 250 | 244 |
| 14.0 | 14.000 | 13.930 | 55 | 53 | 140 | 133 | 280 | 273 |
| 17.0 | 17.000 | 16.930 | 63 | 60 | 160 | 152 | 320 | 312 |
| 19.0 | 19.000 | 18.930 | 70 | 67 | 180 | 171 | 360 | 351 |
| 22.0 | 22.000 | 21.930 | 80 | 76 | 200 | 190 | 400 | 390 |
| 24.0 | 24.000 | 23.930 | 90 | 86 | 224 | 213 | 448 | 437 |
| 27.0 | 27.000 | 26.820 | 100 | 96 | 250 | 238 | 500 | 488 |
| 32.0 | 32.000 | 31.820 | 125 | 121 | 315 | 300 | 630 | 615 |
| 36.0 | 36.000 | 35.820 | 140 | 135 | 355 | 338 | 710 | 693 |


| Size nom. | ASME Long B |  | Torsional Shear Strength Minimum |  | Torsional Yield Strength Minimum |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | max. | min. | N-m | In-lbs. | N-m | In-lbs. |
| 0.71 | 69 |  | 0.12 | 1.1 | 0.1 | 0.9 |
| 0.89 | 71 |  | 0.26 | 2.3 | 0.23 | 2. |
| 1.27 | 75 |  | 0.73 | 6.5 | . 63 | 5.6 |
| 1.5 | 78 | 76 | 1.19 | 10.5 | 1.02 | 9.0 |
| 2.0 | 83 | 81 | 2.90 | 26 | 2.4 | 21 |
| 2.5 | 90 | 87 | 5.40 | 48 | 4.4 | 39 |
| 3.0 | 100 | 97 | 9.30 | 82 | 8.0 | 71 |
| 4.0 | 106 | 102 | 22.2 | 196 | 18.8 | 166 |
| 5.0 | 118 | 114 | 42.7 | 378 | 36.8 | 326 |
| 6.0 | 140 | 136 | 74.0 | 655 | 64 | 566 |
| 8.0 | 160 | 155 | 183.0 | 1,620 | 158 | 1,400 |
| 10.0 | 170 | 164 | 345.0 | 3,050 | 296 | 2,620 |
| 12.0 | 212 | 206 | 634.0 | 5,610 | 546 | 4,830 |
| 14.0 | 236 | 229 | 945.0 | 8,360 | 813 | 7,200 |
| 17.0 | 250 | 242 | 1,690 | 15,000 | 1,450 | 12,800 |
| 19.0 | 280 | 271 | 2,360 | 20,900 | 2,030 | 18,000 |
| 22.0 | 335 | 325 | 3,670 | 32,500 | 3,160 | 28,000 |
| 24.0 | 375 | 364 | 4,140 | 36,600 | 3,560 | 31,500 |
| 27.0 |  |  | 5,870 | 51,900 | 5,050 | 44,700 |
| 32.0 |  |  | 8,320 | 73,600 | 7,150 | 63,300 |
| 36.0 |  |  | 11,800 | 104,000 | 10,200 | 90,300 |


| Size | Part No. | $\square$ | $\begin{gathered} \text { lbs } \\ / 1000 \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| Short Series |  |  |  |
| 0.71 | 110230 | 100 | 0.26 |
| 0.89 | 115932 | 100 | 1.36 |
| 1.27 | 115965 | 100 | 2.27 |
| 1.5 | 125648 | 100 | 2.84 |
| 2.0 | 122263 | 100 | 4.99 |
| 2.5 | 122270 | 100 | 8.73 |
| 3.0 | 121093 | 100 | 13.18 |
| 4.0 | 119953 | 100 | 26.60 |
| 5.0 | 122245 | 100 | 44.24 |
| 6.0 | 121066 | 50 | 71.87 |
| 8.0 | 115557 | 50 | 133.36 |
| 10.0 | 120859 | 25 | 225.54 |
| 12.0 | 120860 | 25 | 354.71 |
| 14.0 | 111100 | 25 | 545.56 |
| 17.0 | 138487 | 10 | 941.60 |
| 19.0 | 111133 | 10 | 1349.77 |
| 22.0 | 402603 | 1 | 2026.20 |
| 24.0 | 402604 | 1 | 2706.00 |
| 27.0 | 402605 | 1 | 3843.40 |
| 32.0 | 402606 | 1 | 6813.40 |


| Size | Part No. | $\pi$ | $\begin{aligned} & \text { lbs } \\ & / 1000 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Long Series (ASME B18.3.2m) |  |  |  |
| 0.89 | C14663 | 100 | 0.95 |
| 1.5 | C04118 | 100 | 3.12 |
| 2.0 | C04119 | 100 | 5.94 |
| 2.5 | C04120 | 100 | 10.08 |
| 3.0 | C04122 | 100 | 16.04 |
| 4.0 | C04123 | 100 | 31.46 |
| 5.0 | C04127 | 100 | 54.52 |
| 6.0 | C04129 | 50 | 92.14 |
| 8.0 | C04130 | 50 | 255.64 |
| 10.0 | C04131 | 10 | 314.91 |
| 12.0 | C04132 | 10 | 556.23 |
| 14.0 | C04133 | 10 | 861.78 |
| 17.0 | C04134 | 1 | 1366.07 |
| 19.0 | C04135 | 1 | 1911.58 |

Note:
-The following Imperial are identical to Metric Sizes : 0.028 ins $=0.71 \mathrm{~mm}$,
$0.035 \mathrm{ins}=0.89 \mathrm{~mm}, 0.050 \mathrm{ins}=1.27 \mathrm{~mm}$. Please order by across flats dimensions and description.

- CAUTION: Unbrako advise that correct tools should be used for the application.
- Safety goggles should be worn for your security and protection.


## Metric Wrenches Application Chart

| Size <br> nom. | Socket Head <br> Cap screws | Low Head <br> Cap Screws | Flat Head <br> Socket screws | Button Head <br> screws | Socket Set <br> screws |
| ---: | :---: | :---: | :---: | :---: | :---: |
| 0.71 | - | - | - | - | M1.6 |
| 0.89 | - | - | - | - | M2 |
| 1.27 | - | - | - | - | M2.5 |
| 1.50 | M1.6/M2 | - | - | - | M3 |
| 2.00 | M2.5 | - | M3 | - | M4 |
| 2.50 | M3 | - | M4 | - | M5 |
| 3.00 | M4 | M4 | M5 | M6 | M6 |
| 4.00 | M5 | M5 | M6 | M8 | M8 |
| 5.00 | M6 | M6 | M8 | M10 | M10 |
| 6.00 | M8 | M8 | M10 | M12 | M12 |
| 8.00 | M10 | M10 | M12 | M16 | M16 |
| 10.00 | M12 | M12 | M16 | M20 | M20 |
| 12.00 | M14 | M16 | - | M24 | M24 |
| 14.00 | M16 | M20 | - | - | - |
| 17.00 | M20 | M24 | - | - | - |
| 19.00 | M24 | - | - | - | - |
| 22.00 | M30 | - | - | - | - |
| 27.00 | M36 | - | - | - | - |
| 32.00 | M42 | - | - | - | - |
| 36.00 | M48 | - | - | - | - |



Tough, ductile, for high torqueing; accurate fit in all types of socket screws; size marked for quick identity

Mechanical Properties
Material: ANSI B18.3, alloy steel Heat treat: Rc 47-57

Torsional Shear and Yield Strength

| size | Torsional shear <br> strength <br> inch-lbs. <br> nom. | Torsional <br> yield <br> inch-lbs. <br> min |
| ---: | ---: | ---: |
| .028 | 1.1 | 0.9 |
| .035 | 2.3 | 2.0 |
| .050 | 6.5 | 5.6 |
| $1 / 16$ | 12.2 | 10.5 |
| $5 / 64$ | 25.0 | 21.0 |
| $3 / 32$ | 43.0 | 35.0 |
| $7 / 64$ | 68.0 | 60.0 |
| $1 / 8$ | 98.0 | 85.0 |
| $9 / 64$ | 146.0 | 125.0 |
| $5 / 32$ | 195.0 | 165.0 |
| $3 / 16$ | 342.0 | 295.0 |
| $7 / 32$ | 535.0 | 460.0 |
| $1 / 4$ | 780.0 | 670.0 |
| $5 / 16$ | $1,600.0$ | $1,370.0$ |
| $3 / 8$ | $2,630.0$ | $2,260.0$ |
| $7 / 16$ | $4,500.0$ | $3,870.0$ |
| $1 / 2$ | $6,300.0$ | $5,420.0$ |
| $9 / 16$ | $8,900.0$ | $7,650.0$ |
| $5 / 8$ | $12,200.0$ | $10,500.0$ |
| $3 / 4$ | $19,500.0$ | $16,800.0$ |
| $7 / 8$ | $29,000.0$ | $24,900.0$ |
| 1 | $43,500.0$ | $37,400.0$ |
| $11 / 4$ | $71,900.0$ | $62,500.0$ |
| $11 / 2$ | $124,000.0$ | $108,000.0$ |
| $13 / 4$ | $198,000.0$ | $172,000.0$ |
| 2 | $276,000.0$ | $240,000.0$ |

## Marking




Product Dimensions

| size <br> nom. | Width <br> Across Flats W |  | Length of Short Arm B |  | C - Length of Long Arm |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | short series | long series |  | 6"long |
|  | max | min |  |  | max | min | max | min | max | min | arm |
| . 028 | . 0280 | . 0275 | . 312 | . 125 | 1.312 | 1.125 | 2.688 | 2.500 | - |
| . 035 | . 0350 | . 0345 | . 438 | . 250 | 1.312 | 1.125 | 2.766 | 2.578 | - |
| . 050 | . 0500 | . 0490 | . 625 | . 438 | 1.750 | 1.562 | 2.938 | 2.750 | - |
| 1/16 | . 0625 | . 0615 | . 656 | . 469 | 1.844 | 1.656 | 3.094 | 2.906 | - |
| 5/64 | . 0781 | . 0771 | . 703 | . 516 | 1.969 | 1.781 | 3.281 | 3.094 | 6.000 |
| 3/32 | . 0937 | . 0927 | . 750 | . 562 | 2.094 | 1.906 | 3.469 | 3.281 | 6.000 |
| 7/64 | . 1094 | . 1079 | . 797 | . 609 | 2.219 | 2.031 | 3.656 | 3.469 | 6.000 |
| 1/8 | . 1250 | . 1235 | . 844 | . 656 | 2.344 | 2.156 | 3.844 | 3.656 | 6.000 |
| 9/64 | . 1406 | . 1391 | . 891 | . 703 | 2.469 | 2.281 | 4.031 | 3.844 | 6.000 |
| 5/32 | . 1562 | . 1547 | . 938 | . 750 | 2.594 | 2.406 | 4.219 | 4.031 | 6.000 |
| 3/16 | . 1875 | . 1860 | 1.031 | . 844 | 2.844 | 2.656 | 4.594 | 4.406 | 6.000 |
| 7/32 | . 2187 | . 2172 | 1.125 | . 938 | 3.094 | 2.906 | 4.969 | 4.781 | 6.000 |
| 1/4 | . 2500 | . 2485 | 1.219 | 1.031 | 3.344 | 3.156 | 5.344 | 5.156 | 6.000 |
| 5/16 | . 3125 | . 3110 | 1.344 | 1.156 | 3.844 | 3.656 | 6.094 | 5.906 | 6.000 |
| 3/8 | . 3750 | . 3735 | 1.469 | 1.281 | 4.344 | 4.156 | 6.844 | 6.656 | 6.000 |
| 7/16 | . 4375 | . 4355 | 1.594 | 1.406 | 4.844 | 4.656 | 7.594 | 7.406 | - |
| 1/2 | . 5000 | . 4975 | 1.719 | 1.531 | 5.344 | 5.156 | 8.344 | 8.156 | - |
| 9/16 | . 5625 | . 5600 | 1.844 | 1.656 | 5.844 | 5.656 | 9.094 | 8.906 | - |
| 5/8 | . 6250 | . 6225 | 1.969 | 1.781 | 6.344 | 6.156 | 9.844 | 9.656 | - |
| 3/4 | . 7500 | . 7470 | 2.219 | 2.031 | 7.344 | 7.156 | 11.344 | 11.156 | - |
| 7/8 | . 8750 | . 8720 | 2.469 | 2.281 | 8.344 | 8.156 | 12.844 | 12.656 | - |
| 1 | 1.0000 | . 9970 | 2.719 | 2.531 | 9.344 | 9.156 | 14.344 | 14.156 | - |
| $11 / 4$ | 1.2500 | 1.2430 | 3.250 | 2.750 | 11.500 | 11.000 |  |  | - |
| $11 / 2$ | 1.5000 | 1.4930 | 3.750 | 3.250 | 13.500 | 13.000 |  |  | - |
| $13 / 4$ | 1.7500 | 1.7430 | 4.250 | 3.750 | 15.500 | 15.000 |  |  | - |
| 2 | 2.0000 | 1.9930 | 4.750 | 4.250 | 17.500 | 17.000 |  |  | - |


| Size | Part No． | 9 | $\begin{aligned} & \text { lbs } \\ & / 1000 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Short Series |  |  |  |
| 1／16 | 108468 | 100 | 3.32 |
| 5／64 | 110164 | 100 | 5.04 |
| 3／32 | 110180 | 100 | 7.77 |
| 7／64 | 110197 | 100 | 10.58 |
| 1／8 | 110213 | 100 | 13.99 |
| 9／64 | 115080 | 100 | 19.36 |
| 5／32 | 110246 | 100 | 24.22 |
| 3／16 | 115915 | 100 | 36.26 |
| 7／32 | 115948 | 50 | 53.46 |
| 1／4 | 115981 | 50 | 73.13 |
| 5／16 | 115997 | 50 | 126.21 |
| 3／8 | 116013 | 25 | 198.97 |
| 7／16 | 116029 | 25 | 294.25 |
| 1／2 | 116046 | 25 | 414.90 |
| 9／16 | 116063 | 25 | 563.86 |
| 5／8 | 116080 | 10 | 743.89 |
| 3／4 | 116096 | 10 | 1331.84 |
| 7／8 | 116112 | 5 | 2050.40 |
| 1 | 116128 | 5 | 2983.20 |

Size Part No． | lbs |
| :---: |
| $/ 1000$ |

Size Part No．$\quad$| lbs |
| :---: |
| $/ 1000$ |

| Long Series |  |  |  |
| ---: | ---: | ---: | ---: |
| $1 / 16$ | 108485 | 100 | 4.51 |
| $5 / 64$ | 117441 | 100 | 7.00 |
| $3 / 32$ | 117457 | 100 | 10.71 |
| $7 / 64$ | 117473 | 100 | 14.81 |
| $1 / 8$ | 114614 | 100 | 19.71 |
| $9 / 64$ | 113098 | 100 | 26.91 |
| $5 / 32$ | 114630 | 100 | 33.92 |
| $3 / 16$ | 114647 | 100 | 51.30 |
| $7 / 32$ | 114679 | 50 | 75.42 |
| $1 / 4$ | 114712 | 50 | 103.73 |
| $5 / 16$ | 114728 | 50 | 179.98 |
| $3 / 8$ | 114744 | 10 | 285.01 |
| $7 / 16$ | 114761 | 10 | 423.06 |
| $1 / 2$ | 114777 | 10 | 598.47 |
| $9 / 16$ | 114794 | 10 | 814.00 |
| $5 / 8$ | 107209 | 1 | 1078.48 |
| $3 / 4$ | 107225 | 1 | 1873.23 |
| $7 / 8$ | 107242 | 1 | 2895.20 |
| 1 | 107258 | 1 | 4219.60 |

## Inch Wrenches Application Chart

| size nom． | 1960 Series socket head cap screws | 1936 Series socket head cap screws | button head screws | flat head screws | shoulder screws | low heads and socket set screws | pressure＊ <br> plugs |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ． 028 | － | － | － | － | － | \＃0 | － |  |
| ． 035 | － | － | \＃0 | \＃0 | － | \＃1，\＃2 | － |  |
| ． 050 | \＃0 | － | \＃1，\＃2 | \＃1，\＃2 | － | \＃3，\＃4 | － |  |
| 1／16 | \＃1 | － | \＃3，\＃4 | \＃3，\＃4 | － | \＃5，\＃6 | － |  |
| 5／64 | \＃2，\＃3 | \＃4 | \＃5，\＃6 | \＃5，\＃6 | － | \＃8 | － |  |
| 3／32 | \＃4，\＃5 | \＃5，\＃6 | \＃8 | \＃8 | － | \＃10 | － |  |
| 7／64 | \＃6 |  | － | － | － | － | － |  |
| 1／8 | － | \＃8 | \＃10 | \＃10 | 1／4 | 1／4 | － |  |
| 9／64 | \＃8 |  | － | － | － | － | － |  |
| 5／32 | \＃10 | \＃10 | 1／4 | 1／4 | 5／16 | 5／16 | 1／16 |  |
| 3／16 | 1／4 | 1／4 | 5／16 | 5／16 | 3／8 | 3／8 | 1／8 |  |
| 7／32 | － | 5／16 | 3／8 | 3／8 | － | 7／16 | － |  |
| 1／4 | 5／16 |  | － | 7／16 | 1／2 | 1／2 | 1／4 |  |
| 5／16 | 3／8 | 3／8，7／16 | 1／2 | 1／2，9／16 | 5／8 | 5／8 | 3／8 |  |
| 3／8 | 7／16，1／2 | 1／2，5／16 | 5／8 | 5／8 | 3／4 | 3／4 | 1／2 |  |
| 7／16 | 9／16 |  | － | － | － | － | － |  |
| 1／2 | 5／8 | 5／8 | － | 3／4 | 7／8， 1 | 7／8 | － |  |
| 9／16 | － | 3／4，7／8 | － | 7／8 | － | 1，1／8 | 3／4 |  |
| 5／8 | 3／4 | 1 | － | 1 | $11 / 4$ | $11 / 4,13 / 8$ | 1 |  |
| 3／4 | 7／8，1 | － | － | － | － | $11 / 2$ | 1－1／4，1－1／2 |  |
| 7／8 | $11 / 8,11 / 4$ | － | － | － | $11 / 2$ | － | － |  |
| 1 | $13 / 8,1$ 1／2 | － | － | － | $13 / 4$ | － | 1／2， 2 |  |
| $11 / 4$ | $13 / 4$ | － | － | － | 2 | － | － |  |
| $11 / 2$ | 2 | － | － | － | － | － | － |  |
| $13 / 4$ | 2 1／4， 2 1／2 | － | － | － | － | － | － | ＊ $11 / 2$ levl seal has $3 / 4$＂socket |
| 2 | $23 / 4$ | － | － | － | － | － | － | $11 / 2$ dry seal has 1 ＂socket |

# Unorako 

THE WロRLD LEADER

## HIGH-PERFORMANCE STAINLESS STEEL FASTENERS

## Unbrako fasteners are now available in all grades of

Stainless Steel A2-70, A2-80, A4-70, A4-80, A4-90 and A4-100.

- Socket Head Cap Screws
- Socket Countersunk Head Screws
- Socket Button Head Screw's
- Hex Head Screms
- Hex Nuts
- Plain Masher
- Spring Washer
- Socket Set Screws
- Threaded Rod
- Specials



Corrosion
Resistance

Unbrako Stainless Steel Fasteners - available in SS304 \& SS316 - offer excellent corrosion resistance in a wide variety of environments.


Not attracted by a magnet. Maximum permeability is 1.2 . High valuable characteristic in electrical applications.


Retention of a high percentage of tensile strength and good creep resistance up to $800^{\circ} \mathrm{F}$ (without scaling or oxidation).


Useful in cryogenic application (like Liquid Nitrogen Gas(LNG) Processing), especially SS304, because it dose not become brittle as it is chilled.

## Unbrako <br> THE WロRLD LEADER

Durlok

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## Durlok Self-locking Anti-vibration Fasteners



Why do fasteners rotate loose under vibration?

The basic design \& function of a threaded fastener is to join multi--component assemblies so that the whole assembly performs as a single component.

In most cases, even in preloaded joints, the external forces create minimal relative displacements between the clamped parts, resulting in small sliding movements both in threads and under the head. Thus, the fastener becomes free of friction in a circumferential direction and the internal loosening or "off-torque" created by the preload on the threads will rotate the fastener loose.

In addition to self-loosening, fatigue failures can occur because the fastener will lose preload as soon as partial loosening takes place.

How does DURLOK ${ }^{\circledR}$ work?
Durlok ${ }^{\circledR}$ Free Spinning Self-locking fasteners come with all the benefits of serrated fasteners but with none of the disadvantages. Unlike serrated fasteners, with the unique Durlok ${ }^{\circledR}$ tooth formation, the locking is caused by the elastic spring back of the material at clamping load. A little wall of material builds up behind each tooth thereby blocking the bolt from turning.

Durlok ${ }^{\circledR}$ is designed with long, ramp shaped, radial teeth blended evenly into a smooth slightly conical outer bearing surface. It is this plain outer bearing ring that prevents excessive penetration into the bearing material, together with the long radial teeth which embed with only moderate edge pressure just sufficient to guarantee self-locking.

Durlok ${ }^{\circledR}$ Bolts of strength grade 12.9 are manufactured from alloy steel and are through hardened to give the same hardness from the tooth surface to the core. These are typically heavy duty bolts and can be used for all joints subjected to high loads.

## Advantages of DURLOK ${ }^{\circledR}$

Durlok ${ }^{\circledR}$ Bolts \& Nuts are suitable for multiple re-use because the serrations do not groove the clamped material and maintain locking ability.

The Durlok ${ }^{\circledR}$ fastener system is effective on a wide variety of engineering materials including steel both heat--treated and non heat-treated, cast irons including nodular types, non--ferrous metals and sheet materials.

The presence of oil or other lubricants, organic or inorganic coatings will not adversely affect the locking ability. In addition, the corrosion resistance of protected surfaces will generally be maintained because the smooth annular ring of Durlok ${ }^{\circledR}$ fastener shields the bearing area against liquid penetration.

Durlok ${ }^{\circledR}$ Fasteners can be used at elevated temperatures up to $300^{\circ} \mathrm{C}$.

## How can the self-locking ability be evaluated?

The most commonly used method for measuring locking ability has been by the indirect method of measuring \& comparing the tightening \& untightening torques. However, there is a growing realization that such a test in no way simulates the self-loosening mechanics of a fastener subjected to vibration. The only way this can be achieved is to apply a vibratory force to the bolted joint \& determine whether the fastener rotates loose. This has been attempted but without achieving any real measure of the self-locking ability of the fastener.

There are numerous possibilities of recording test data. However, the clearest presentation of self-locking ability is shown by recording loss of preload versus number of cycles.

A typical recording for both unlocked bolts \& bolts supposedly locked with spring washers shows that the initial bolt preload is completely lost after very few test cycles; conclusive evidence that the bolt has undergone total self-loosening.

These results clearly show that spring washers do not possess any genuine self-locking ability.

1. Hex Head Bolt M 10x30 DIN 933-8.8 unlocked.
2. Hex Head Bolt M 10x30 DIN 933-8.8 locked with spring washer according to DIN128B.
3. Hex Head Bolt M 10x30 DIN 933-8.8 locked with spring washer according to DIN 127A.

## Other advantages of DURLOK.

DURLOK bolts and nuts are suitable for re-use because the serrations cause relatively little damage to the clamped material. This means that the locking ability can be maintained as shown by the original vibration test recorded (see table 3)

This recording shows that the minimal loss of preload due to embedding even decreases due to cold-working of the surface of the clamped material during retightening of the fastener. The DURLOK fastener system is effective on a wide variety of engineering material including steel-both heat-treated \& non heat-treated, cast irons including nodular types, non-ferrous metals \& sheet materials.


Table 3
DURLOK bolts, however do not rotate loose when tested in the same way, even under the heaviest amplitudes. Even when only half of the recommended preload was used. Durlok bolts still did not loosen. This is illustrated by the figure:2, which is an original recording of a vibration test on M 10 DURLOK bolts. This shows that there is a mineral loss of preload even when the fastener is re-used.


THE WロRLD LEADER

## Durlok Self-locking Anti-vibration Fasteners

Will not loosen or unscrew even under the most severe transverse jarring and vibration.

Unique head design ensures absence of 'notch-effect' after assembly

Effectiveness at elevated temperatures upto $300^{\circ} \mathrm{C}$ is ensured.


Durlok ${ }^{\circledR}$ Washer
The DURLOK Advantage

Closely controlled manufacturing for extra safety and reliability.

During the 1960's, Dr. Junker while working in Unbrako's Koblenz facility in Germany completed his seminal work on the self-loosening behavior of bolted joints. This in turn led to the design of the original Durlok ${ }^{\circledR}$ anti-vibration nuts \& bolts. The Durlok 12.9 nuts \& bolts are designed for high-performance critical applications and do not require a washer. However, our industrial OEM customers requested a Durlok product in washer form for applications where it was deemed desirable to use a washer in the joint design. Thus we began researching and developed Unbrako's new Durlok locking wedge washer.


The Durlok ${ }^{\circledR}$ washer when used in combination with standard hex helps achieve self-locking properties. It is an anti-vibration solution that not only prevents bolted joint failure, but also enables the bolted joint to retain its pre-load, thus reducing maintenance requirements. The test regime highlighted this feature (fig 1).

Typical Applications for DURLOK ${ }^{\circledR}$ Fasteners

Automotive Engines
Power Unit Accessories
Transmission Units
Frames and Chassis Units
Bodywork
Vibratory Feeders
Shaking Chutes, Hoppers

Vibration Resistance Testing / Junker Test




Durlok free spinning self-locking bolts are designed with long, ramp shaped, radial teeth blended evenly into a smooth slightly conical outer surface. Reusable. Self-locking. Anti-vibration.

## Mechanical Properties

Property Class: 12.9
Material: Alloy Steel ISO 898-1
Hardness: 40-43HRc
Tensile Strength: $1220 \mathrm{~N} / \mathrm{mm}^{2} \mathrm{~min}$
Thread class: 6 g
Threads: ANSI B1.13M, ISO 261, ISO 262 (coarse series only)


Product Dimensions

|  | D | D1 | D2 | K | K1 | H | S | P | Length |
| ---: | :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Size | max | $\min$ |  | nom | min | min | $\max$ | $\max$ | ref |
| M5 | 12 | 11.0 | 5.5 | 4.5 | 1.0 | 2.09 | 8 | 3.65 | 50.0 |
| M6 | 14 | 11.8 | 6.6 | 5.2 | 1.1 | 2.69 | 10 | 4.35 | 50.0 |
| M8 | 18 | 15.2 | 9.0 | 7.2 | 1.3 | 4.21 | 13 | 5.90 | 60.0 |
| M10 | 21 | 17.2 | 11.0 | 9.0 | 1.6 | 5.47 | 15 | 7.50 | 60.0 |
| M12 | 25 | 20.6 | 14.0 | 11.0 | 1.9 | 6.71 | 17 | 9.10 | 80.0 |
| M14 | 28 | 22.8 | 16.0 | 12.5 | 2.2 | 7.65 | 19 | 10.65 | 80.0 |
| M16 | 32 | 25.5 | 18.0 | 16.0 | 3.8 | 9.27 | 22 | 12.55 | 100.0 |
| M20 | 39 | 31.2 | 22.0 | 18.0 | 3.1 | 11.86 | 27 | 15.70 | 100.0 |

Application Data

| Size | Stress <br> Area <br> mm2 | Proof Load | Load at yield (N) | load at min UTS <br> (N) | Induced preload <br> ( N ) | Tightening Torque Tmax (Nm) for $\mu$ head of |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | 0.125 | 0.16 | 0.2 |
| M5 | 14.2 | 13,750 | 15,600 | 17,300 | 11,300 | 10.8 | 12.4 | 14.2 |
| M6 | 20.1 | 19,500 | 22,100 | 24,500 | 15,950 | 18.2 | 21.0 | 24.0 |
| M8 | 36.6 | 35,500 | 40,300 | 44,600 | 29,300 | 44.0 | 50.0 | 58.0 |
| M10 | 58.0 | 56,300 | 63,800 | 70,800 | 46,600 | 84.0 | 96.0 | 109.0 |
| M12 | 84.3 | 81,800 | 92,700 | 102,800 | 68,000 | 148.0 | 169.0 | 194.0 |
| M14 | 115.0 | 111,500 | 126,500 | 140,000 | 93,000 | 233.0 | 266.0 | 304.0 |
| M16 | 157.0 | 152,000 | 172,500 | 191,500 | 129,000 | 362.0 | 413.0 | 472.0 |
| M20 | 245.0 | 238,000 | 270,000 | 299,000 | 201,000 | 695.0 | 797.0 | 913.0 |

## Note

*Fmax for $\mu$ thread $=0.125$

## Marking



Unoraco


Durlok nuts are designed with long, ramp shaped, radial teeth blended evenly into a smooth slightly conical outer surface. For use with Durlok Bolts. Self-locking. Anti-vibration. Reusable.

## Mechanical Properties

Material: Alloy Steel ISO 898-1
Hardness: 28-36HRc
Thread class: 6H
Head marking: U 12
Threads: ANSI B1.13M, ISO 261,
ISO 262 (coarse series only)
Property Class: 12

Marking


Product Dimensions

|  |  |  |  |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Size | max | D1 | D2 | S | H | K | K1 |
| M5 | 12 | 10.0 | 6.2 | 8 | 2.46 | 4.5 | 1.0 |
| M6 | 14 | 11.8 | 7.4 | 10 | 3.06 | 5.2 | 1.1 |
| M8 | 18 | 15.2 | 9.5 | 13 | 4.60 | 7.2 | 1.3 |
| M10 | 21 | 17.2 | 12.5 | 15 | 5.90 | 9.0 | 1.6 |
| M12 | 25 | 20.6 | 15.0 | 19 | 7.45 | 11.0 | 1.9 |
| M14 | 28 | 23.4 | 17.0 | 22 | 8.55 | 12.5 | 2.2 |
| M16 | 32 | 26.4 | 19.0 | 24 | 10.25 | 16.0 | 2.3 |
| M20 | 39 | 32.4 | 23.0 | 30 | 13.05 | 18.0 | 2.9 |

## Technical Data

The Durlok fastener system is effective on a wide variety of engineering materials including steel - both heat treated and non-heat treated, cast irons including nodular types, non ferrous metals and sheet materials.

The Presence of oil or other lubricants, organic or inorganic coatings should not adversely affect the locking ability. Durlok Fasteners can be used at elevated temperatures up to $300^{\circ} \mathrm{C}$.

The Induced assembly pre-load Fmax and the corresponding tightening torques, $T$ max are based on a $90 \%$ utilisation of the minimum yield strength by combined tension and torsional stresses. For cases where the yield strength must never be exceeded during tightening, the tightening torque must be reduced by a value equivalent to the scatter. Comprehensive investigation has shown that the scatter, due to variations in friction coefficient and torque scatter when tightening with torque wrench, must be accounted for by using a reduced torque $T$ which is $90 \%$ of the tabulated value T max, T = $0.9 \times$ Tmax Accordingly the induced pre-load Fmax will be reduced to the new pre-load $\mathrm{F}, \mathrm{Ff}=0.9 \times$ Fmax

It should be noted that pre-load and tightening torque are a function of the joint stiffness. The tabulated values are valid for
a joint stiffness which occurs under snug conditions with a clamping length of 2.5-4d. In addition, the values are based on an average friction co-efficent for the threads of $\mu=0.125$.

The value of the friction coefficient in the bearing area $\mu$ h, has a different value to that of the friction coefficient in the threads $\mu \mathrm{t}$, due to the serrations. As for all bolts the friction coefficient under the head is a function of the material, surface finish and lubrication condition of the contacting materials. To account for this the tightening torques are listed for various values of $\mu \mathrm{h}$.

For guidance the following chart is designed to indicate the appropriate value of friction coefficient to be applied for various engineering materials and finishes. The value of $\mu \mathrm{h}$ are based on the results of comprehensive tests:

| Coated Surface |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Bare Bolt Surface | Fine Turning <br> Grinding | Turning, Boring, <br> Milling | Rough Turning <br> Rough Milling |  |  |  |
| Steel Hardness <br> $250-350 ~ H V ~$ | 0.125 | 0.16 | 0.125 | 0.160 | 0.125 | 0.125 |
| Steel Hardness <br> $150-250 H V$ | 0.160 | 0.20 | 0.160 | 0.160 | 0.160 | 0.160 |
| Grey cast Iron <br> Nodular Cast Iron | 0.20 |  | 0.160 |  | 0.125 |  |


| Durlok ${ }^{\circledR}$ Bolts |  |  |  |
| :---: | :---: | :---: | :---: |
| Size | Part No. | 5 | $\begin{aligned} & \text { lbs } \\ & \text { /1000 } \end{aligned}$ |
| M6 (1) |  |  |  |
| M6x 12 | 190540 | 200 | 13.42 |
| 16 | 190560 | 200 | 14.94 |
| 20 | 190160 | 200 | 16.46 |
| 25 | 190170 | 200 | 18.35 |
| 30 | 190180 | 200 | 20.24 |
| M8 (1.25) |  |  |  |
| M8 $\times 12$ | 190570 | 200 | 28.49 |
| 16 | 190590 | 200 | 31.24 |
| 20 | 190210 | 200 | 33.99 |
| 25 | 190220 | 200 | 37.66 |
| 30 | 190230 | 200 | 40.88 |
| 35 | 190600 | 200 | 44.31 |
| 40 | 190240 | 200 | 47.76 |
| 45 | 408127 | 200 | 51.19 |
| 50 | 190610 | 100 | 54.63 |
| 60 | 407393 | 100 | 61.51 |


| Size | Part No. | lbs |  |
| ---: | ---: | ---: | ---: |
| M14 $\times 45$ | 190750 | 25 | 174.53 |
| 50 | 190760 | 25 | 185.33 |
| 60 | 190770 | 25 | 206.93 |
|  |  |  |  |
| M16 (2) |  |  |  |
| M16 x 30 | 190410 | 25 | 220.42 |
| 35 | 190420 | 25 | 234.92 |
| 40 | 190430 | 25 | 249.41 |
| 45 | 190820 | 25 | 263.91 |
| 50 | 190440 | 25 | 278.41 |
| 55 | 405105 | 25 | 292.91 |
| 60 | 190450 | 25 | 307.38 |
| 70 | 190460 | 25 | 336.38 |
| 80 | 190855 | 25 | 365.38 |
| 90 | 190860 | 25 | 392.48 |
| 100 | 190870 | 25 | 423.37 |


| M20 (2.5) |  |  |  |
| ---: | ---: | ---: | ---: |
| M20 x 40 | 190875 | 25 | 403.92 |
| 45 | 405793 | 25 | 426.92 |
| 50 | 182991 | 25 | 449.28 |
| 60 | 190885 | 25 | 494.65 |
| 70 | 190890 | 25 | 540.03 |
| 80 | 190900 | 25 | 585.40 |
| 90 | 190910 | 25 | 630.78 |
| 100 | 406937 | 25 | 676.15 |

Durlok ${ }^{\circledR}$ Nuts

| M12 (1.75) |  |  |  |
| ---: | ---: | ---: | ---: |
| M12 x 20 | 183640 | 100 | 86.06 |
| 25 | 190320 | 100 | 93.94 |
| 30 | 190330 | 100 | 101.84 |
| 35 | 190660 | 100 | 109.74 |
| 40 | 190340 | 50 | 117.63 |
| 45 | 190670 | 50 | 125.53 |
| 50 | 190350 | 50 | 133.43 |
| 55 | 190680 | 50 | 141.33 |
| 60 | 190360 | 50 | 149.23 |
| 70 | 190700 | 50 | 165.02 |
| 80 | 190710 | 50 | 180.80 |


| Size | Part No. | Ibs <br> $/ 1000$ |  |
| :--- | :--- | ---: | ---: | ---: |
| Nut |  |  |  |
| M6 (1) | 404916 | 200 | 5.50 |
| M8 (1.25) | 404917 | 200 | 13.86 |
| M10 (1.5) | 405202 | 200 | 23.59 |
| M12 (1.75) | 404918 | 100 | 39.60 |
| M14 (2) | 405240 | 50 | 69.52 |
| M16 (2) | 404915 | 50 | 88.00 |
| M20 (2.5) | 403618 | 50 | 166.96 |


| M14 (2) |  |  |  |
| ---: | :--- | :--- | :--- |
| M14 $\times 25$ | 190730 | 25 | 131.32 |
| 30 | 190370 | 25 | 142.12 |
| 35 | 190740 | 25 | 152.92 |
| 40 | 190380 | 25 | 163.72 |



Durlok washers are designed for use with standard hex bolts \& nuts. Self-locking. Anti-vibration.

## Mechanical Properties

Material: SAE 4130 or equivalent alloy. Through Hardened.
Plating: Zinc flake coating (Delta Protekt(R)) Heat treatment: 47-52 HRC

Product Dimensions

| Size | D |  | D2 |  | H |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | min. | max | min. | max | min. | max |
| 6 mm | 10.60 | 11.00 | 6.40 | 6.60 | 0.80 | 1.00 |
| 8 mm | 13.30 | 13.70 | 8.60 | 8.80 | 1.15 | 1.35 |
| 10 mm | 16.40 | 16.80 | 10.60 | 10.80 | 1.15 | 1.35 |
| 12 mm | 19.30 | 19.70 | 12.90 | 13.10 | 1.15 | 1.35 |
| 14 mm | 22.80 | 23.20 | 15.10 | 15.30 | 1.60 | 1.80 |
| 16 mm | 25.20 | 25.60 | 16.90 | 17.10 | 1.60 | 1.80 |
| 20 mm | 30.50 | 30.90 | 21.30 | 21.50 | 1.60 | 1.80 |
| 24 mm | 38.80 | 39.20 | 25.30 | 25.50 | 1.60 | 1.80 |

Product Range

| Size | Part No. | $8$ | $\begin{aligned} & \text { lbs } \\ & / 1000 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Zinc Flake Coated |  |  |  |
| M6 | 183794 | 200 | 0.91 |
| M8 | 183795 | 200 | 1.80 |
| M10 | 183796 | 200 | 2.73 |
| M12 | 183797 | 200 | 3.58 |
| M14 | 183798 | 100 | 5.88 |
| M16 | 183799 | 100 | 8.45 |
| M20 | 183801 | 100 | 11.50 |

## About Durlok Washers

Durlok ${ }^{\circledR}$ locking wedge washers when used with standard or high grade screws helps achieve self-locking properties. It utilizes tension instead of friction to secure bolted joints. Durlok washers come pre-assembled in pairs. They have wedge faces on the inside and radial teeth on the outside. They are designed such that the wedge angle is greater than the thread angle.

When the screw or the nut is tightened the radial teeth of Durlok washer locks itself onto the surface, allowing movement only across the wedge faces. During vibration, even a smallest turn of the screw causes an increase in pre-load force due to the wedge effect and the screw locks itself.

Thus the screw will not loosen or unscrew, even under severe jarring \& vibration. Durlok washers are re-usable with locking ability maintained.


Wedge Angle > Thread Angle



## Engineering Guide Technical Section



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## NOTE:

The technical discussions represent typical applications only. The use of the information is at the sole discretion of the reader. Because applications vary enormously, UNBRAKO does not warrant the scenarios described are appropriate for any specific application. The reader must consider all variables prior to using this information.

## INSTALLATION CONTROL

Several factors should be considered in designing a joint or selecting a fastener for a particular application.

## JOINT DESIGN AND FASTENER SELECTION. <br> Joint Length

The longer the joint length, the greater the total elongation will occur in the bolt to produce the desired clamp load or preload. In design, if the joint length is increased, the potential loss of preload is decreased.

## Joint Material

If the joint material is relatively stiff compared to the bolt material, it will compress less and therefore provide a less sensitive joint, less sensitive to loss of preload as a result of brinelling, relaxation and even loosening.

## Thread Stripping Strength

Considering the material in which the threads will be tapped or the nut used, there must be sufficient engagement length to carry the load. Ideally, the length of thread engagement should be sufficient to break the fastener in tension. When a nut is used, the wall thickness of the nut as well as its length must be considered.

An estimate, a calculation or joint evaluation will be required to determine the tension loads to which the bolt and joint will be exposed. The size bolt and the number necessary to carry the load expected, along with the safety factor, must also be selected.

The safety factor selected will have to take into consideration the consequence of failure as well as the additional holes and fasteners. Safety factors, therefore, have to be determined by the designer.

## SHEAR APPLICATIONS

Shear Strength of Material
Not all applications apply a tensile load to the fastener. In many cases, the load is perpendicular to the fastener in shear. Shear loading may be single, double or multiple loading.

There is a relationship between the tensile strength of a material and its shear strength. For alloy steel, the shear strength is $60 \%$ of its tensile strength. Corrosion resistant steels (e.g. 300-Series stainless steels) have a lower tensile/shear relationship and it is usually 50-55\%

## Single/Double Shear

Single shear strength is exactly one-half the double shear value. Shear strength listed in pounds per square inch (psi) is the shear load in pounds divided by the cross sectional area in square inches.


Double Shear


## OTHER DESIGN CONSIDERATIONS <br> Application Temperature

For elevated temperature, standard alloy steels are useful to about $550^{\circ} \mathrm{F}-600^{\circ} \mathrm{F}$. However, if plating is used, the maximum temperature may be less (eg. cadmium should not be used over $450^{\circ} \mathrm{F}$.

Austenitic stainless steels ( 300 Series) may be useful to $800^{\circ} \mathrm{F}$. They can maintain strength above $800^{\circ} \mathrm{F}$ but will begin to oxidize on the surface.

## Corrosion Environment

A plating may be selected for mild atmospheres or salts. If plating is unsatisfactory, a corrosion resistant fastener may be specified. The proper selection will be based upon the severity of the corrosive environment.

## FATIGUE STRENGTH

## S/N Curve

Most comparative fatigue testing and specification fatigue test requirements are plotted on an S/N curve. In this curve, the test stress is shown on the ordinate (y-axis) and the number of cycles is shown on the abscissa ( $x$-axis) in a logarithmic scale. On this type curve, the high load to low load ratio must be shown. This is usually $R=.1$, which means the low load in all tests will be $10 \%$ of the high load.


## Effect of Preload

Increasing the R to $.2, .3$ or higher will change the curve shape. At some point in this curve, the number of cycles will reach 10 million cycles. This is considered the
endurance limit or the stress at which infinite life might be expected.

## Modified Goodman/ Haigh Soderberg Curve

The $\mathrm{S} / \mathrm{N}$ curve and the information it supplies will not provide the information needed to determine how an individual fastener will perform in an actual application. In application, the preload should be higher than any of the preloads on the $\mathrm{S} / \mathrm{N}$ curve.

Therefore, for application information, the modified Goodman Diagram and/or the Haigh Soderberg Curve are more useful. These curves will show what fatigue performance can be expected when the parts are properly preloaded.


METHODS OF PRELOADING
Elongation
The modulus for steel of 30,000,000 (thirty million) psi means that a fastener will elongate $.001 \mathrm{in} / \mathrm{in}$ of length for every 30,000 psi in applied stress. Therefore, if $90,000 \mathrm{psi}$ is the desired preload, the bolt must be stretched .003 inches for every inch of length in the joint.

This method of preloading is very accurate but it requires that the ends of the bolts be properly prepared and also that all measurements be very carefully made. In addition, direct measurements are only possible where both ends of the fastener are available for measurement after installation. Other methods of measuring lengths changes are ultrasonic, strain gages and turn of the nut.

## Torque

By far, the most popular method of preloading is by torque. Fastener manufacturers usually have recommended seating torques for each size and material fastener. The only requirement is the proper size torque wrench, a conscientious operator and the proper torque requirement.

Strain
Since stress/strain is a constant relationship for any given material, we can use that relationship just as the elongation change measurements were used previously.

Now, however, the strain can be detected from strain gages applied directly to the outside surface of the bolt or by having a hole drilled in the center of the bolt \& the strain gage installed internally. The output from these gages need instrumentation to convert the gage electrical measurement method. It is, however, an expensive method and not always practical.

Turn of the Nut
The nut turn method also utilizes change in bolt length. In theory, one bolt revolution ( $360^{\circ}$ rotation) should increase the bolt length by the thread pitch. There are at least two variables, however, which influence this relationship. First, until a snug joint is obtained, no bolt elongation can be measured. The snugging produces a large variation in preload. Second, joint compression is also taking place so the relative stiff nesses of the joint and bolt influences the load obtained.

## VARIABLES IN TORQUE <br> Coefficient of Friction

Since the torque applied to a fastener must overcome all friction before any loading takes place, the amount of friction present is important.

In a standard unlubricated assembly, the friction to be overcome is the head bearing area and the thread-tothread friction. Approximately $50 \%$ of the torque applied will be used to overcome this head-bearing friction and approximately $35 \%$ to overcome the thread friction. So $85 \%$ of the torque is overcoming friction and only $15 \%$ is available to produce bolt load.

If these interfaces are lubricated (cadmium plate, molybdenum disulfide, anti-seize compounds, etc.), the friction is reduced and thus greater preload is produced with the same torque.

The change in the coefficient of friction for different conditions can have a very significant effect on the slope of the torque tension curve. If this is not taken into consideration, the proper torque specified for a plain unlubricated bolt may be sufficient to yield or break a lubricated fastener.

## Thread Pitch

The thread pitch must be considered when a given stress is to be applied, since the cross-sectional area used for stress calculations is the thread tensile stress area and is different for coarse and fine threads. The torque recommendations, therefore, are slightly higher for fine threads than for coarse threads to achieve the same stress.

Differences between coarse and fine threads. Coarse Threads are...

- more readily available in industrial fasteners.
- easier to assemble because of larger helix angle.
- require fewer turns and reduce cross threading.
- higher thread stripping strength per given length.
- less critical of tap drill size.
- not as easily damaged in handling

Their disadvantages are...

- lower tensile strength.
- reduced vibrational resistance.
- coarse adjustment.

Fine Threads provide...

- higher tensile strength.
- greater vibrational resistance.
- finer adjustment.

Their disadvantages are...

- easier cross threaded.
- threads damaged more easily by handling.
- tap drill size slightly more critical.
- slightly lower thread stripping strength.


## Other Design Guidelines

In addition to the joint design factors discussed, the following considerations are important to the proper use of high-strength fasteners.

- Adequate thread engagement should be guaranteed by use of the proper mating nut height for the system. Minimum length of engagement recommended in a tapped hole depends on the strength of the material, but in all cases should be adequate to prevent stripping.
- Specify nut of proper strength level. The bolt and nut should be selected as a system.
- Specify compatible mating female threads. 2B tapped holes or 3B nuts are possibilities.
- Corrosion, in general, is a problem of the joint, and not just of the bolt alone. This can be a matter of galvanic action between dissimilar metals. Corrosion of the fastener material surrounding the bolt head or nut can be critical with high-strength bolting. Care must be exercised in the compatibility of joint materials and/or coatings to protect dissimilar metals.


## PROCESSING CONTROL

The quality of the raw material and the processing control will largely affect the mechanical properties of the finished parts.

## MATERIAL SELECTION

The selection of the type of material will depend on its end use. However, the control of the analysis and quality is a critical factor in fastener performance. The material must yield reliable parts with few hidden defects such as cracks, seams, decarburization and internal flaws.

## FABRICATION METHOD

Head
There are two general methods of making bolt heads, forging and machining. The economy and grain flow resulting from forging make it the preferred method.

The temperature of forging can vary from room temperature to $2000^{\circ} \mathrm{F}$. By far, the greatest number of parts are cold upset on forging machines known as headers or bolt makers. For materials that do not have enough formability for cold forging, hot forging is used. Hot forging is also used for bolts too large for cold upsetting due to machine capacity. The largest cold forging machines can make bolts up to 1-1/2 inch diameter. For
large quantities of bolts, hot forging is more expensive then cold forging.

Some materials, such as stainless steel, are warm forged at temperatures up to $1000^{\circ} \mathrm{F}$. The heating results in two benefits, lower forging pressures due to lower yield strength and reduced work hardening rates.

Machining is the oldest method and is used for very large diameters or small production runs.

The disadvantage is that machining cuts the metal grain flow, thus creating planes of weakness at the critical head-to-shank fillet area. This can reduce tension fatigue performance by providing fracture planes.

## Fillets

The head-to-shank transition (fillet) represents a sizable change in cross section at a critical area of bolt performance. It is important that this notch effect be minimized. A generous radius in the fillet reduces the notch effect. However, a compromise is necessary because too large a radius will reduce load-bearing area under the head.

Composite radii such as elliptical fillets, maximize curvature on the shank side of the fillet and minimize it on the head side to reduce loss of bearing area on the load-bearing surface.

Critical Fastener Features
Head-Shank-Fillet: This area on the bolt must not be restricted or bound by the joint hole. A sufficient chamfer or radius on the edge of the hole will prevent interference that could seriously reduce fatigue life. Also, if the bolt should seat on an unchamfered edge, there might be serious loss of preload if the edge breaks under load.

## Threads

Threads can be produced by grinding, cutting or rolling. In a rolled thread, the material is caused to flow into the thread die contour, which is ground into the surface during the manufacture of the die. Machines with two or three circular dies or two flat dies are most common.

Thread cutting requires the least tooling costs and is by far the most popular for producing internal threads. It is the most practical method for producing thin wall parts and the only technique available for producing large diameter parts (over 3 inches in diameter).

Thread grinding yields high dimensional precision and affords good control of form and finish. It is the only practical method for producing thread plug gages.

Both machining and grinding have the disadvantage of cutting material fibers at the most critical point of performance.

The shape or contour of the thread has a great effect on the resulting fatigue life. The thread root should be large and well rounded without sharp corners or stress risers. Threads with larger roots should always be used for harder materials.

In addition to the benefits of grain flow and controlled shape in thread rolling, added fatigue life can result when the rolling is performed after heat treatment.

This is the accepted practice for high fatigue performance bolts such as those used in aircraft and space applications.


## EVALUATING PERFORMANCE

Mechanical Testing
In the fastener industy, a system of tests and examinations has evolved which yields reliable parts with proven performance.

Some tests are conducted on the raw material; some on the finished product.

There always seems to be some confusion regarding mechanical versus metallurgical properties. Mechanical properties are those associated with elastic or inelastic reaction when force is applied, or that involve the relationship between stress and strain. Tensile testing stresses the fastener in the axial direction. The force at which the fastener breaks is called the breaking load or ultimate tensile strength. Load is designated in pounds, stress in pounds per square inch and strain in inches per inch.

When a smooth tensile specimen is tested, the chart obtained is called a Stress-Strain Curve. From this curve, we can obtain other useful data such as yield strength. The method of determining yield is known as the offset method and consists of drawing a straight line parallel to the stress strain curve but offset from the zero point by a specified amount. This value is usually $0.2 \%$ on the strain ordinate. The yield point is the intersection of the stressstrain curve and the straight line. This method is not applicable to fasteners because of the variables introduced by their geometry.

When a fastener tensile test is plotted, a load/ elongation curve can be obtained. From this curve, a yield determination known as Johnson's 2/3 approximate method for determination of yield strength is used to establish fastener yield, which will be acceptable for design purposes. It is not recommended for quality control or specification requirements.

Torque-tension testing is conducted to correlate the required torque necessary to induce a given load in a mechanically fastened joint. It can be performed by hand or machine. The load may be measured by a tensile machine, a load cell, a hydraulic tensile indicator or by a strain gage.

Fatigue tests on threaded fasteners are usually alternating tension-tension loading. Most testing is done at more severe strain than its designed service load but usually below the material yield strength.

Shear testing, as previously mentioned, consists of loading a fastener perpendicular to its axis. All shear testing should be accomplished on the un-threaded portion of the fastener.

Checking hardness of parts is an indirect method for testing tensile strength. Over the years, a correlation of tensile strength to hardness has been obtained for most materials. See page 136 for more detailed information. Since hardness is a relatively easy and inexpensive test, it makes a good inspection check. In hardness checking, it is very important that the specimen be properly prepared and the proper test applied.

Stress durability is used to test parts which have been subjected to any processing which may have an embrittling effect. It requires loading the parts to a value higher than the expected service load and maintaining that load for a specified time after which the load is removed and the fastener examined for the presence of cracks.

Impact testing has been useful in determining the ductile brittle transformation point for many materials. However, because the impact loading direction is transverse to a fastener's normal longitude loading, its usefulness for fastener testing is minimal. It has been shown that many fastener tension impact strengths do not follow the same pattern or relationship of Charpy or Izod impact strength.

## Metallurgical Testing

Metallurgical testing includes chemical composition, micro structure, grain size, carburization and decarburization, and heat treat response.

The chemical composition is established when the material is melted. Nothing subsequent to that process will influence the basic composition.

The microstructure and grain size can be influenced by heat treatment. Carburization is the addition of carbon to the surface which increases hardness. It can occur if heat treat furnace atmospheres are not adequately controlled. Decarburization is the loss of carbon from the surface, making it softer. Partial decarburization is preferable to carburization, and most industrial standards allow it within limits.

In summary, in order to prevent service failures, many things must be considered:

## The Application Requirements

Strength Needed - Safety Factors

- Tension/Shear/Fatigue
- Temperature
- Corrosion
- Proper Preload

The Fastener Requirements

- Material
- Fabrication Controls
- Performance Evaluations


## AN EXPLANATION OF JOINT DIAGRAMS

When bolted joints are subjected to external tensile loads, what forces and elastic deformation really exist? The majority of engineers in both the fastener manufacturing and user industries still are uncertain. Several papers, articles, and books, reflecting various stages of research into the problem have been published and the volume of this material is one reason for confusion. The purpose of this article is to clarify the various explanations that have been offered and to state the fundamental concepts which apply to forces and elastic deformations in concentrically loaded joints. The article concludes with general design formulae that take into account variations in tightening, preload loss during service, and the relation between preloads, external loads and bolt loads.

## The Joint Diagram

Forces less than proof load cause elastic strains. Conversely, changes in elastic strains produce force variations. For bolted joints this concept is usually demonstrated by joint diagrams.

The most important deformations within a joint are elastic bolt elongation and elastic joint compression in the axial direction. If the bolted joint in Fig. 1 is subjected to the preload $F_{i}$ the bolt elongates as shown by the line $O B$ in Fig. 2A and the joint compresses as shown by the line OJ. These two lines, representing the spring characteristics of the bolt and joint, are combined into one diagram in Fig. 2B to show total elastic deformation.

If a concentric external load $F_{e}$ is applied under the bolt head and nut in Fig. 1, the bolt elongates an additional amount while the compressed joint members partially relax. These changes in deformation with external loading are the key to the interaction of forces in bolted joints.

In Fig. 3A the external load $F_{e}$ is added to the joint diagram Fe is located on the diagram by applying the upper end to an extension of $O B$ and moving it in until the lower end contacts OJ. Since the total amount of elastic deformation (bolt plus joint) remains constant for a given preload, the external load changes the total bolt elongation to $\Delta I_{\mathrm{B}}+\lambda$ and the total joint compression to $\Delta J_{J}-\lambda$.

In Fig. 3B the external load $F_{e}$ is divided into an additional bolt load $F_{e B}$ and the joint load $F_{e J}$, which unloads the compressed joint members. The maximum bolt load is the sum of the load preload and the additional bolt load:
$F_{B \text { max }}=F_{i}+F_{e B}$
If the external load Fe is an alternating load, $\mathrm{F}_{\mathrm{eB}}$ is that part of $F_{e}$ working as an alternating bolt load, as shown in Fig. 3B. This joint diagram also illustrates that the joint absorbs more of the external load than the bolt subjected to an alternating external load.

The importance of adequate preload is shown in Fig. 3C. Comparing Fig. 3B and Fig. 3C, it can be seen that $F_{e B}$ will remain relatively small as long as the preload $F_{i}$ is greater than $F_{\text {eJ. }}$ Fig. 3C represents a joint with insufficient preload. Under this condition, the amount of external load that the joint can absorb is limited, and the excess load
must then be applied to the bolt. If the external load is alternating, the increased stress levels on the bolt producea greatly shortened fatigue life.

When seating requires a certain minimum force or when transverse loads are to be transformed by friction, the minimum clamping load $F_{J \text { min }}$ is important.


H


Fig. 2 Joint diagram is obtained by combining load vs. deformation diagrams of bolt and joints.


## Spring Constants

To construct a joint diagram, it is necessary to determine the spring rates of both bolt and joint. In general, spring rate is defined as:
$K=\frac{F}{\Delta l}$
From Hook's law:
$\Delta I=\frac{\mathrm{IF}}{\mathrm{EA}}$
Therefore:
$K=\frac{E A}{I}$
To calculate the spring rate of bolts with different cross sections, the reciprocal spring rates, or compliances, of each section are added:

$$
\frac{1}{\mathrm{~K}_{\mathrm{B}}}=\frac{1}{\mathrm{~K}_{1}}+\frac{1}{\mathrm{~K}_{2}}+\cdots+\frac{1}{\mathrm{~K}_{\mathrm{n}}}
$$

Thus, for the bolt shown in Fig. 4:

$$
\frac{1}{\mathrm{~K}_{\mathrm{B}}}=\frac{1}{\mathrm{E}}\left(\frac{0.4 \mathrm{~d}}{\mathrm{~A}_{1}}+\frac{I_{1}}{\mathrm{~A}_{1}}+\frac{I_{2}}{\mathrm{~A}_{2}}+\frac{I_{3}}{\mathrm{~A}_{\mathrm{m}}}+\frac{0.4 \mathrm{~d}}{\mathrm{~A}_{\mathrm{m}}}\right)
$$

where
$\mathrm{d}=$ the minor thread diameter and
$A_{m}=$ the area of the minor thread diameter
This formula considers the elastic deformation of the head and the engaged thread with a length of 0.4 d each.
Calculation of the spring rate of the compressed joint members is more difficult because it is not always obvious which parts of the joint are deformed and which are not. In general, the spring rate of a clamped part is:
$K_{J}=\frac{E A_{S}}{I_{J}}$
where $A_{s}$ is the area of a substitute cylinder to be determined.


Fig. 4 Analysis of bolt lengths contributing to the bolt spring rate.

When the outside diameter of the joint is smaller than or equal to the bolt head diameter, i.e.,as in a thin bushing, the normal cross sectioned area is computed:
$A_{s}=\frac{\pi}{4}\left(D_{c}{ }^{2}-D_{h}{ }^{2}\right)$
where
$D_{c}=O D$ of cylinder or bushing and
$D_{h}=$ hole diameter
When the outside diameter of the joint is larger than head or washer diameter Dн, the stress distribution is in the shape of a barrel, Fig 5 . A series of investigations proved that the areas of the following substitute cylinders are close approximations for calculating the spring contents of concentrically loaded joints.

When the joint diameter $D_{J}$ is greater than $D_{H}$ but less than $3 \mathrm{D}_{\mathrm{H}}$;


Fig. 5 Lines of equal axial stresses in a bolted joint obtained by the axisymmetric finite element method are shown for a 9/16-18 bolt preloaded to 100 KSI . Positive numbers are tensile stresses in KSI; negative numbers are compressive stresses in KSI.

$$
\begin{aligned}
A_{s}= & \frac{\pi}{4}\left(D_{H}{ }^{2}-D_{h}{ }^{2}\right) \\
& +\frac{\pi}{8}\left(\frac{D_{J}}{D H}-1\right)\left(\frac{D_{H} I_{J}}{5}+\frac{I_{J}{ }^{2}}{100}\right)
\end{aligned}
$$

When the joint diameter $D_{J}$ is equal to or greater than $3 D_{H}$ :
$A_{s}=\frac{\pi}{4}\left[\left(D_{H}+0.1 / I_{J}\right)^{2}-D_{h}{ }^{2}\right]$
These formulate have been verified in laboratories by finite element method and by experiments.

Fig. 6 shows joint diagrams for springy bolt and stiff joint and for a stiff bolt and springy joint. These diagrams demonstrate the desirability of designing with springy bolt and a stiff joint to obtain a low additional bolt load $F_{e B}$ and thus a low alternating stress.

## The Force Ratio

Due to the geometry of the joint diagram, Fig. 7,
$F_{e B}=\frac{K_{e} K_{B}}{K_{B}+K_{J}}$
Defining $\Phi=\frac{K_{B}}{K_{B}+K_{J}}$
$\mathrm{F}_{\mathrm{eB}}=\mathrm{F}_{\mathrm{e}} \Phi$ and
$\Phi$, called the Force Ratio, $=\frac{F_{e B}}{F_{e}}$
For complete derivation of $\Phi$ see Fig. 7 .
To assure adequate fatigue strength of the selected fastener the fatigue stress amplitude of the bolt resulting from an external load $F_{e}$ is computed as follows:
$\sigma_{B}= \pm \frac{F_{e B} / 2}{A_{m}}$ or
$\sigma_{\mathrm{B}}= \pm \frac{\Phi \mathrm{F}_{\mathrm{e}}}{2 \mathrm{~A}_{\mathrm{m}}}$

## Effect of Loading Planes

The joint diagram in Fig 3, 6 and 7 is applicable only when the external load $\mathrm{F}_{\mathrm{e}}$ is applied at the same loading planes as the preloaded $F_{i}$, under the bolt head and the nut. However, this is a rare case, because the external load usually affects the joint somewhere between the center of the joint and the head and the nut.

When a preloaded joint is subjected to an external load $F_{e}$ at loading planes 2 and 3 in Fig. 8, $F_{e}$ relieves the compression load of the joint parts between planes 2 and 3. The remainder of the system, the bolt and the joint parts between planes 1-2 and 3-4, feel additional load due to $\mathrm{F}_{\mathrm{e}}$ applied planes 2 and 3 , the joint material between planes 2 and 3 is the clamped part and all other joint members, fastener and remaining joint material, are clamping parts. Because of the location of the loading planes, the joint diagram changes from black line to the blue line. Consequently, both the additional bolt load $F_{B \text { max }}$ decrease significantly when the loading planes of $F_{e}$ shift from under the bolt head and nut toward the joint center.

Determination of the length of the clamped parts is, however, not that simple. First, it is assumed that the external load is applied at a plane perpendicular to the bolt axis. Second, the distance of the loading planes from each other has to be estimated. This distance may be expressed as the ratio of the length of clamped parts to the total joint length. Fig. 9 shows the effect of two different loading planes on the bolt load, both joints having the same preload $F_{i}$ and the same external load $F_{\mathrm{e}}$. The lengths of the clamped parts are estimated to be $0.75 / \mathrm{J}$ for joint A , and $0.25 / \mathrm{J}$ for joint B .

In general, the external bolt load is somewhere between $F_{e B}=1 \Phi F_{e}$ for loading planes under head and nut and $\mathrm{F}_{\mathrm{eB}}=0 Ф \mathrm{~F}_{\mathrm{e}}=0$ when loading planes are in the joint center, as shown in Fig. 10. To consider the loading planes in calculation, the formula:


Fig. 6 Joint diagram of a springy bolt in a stiff joint (A), is compared to a diagram of a stiff bolt in a springy joint (B). Preload $F_{i}$ and external load $F_{e}$ are the same but diagrams show that alternating bolt stresses are significantly lower with a spring bolt in a stiff joint.


Fig. 7 Analysis of external load $\mathrm{F}_{\mathrm{e}}$ and derivation of Force Ratio $\Phi$.
$\tan \alpha=\frac{F_{i}}{\Delta l_{B}}=K_{B}$ and $\tan \beta=\frac{F i}{\Delta l_{J}}=K_{J}$
$\lambda=\frac{\mathrm{F}_{\text {eB }}}{\tan \alpha}=\frac{\mathrm{Fe}_{\text {e }}}{\tan \beta}=\frac{\mathrm{FeB}}{\mathrm{K}_{\mathrm{B}}}=\frac{\mathrm{F}_{\text {e }}}{\mathrm{K}_{\mathrm{J}}}$ or
$F_{e J}=\lambda \tan \beta$ and $F_{e B}=\lambda \tan \alpha$
Since $\mathrm{Fe}_{\mathrm{e}}=\mathrm{FeB}_{\mathrm{e}}+\mathrm{FeJ}_{\mathrm{e}}$
$\mathrm{Fe}_{\mathrm{e}}=\mathrm{FeB}_{\mathrm{e}}+\lambda \tan \beta$
Substituting $\frac{\mathrm{F}_{\mathrm{e}} \mathrm{B}}{\tan \alpha}$ for $\lambda$ produces:

$$
\mathrm{F}_{\mathrm{e}}=\mathrm{F}_{\mathrm{eB}}+\frac{\mathrm{F}_{\mathrm{eB}} \tan \beta}{\tan \alpha}
$$

Multiplying both sides by $\tan \alpha$ :
$F_{\mathrm{e}} \tan \alpha=\mathrm{FeB}_{\mathrm{e}}(\tan \alpha+\tan \beta)$ and
$\mathrm{FeB}_{\mathrm{e}}=\frac{\mathrm{F}_{\mathrm{e}} \tan \alpha}{\tan \alpha \tan \beta}$
Substituting $K_{B}$ for $\tan \alpha$ and $K_{J}$ for $\tan \beta$
$F_{e B}=F_{e} \frac{F_{B}}{K_{B}+K_{B}}$
Defining $\Phi=\frac{K_{B}}{K_{B}+K_{J}}$
$\mathrm{F}_{\mathrm{eB}}=\Phi \mathrm{F}_{\mathrm{e}}$
$\Phi=\frac{F_{e B}}{F_{e}} \quad \begin{aligned} & \text { and it becomes obvious why } \Phi \\ & \text { is called force ratio. }\end{aligned}$


Fig. 8 Joint diagram shows effect of loading planes of $F_{e}$ on bolt loads $\mathrm{F}_{\mathrm{e}}$ and $\mathrm{F}_{\mathrm{B} \text { max }}$. Black diagram shows $\mathrm{F}_{\mathrm{eB}}$ and $F_{B \max }$ resulting from $F_{e}$ applied in planes 1 and 4. Orange diagram shows reduced bolt loads when Fe is applied in planes 2 and 3.


Fig. 9 When external load is applied relatively near bolt head, joint diagram shows resulting alternating stress $\alpha_{B}$ (A). When same value external load is applied relatively near joint center, lower alternating stress results (B).


Fig. 10 Force diagrams show the effect of the loading planes of the external load on the bolt load.


Fig. 11 Modified joint diagram shows nonlinear compression of joint at low preloads.
$\mathrm{F}_{\mathrm{eB}}=\Phi \mathrm{F}_{\mathrm{e}}$ must be modified to:
$\mathrm{F}_{\mathrm{eB}}=\mathrm{n} \Phi \mathrm{F}_{\mathrm{e}}$
where $n$ equals the ratio of the length of the clamped parts due to $F_{e}$ to the joint length $/ \mathrm{j}$. The value of $n$ can range from 1, when Fe is applied under the head and nut, to O , when $\mathrm{F}_{\mathrm{e}}$ is applies at the joint center. Consequently the stress amplitude:
$\sigma_{B}= \pm \frac{\Phi F_{e}}{2 A_{m}} \quad$ becomes
$\sigma_{B}= \pm \frac{n \Phi F_{e}}{2 A_{m}}$

## General Design Formulae

Hitherto, construction of the joint diagram has assumed linear resilience of both bolt and joint members. However, recent investigations have shown that this assumption is not quite true for compressed parts.

Taking these investigations into account, the joint diagram is modified to Fig. 11. The lower portion of the joint spring rate is nonlinear, and the length of the linear portion depends on the preload level $F_{i}$. The higher $F_{i}$ the longer the linear portion. By choosing a sufficiently high minimum load, $\mathrm{F}_{\text {min }}>2 \mathrm{~F}_{\mathrm{e}}$, the non-linear range of the joint spring rate is avoided and a linear relationship between $F_{e B}$ and $F_{e}$ is maintained.

Also from Fig. 11 this formula is derived:
$F_{i \text { min }}=F_{J \text { min }}+(1-\Phi) F_{e}+\Delta F_{i}$
where $\Delta F_{i}$ is the amount of preload loss to be expected. For a properly designed joint, a preload loss $\Delta F_{i}=-(0.005$ to 0.10$) F_{i}$ should be expected.

The fluctuation in bolt load that results from tightening is expressed by the ratio:
$\mathrm{a}=\frac{\mathrm{F}_{\mathrm{i} \text { max }}}{\mathrm{F}_{\mathrm{i} \text { min }}}$
where a varies between 1.25 and 3.0 depending on the tightening method.

Considering a the general design formulae are:
$F_{\text {inom }}=F_{J \text { min }}=(1-\Phi) F_{e}$
$F_{i \text { max }}=a\left[F_{j \text { min }}+(1-\Phi) F_{e}+\Delta F_{i}\right]$
$F_{B \text { max }}=a\left[F_{j \text { min }}+(1-\Phi) F_{e}+\Delta F_{i}\right]+\Phi F_{e}$

## Conclusion

The three requirements of concentrically loaded joints that must be met for an integral bolted joint are:

1. The maximum bolt load FB max must be less than the bolt yield strength.
2. If the external load is alternating, the alternating stress must be less than the bolt endurance limit to avoid fatigue failures.
3. The joint will not lose any preload due to permanent set or vibration greater than the value assumed for $\Delta \mathrm{Fi}_{\mathrm{i}}$.

## SYMBOLS

| A | Area (in. ${ }^{2}$ ) |
| :---: | :---: |
| $A_{m}$ | Area of minor thread diameter (in. ${ }^{2}$ ) |
| As | Area of substitute cyliner (in. ${ }^{2}$ ) |
| Ax | Area of bolt part $1_{\mathrm{x}}\left(\mathrm{in} .^{2}\right)$ |
| d | Diameter of minor thread (in.) |
| D | Outside diameter of bushing (cylinder) (in.) |
| Dн | Diameter of Bolt head (in.) |
| Dh | Diameter of hole (in.) |
| DJ | Diameter of Joint |
| E | Modulus of Elasticity (psi) |
| F | Load (lb) |
| $\mathrm{F}_{\mathrm{e}}$ | External load (lb.) |
| $\mathrm{F}_{\text {eb }}$ | Additinal Bolt Load due to external load (lb) |
| $\mathrm{FeJ}_{\text {J }}$ | Reduced Joint load due to external load (lb) |
| $\mathrm{F}_{\mathrm{i}}$ | Preload on Bolt and Joint (lb) |
| $\Delta \mathrm{F}_{\mathrm{i}}$ | Preload loss (-lb) |
| $\mathrm{Fimin}^{\text {m }}$ | Minimum preload (lb) |
| $\mathrm{Fimax}_{\text {max }}$ | Maximum preload (lb) |
| $\mathrm{F}_{\mathrm{j} \text { nom }}$ | Nominal preload (lb) |


| $\mathrm{F}_{\text {B max }}$ | Maximum Bolt load (lb) |
| :---: | :---: |
| FJ ${ }_{\text {min }}$ | Minimum Joint load (lb) |
| K | Spring rate (lb/in.) |
| K ${ }_{\text {B }}$ | Spring rate of Bolt (lb/in.) |
| KJ | Spring rate of Joint (lb/in.) |
| K | Spring rate of Bolt part Ix (lb/in.) |
| 1 | Length (in.) |
| $\Delta 1$ | Change in length (in.) |
| $\mathrm{l}_{\mathrm{B}}$ | Length of Bolt (in.) |
| $\Delta_{\text {l }}$ | Bolt elongation due to $\mathrm{Fi}_{\text {( }}$ (in.) |
| $1 J$ | Length of Joint (in.) |
| $\Delta \mathrm{l}$ | Joint compression to $\mathrm{Fi}_{\text {i }}$ (in.) |
| $\mathrm{I}_{\mathrm{x}}$ | Length of Bolt part x (in.) |
| n | Length of clamped parts |
| n | Total Joint Length |
| a | Tightening factor |
| Ф | Force ratio |
| $\lambda$ | Bolt and Joint elongation due to $\mathrm{F}_{\mathrm{e}}$ (in.) |
| $\sigma_{B}$ | Bolt stress amplitude ( $\pm \mathrm{psi}$ ) |

## TIGHTENING TORQUES AND THE TORQUE-TENSION RELATIONSHIP

All of the analysis and design work done in advance will have little meaning if the proper preload is not achieved. Several discussions in this technical section stress the importance of preload to maintaining joint integrity. There are many methods for measuring preload (see Table 12). However, one of the least expensive techniques that provides a reasonable level of accuracy versus cost is by measuring torque. The fundamental characteristic required is to know the relationship between torque and tension for any particular bolted joint. Once the desired design preload must be identified and specified first, then the torque required to induce that preload is determined.

Within the elastic range, before permanent stretch is induced, the relationship between torque and tension is essentially linear (see figure 13). Some studies have found up to 75 variables have an effect on this relationship: materials, temperature, rate of installation, thread helix angle, coefficients of friction, etc. One way that has been developed to reduce the complexity is to depend on empirical test results. That is, to perform experiments under the application conditions by measuring the induced torque and recording the resulting tension. This can be done with relatively simple, calibrated hydraulic pressure sensors, electric strain gages, or piezoelectric load cells. Once the data is gathered and plotted on a chart, the slope of the curve can be used to calculate a correlation factor. This technique has created an accepted formula for relating torque to tension.
$T=K \times D \times P$
T = torque, lbf.-in.
$D=$ fastener nominal diameter, inches
$\mathrm{P}=$ preload, lbf.
$\mathrm{K}=$ "nut factor," "tightening factor," or "k-value"
If the preload and fastener diameter are selected in the design process, and the K-value for the application conditions is known, then the necessary torque can be calculated. It is noted that even with a specified torque, actual conditions at the time of installation can result in variations in the actual preload achieved (see Table 12).
One of the most critical criteria is the selection of the K-value. Accepted nominal values for many industrial applications are:
$\mathrm{K}=0.20$ for as-received steel bolts into steel holes
$\mathrm{K}=0.15$ steel bolts with cadmium plating, which acts like a lubricant,
$\mathrm{K}=0.28$ steel bolts with zinc plating.
The K-value is not the coefficient of the friction ( $\mu$ ); it is an empirically derived correlation factor.

It is readily apparent that if the torque intended for a zinc plated fastener is used for cadmium plated fastener, the preload will be almost two times that intended; it may actually cause the bolt to break.

Another influence is where friction occurs. For steel bolts holes, approximately $50 \%$ of the installation torque is consumed by friction under the head, $35 \%$ by thread friction, and only the remaining $15 \%$ inducing preload tension. Therefore, if lubricant is applied just on the
fastener underhead, full friction reduction will not be achieved. Similarly, if the material against which the fastener is bearing, e.g. aluminum, is different than the internal thread material, e.g. cast iron, the effective friction may be difficult to predict, These examples illustrate the importance and the value of identifying the torque-tension relationship. It is a recommend practice too contact the lubricant manufacturer for K-value information if a lubricant will be used.

The recommended seating torques for Unbrako headed socket screws are based on inducing preloads reasonably expected in practice for each type. The values for Unbrako metric fasteners are calculated using VDI2230, a complex method utilized extensively in Europe. All values assume use in the received condition in steel holes. It is understandable the designer may need preloads higher than those listed. The following discussion is presented for those cases.

## TORSION-TENSION YIELD AND TENSION CAPABILITY AFTER TORQUING

Once a headed fastener has been seated against a bearing surface, the inducement of torque will be translated into both torsion and tension stresses. These stresses combine to induce twist. If torque continues to be induced, the stress along the angle of twist will be the largest stress while the bolt is being torqued. Consequently, the stress along the bolt axis (axial tension) will be something less. This is why a bolt can fail at a lower tensile stress during installation than when it is pulled in straight tension alone, eg . a tensile test. Research has indicated the axial tension can range from 135,000 to 145,000 PSI for industry socket head cap screws at torsion-tension yield, depending on diameter. Including the preload variation that can occur with various installation techniques, eg. up to $25 \%$, it can be understood why some recommended torques induce preload reasonably lower than the yield point.

Figure 13 also illustrates the effect of straight tension applied after installation has stopped. Immediately after stopping the installation procedure there will be some relaxation, and the torsion component will drop toward zero. This leaves only the axial tension, which keeps the joint clamped together. Once the torsion is relieved, the axial tension yield value and ultimate value for the fastener will be appropriate.

Table 12
Industrial Fasteners Institute's
Torque-Measuring Method

| Preload Measuring <br> Method | Accuracy <br> Percent | Relative <br> Cost |
| :--- | :---: | :---: |
| Feel (operator's judgement) | $\pm 35$ | 1 |
| Torque wrench | $\pm 25$ | 1.5 |
| Turn of the nut | $\pm 15$ | 3 |
| Load-indicating washers | $\pm 10$ | 7 |
| Fastener elongation | $\pm 3$ to 5 | 15 |
| Strain gages | $\pm 1$ | 20 |

Fig. 14


Fig. 13 Torque/Tension Relationship


Elongation (in.)

Fig. 15 Recommended Seating Torques (Inch-Lb.) for Application in Various Materials UNBRAKO pHd (1960 Series) Socket Head Cap Screws

|  | mild steel Rb 87 cast iron Rb 83 note 1 |  | brass Rb 72 note 2 |  | aluminum Rb 72 (2024-T4) note 3 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | UNC | UNF | UNC | UNF | UNC | UNF |
| $\begin{aligned} & \text { screw } \\ & \text { size } \end{aligned}$ | plain | plain | plain | plain | plain | plain |
| $\begin{aligned} & \# 0 \\ & \# 1 \\ & \# 2 \\ & \hline \end{aligned}$ | $\begin{gathered} - \\ \text { *3.8 } \\ \text { *6.3 } \end{gathered}$ | $\begin{gathered} \text { *2.1 } \\ \text { *4.1 } \\ \text { *6.8 } \\ \hline \end{gathered}$ | $\begin{aligned} & \text { * } 3.8 \\ & \text { *6.3 } \end{aligned}$ | $\begin{aligned} & \text { *2.1 } \\ & \text { *4.1 } \\ & \text { *6.8 } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { * } \\ & \text { *6.8 } \\ & \text { *6.3 } \end{aligned}$ | $\begin{aligned} & \text { *2.1 } \\ & \text { *4.1 } \\ & \text { *6.8 } \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \# 3 \\ & \# 4 \\ & \# 5 \end{aligned}$ | $\begin{gathered} \text { *9.6 } \\ \text { *13.5 } \\ \text { *20 } \end{gathered}$ | $\begin{aligned} & \text { *10.3 } \\ & \text { *14.8 } \\ & \text { *21 } \end{aligned}$ | $\begin{aligned} & \text { *9.6 } \\ & \text { *13.5 } \\ & \text { *20 } \end{aligned}$ | $\begin{aligned} & \text { *10.3 } \\ & \text { *14.8 } \\ & \text { *21 } \end{aligned}$ | $\begin{aligned} & \text { *9.6 } \\ & \text { *13.5 } \\ & \text { *20 } \end{aligned}$ | $\begin{aligned} & \text { *10.3 } \\ & \text { *14.8 } \\ & \text { *21 } \end{aligned}$ |
| $\begin{gathered} \hline \# 6 \\ \# 8 \\ \# 10 \end{gathered}$ | $\begin{aligned} & \text { *25 } \\ & \text { *46 } \\ & \text { *67 } \end{aligned}$ | $\begin{aligned} & \text { *28 } \\ & \text { *48 } \\ & \text { *76 } \end{aligned}$ | $\begin{aligned} & \text { *25 } \\ & \text { *46 } \\ & \text { *67 } \end{aligned}$ | $\begin{aligned} & \text { *28 } \\ & \text { *48 } \\ & \text { *76 } \end{aligned}$ | $\begin{aligned} & \text { *25 } \\ & \text { *46 } \\ & \text { *67 } \end{aligned}$ | $\begin{aligned} & \text { *28 } \\ & \text { *48 } \\ & \text { *76 } \end{aligned}$ |
| $\begin{gathered} 1 / 4 \\ 5 / 16 \\ 3 / 8 \\ \hline \end{gathered}$ | $\begin{aligned} & \text { *158 } \\ & \text { *326 } \\ & \text { *580 } \end{aligned}$ | $\begin{array}{r} \text { *180 } \\ \text { *360 } \\ 635 \end{array}$ | $\begin{aligned} & 136 \\ & 228 \\ & 476 \\ & \hline \end{aligned}$ | $\begin{aligned} & 136 \\ & 228 \\ & 476 \\ & \hline \end{aligned}$ | $\begin{aligned} & 113 \\ & 190 \\ & 397 \\ & \hline \end{aligned}$ | $\begin{array}{r} 113 \\ 190 \\ 397 \\ \hline \end{array}$ |
| $\begin{gathered} 7 / 16 \\ 1 / 2 \\ 9 / 16 \end{gathered}$ | $\begin{array}{r} \text { *930 } \\ \text { *1,420 } \\ \text { *2,040 } \end{array}$ | $\begin{array}{r} \text { *1,040 } \\ \text { *1,590 } \\ 2,250 \\ \hline \end{array}$ | $\begin{gathered} 680 \\ 1,230 \\ 1,690 \end{gathered}$ | $\begin{array}{r} 680 \\ 1,230 \\ 1,690 \end{array}$ | $\begin{array}{r} 570 \\ 1,030 \\ 1,410 \end{array}$ | $\begin{array}{r} 570 \\ 1,030 \\ 1,410 \end{array}$ |
| $\begin{aligned} & 5 / 8 \\ & 3 / 4 \\ & 7 / 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { *2,820 } \\ & \text { *5,000 } \\ & \text { *8,060 } \end{aligned}$ | $\begin{aligned} & 3,120 \\ & 5,340 \\ & 8,370 \end{aligned}$ | $\begin{aligned} & 2,340 \\ & 4,000 \\ & 6,280 \end{aligned}$ | $\begin{aligned} & 2,340 \\ & 4,000 \\ & 6,280 \end{aligned}$ | $\begin{aligned} & 1,950 \\ & 3,340 \\ & 5,230 \end{aligned}$ | $\begin{aligned} & 1,950 \\ & 3,340 \\ & 5,230 \\ & \hline \end{aligned}$ |
| $\begin{array}{cc} 1 \\ 1 & 1 / 8 \\ 1 & 1 / 4 \end{array}$ | $\begin{aligned} & \text { *12,100 } \\ & \text { *13,800 } \\ & \text { *19,200 } \\ & \hline \end{aligned}$ | $\begin{array}{r} 12,800 \\ * 15,400 \\ * 21,600 \end{array}$ | $\begin{gathered} \hline 9,600 \\ 13,700 \\ 18,900 \\ \hline \end{gathered}$ | 9,600 <br> 13,700 <br> 18,900 | $\begin{array}{r} 8,000 \\ 11,400 \\ 15,800 \end{array}$ | $\begin{array}{r} 8,000 \\ 11,400 \\ 15,800 \\ \hline \end{array}$ |
| $\begin{aligned} & 13 / 8 \\ & 1 \text { 1/2 } \end{aligned}$ | $\begin{aligned} & \text { *25,200 } \\ & \text { *33,600 } \end{aligned}$ | $\begin{aligned} & * 28,800 \\ & * 36,100 \end{aligned}$ | $\begin{aligned} & 24,200 \\ & 32,900 \end{aligned}$ | $\begin{aligned} & 24,200 \\ & 32,900 \end{aligned}$ | $\begin{aligned} & 20,100 \\ & 27,400 \end{aligned}$ | $\begin{aligned} & 20,100 \\ & 27,400 \end{aligned}$ |

## NOTES:

1. Torques based on 80,000 psi bearing stress under head of screw.
2. Torques based on 60,000 psi bearing stress under head of screw.
3. Torques based on 50,000 psi bearing stress under head of screw.
*Denotes torques based on 100,000 psi tensile stress in screw threads up to 1 " dia., and 80,000 psi for sizes 1 1/8" dia. and larger. To convert inch-pounds to inch-ounces - multiply by 16.
To convert inch-pounds to foot-pounds - divide by 12.

## STRIPPING STRENGTH OF TAPPED HOLES

Charts and sample problems for obtaining minimum thread engagement based on applied load, material, type of thread and bolt diameter.
Knowledge of the thread stripping strength of tapped holes is necessary to develop full tensile strength of the bolt or, for that matter, the minimum engagement needed for any lesser load.

Conversely, if only limited length of engagement is available, the data help determine the maximum load that can be safely applied without stripping the threads of the tapped hole.

Attempts to compute lengths of engagement and related factors by formula have not been entirely satisfactorymainly because of subtle differences between various materials. Therefore, strength data has been empirically developed from a series of tensile tests of tapped specimens for seven commonly used metals including steel, aluminum, brass and cast iron.

The design data is summarized in the six accompanying charts, (Charts E504-E509), and covers a range of screw thread sizes from \#0 to one inch in diameter for both coarse and fine threads. Though developed from tests of Unbrako socket head cap screws having minimum ultimate tensile strengths (depending on the diameter) from 190,000 to 180,000 psi , these stripping strength values are valid for all other screws or bolts of equal or lower strength having a standard thread form. Data are based on static loading only.

In the test program, bolts threaded into tapped specimens of the metal under study were stressed in tension until the threads stripped. Load at which stripping occurred and the length of engagement of the specimen were noted. Conditions of the tests, all of which are met in a majority of industrial bolt applications, were:

- Tapped holes had a basic thread depth within the range of 65 to 80 per cent. Threads of tapped holes were Class 2B fit or better.
- Minimum amount of metal surrounding the tapped hole was $21 / 2$ times the major diameter.
- Test loads were applied slowly in tension to screws having standard Class 3 A threads. (Data, though, will be equally applicable to Class 2A external threads as well.)
- Study of the test results revealed certain factors that greatly simplified the compilation of thread stripping strength data:
- Stripping strengths are almost identical for loads applied either by pure tension or by screw torsion. Thus data are equally valid for either condition of application.
- Stripping strength values vary with diameter of screw. For a given load and material, larger diameter bolts required greater engagement.
- Minimum length of engagement (as a percent of screw diameter) is a straight line function of load. This permits easy interpolation of test data for any intermediate load condition.
- When engagement is plotted as a percentage of bolt diameter, it is apparent that stripping strengths for a wide range of screw sizes are close enough to be grouped in a single curve. Thus, in the accompanying charts, data for sizes \#0 through \#12 have been represented by a single set of curves.

With these curves, it becomes a simple matter to determine stripping strengths and lengths of engagement for any condition of application. A few examples are given below:

Example 1. Calculate length of thread engagement necessary to develop the minimum ultimate tensile strength (190,000 psi) of a 1/2-13 (National Coarse) Unbrako cap screw in cast iron having an ultimate shear strength of 30,000 psi. E505 is for screw sizes from \#0 through \#10; E506 and E507 for sizes from 1/4 in. through 5/8 in.; E508 and E509 for sizes from 3/4 in. through 1 in. Using E506 a value 1.40D is obtained. Multiplying nominal bolt diameter ( 0.500 in .) by 1.40 gives a minimum length of engagement of 0.700 in .

Example 2. Calculate the length of engagement for the above conditions if only 140,000 psi is to be applied. (This is the same as using a bolt with a maximum tensile strength of 140,000 psi.) From E506 obtain value of 1.06 D Minimum length of engagement $=(0.500)(1.06)=0.530$.

Example 3. Suppose in Example 1 that minimum length of engagement to develop full tensile strength was not available because the thickness of metal allowed a tapped hole of only 0.600 in . Hole depth in terms of bolt dia. $=0.600 / 0.500=1.20 \mathrm{D}$. By working backwards in Fig. 2, maximum load that can be carried is approximately 159,000 psi.

Example 4. Suppose that the hole in Example 1 is to be tapped in steel having an ultimate shear strength 65,000 psi. There is no curve for this steel in E506 but a design value can be obtained by taking a point midway between curves for the $80,000 \mathrm{psi}$ and 50,000 psi steels that are listed. Under the conditions of the example, a length of engagement of 0.825 D or 0.413 in . will be obtained.




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## HIGH-TEMPERATURE JOINTS

Bolted joints subjected to cyclic loading perform best if an initial preload is applied. The induced stress minimizes the external load sensed by the bolt, and reduces the chance of fatigue failure. At high temperature, the induced load will change, and this can adversely affect the fastener performance. It is therefore necessary to compensate for high-temperature conditions when assembling the joint at room temperature. This article describes the factors which must be considered and illustrates how a high-temperature bolted joint is designed.

In high-temperature joints, adequate clamping force or preload must be maintained in spite of temperatureinduced dimensional changes of the fastener relative to the joint members. the change in preload at any given temperature for a given time can be calculated, and the affect compensated for by proper fastener selection and initial preload.

Three principal factors tend to alter the initial clamping force in a joint at elevated temperatures, provided that the fastener material retains requisite strength at the elevated temperature. These factors are: Modulus of elasticity, coefficient of thermal expansion, and relaxation.

Modulus Of Elasticity: As temperature increases, less stress or load is needed to impart a given amount of elongation or strain to a material than at lower temperatures. This means that a fastener stretched a certain amount at room temperature to develop a given preload will exert a lower clamping force at higher temperature if there is no change in bolt elongation.

Coefficient of Expansion: With most materials, the size of the part increases as the temperature increases. In a joint, both the structure and the fastener grow with an increase in temperature, and this can result, depending on the materials, in an increase or decrease in the clamping force. Thus, matching of materials in joint design can assure sufficient clamping force at both room and elevated temperatures. Table 16 lists mean coefficient of thermal expansion of certain fastener alloys at several temperatures.

Relaxation: At elevated temperatures, a material subjected to constant stress below its yield strength will flow plastically and permanently change size. This phenomenon is called creep. In a joint at elevated temperature, a fastener with a fixed distance between the bearing surface of the head and nut will produce less and less clamping force with time. This characteristic is called relaxation. It differs from creep in that stress changes while elongation or strain remains constant. Such elements as material, temperature, initial stress, manufacturing method, and design affect the rate of relaxation.

Relaxation is the most important of the three factors. It is also the most critical consideration in design of elevatedtemperature fasteners. A bolted joint at $1200^{\circ} \mathrm{F}$ can lose as much as 35 per cent of preload. Failure to compensate for this could lead to fatigue failure through a loose joint even though the bolt was properly tightened initially.

If the coefficient of expansion of the bolt is greater than that of the joined material, a predictable amount of clamping force will be lost as temperature increases. Conversely, if the coefficient of the joined material is greater, the bolt may be stressed beyond its yield or even fracture strength. Or, cyclic thermal stressing may lead to thermal fatigue failure.

Changes in the modulus of elasticity of metals with increasing temperature must be anticipated, calculated, and compensated for in joint design. Unlike the coefficient of expansion, the effect of change in modulus is to reduce clamping force whether or not bolt and structure are the same material, and is strictly a function of the bolt metal.

Since the temperature environment and the materials of the structure are normally "fixed," the design objective is to select a bolt material that will give the desired clamping force at all critical points in the operating range of the joint. To do this, it is necessary to balance out the three factorsrelaxation, thermal expansion, and modulus-with a fourth, the amount of initial tightening or clamping force.

In actual joint design the determination of clamping force must be considered with other design factors such as ultimate tensile, shear, and fatigue strength of the fastener at elevated temperature. As temperature increases the inherent strength of the material decreases. Therefore, it is important to select a fastener material which has sufficient strength at maximum service temperature.

## Example

The design approach to the problem of maintaining satisfactory elevated-temperature clamping force in a joint can be illustrated by an example. The example chosen is complex but typical. A cut-and-try process is used to select the right bolt material and size for a given design load under a fixed set of operating loads and environmental conditions, Fig.17.

The first step is to determine the change in thickness, $\Delta t$, of the structure from room to maximum operating temperature.

For the AISI 4340 material:
$\Delta t_{1}=t_{1}\left(T_{2}-T_{1}\right) \alpha$
$\Delta t_{1}=(0.05)(800-70)\left(7.4 \times 10^{-6}\right)$
$\Delta t_{1}=0.002701 \mathrm{in}$.
For the AMS 6304 material:
$\Delta t_{2}=(0.75)(800-70)\left(7.6 \times 10^{-6}\right)$
$\Delta t_{2}=0.004161 \mathrm{in}$.
The total increase in thickness for the joint members is 0.00686 in.

The total effective bolt length equals the total joint thickness plus one-third of the threads engaged by the nut. If it is assumed that the smallest diameter bolt should be used for weight saving, then a $1 / 4-i n$. bolt should be tried. Thread engagement is approximately one diameter, and the effective bolt length is:

$d=$ Bolt diam, in.
$E=$ Modulus of elasticity, psi
$F_{b}=$ Bolt preload, lb
$F_{c}=$ Clamping force, lb
( $\mathrm{Fb}=\mathrm{F}_{\mathrm{c}}$ )
$F_{w}=$ Working load $=1500 \mathrm{lb}$
static + 100 lb cyclic
$T_{1}=$ Room temperature $=70^{\circ} \mathrm{F}$
$T_{2}=$ Maximum operatng temperature for $1000 \mathrm{hr}=800^{\circ} \mathrm{F}$
$t=$ Panel thickness, in.
$a=$ Coefficient of thermal expansion
$L=$ Effective bolt length, inc.
Fig. 17 - Parameters for joint operating at $800^{\circ} \mathrm{F}$.
$L=\mathrm{t}_{1}+\mathrm{t}_{2}+(1 / 3 \mathrm{~d})$
$L=0.50+0.75+(1 / 3 \times 0.25)$
$L=1.333 \mathrm{in}$.
The ideal coefficient of thermal expansion of the bolt material is found by dividing the total change in joint thickness by the bolt length times the change in temperature.
$\mathrm{ab}=\frac{\Delta \mathrm{t}}{\mathrm{LX} \Delta \mathrm{t}}$
$\alpha=\frac{.00686}{(1.333)(800-70)}=7.05 \times 10^{-6} \mathrm{in} . / \mathrm{in} . /$ deg. F
The material, with the nearest coefficient of expansion is with a value of $9,600,000$ at $800^{\circ} \mathrm{F}$.

To determine if the bolt material has sufficient strength and resistance to fatigue, it is necessary to calculate the stress in the fastener at maximum and minimum load. The bolt load plus the cyclic load divided by the tensile stress of the threads will give the maximum stress. For a 1/4-28 bolt, tensile stress area, from thread handbook H 28 , is 0.03637 sq. in. The maximum stress is
$S_{\max }=\frac{\text { Bolt load }}{\text { Stress area }}=\frac{1500+100}{0.03637}$
$S_{\text {max }}=44,000 \mathrm{psi}$
and the minimum bolt stress is 41,200 psi.
$\mathrm{H}-11$ has a yield strength of 175,000 psi at $800^{\circ} \mathrm{F}$, Table 3, and therefore should be adequate for the working loads.

A Goodman diagram, Fig. 18, shows the extremes of stress within which the $\mathrm{H}-11$ fastener will not fail by fatigue. At the maximum calculated load of $44,000 \mathrm{psi}$, the fastener will withstand a minimum cyclic loading at $800^{\circ} \mathrm{F}$ of about 21,000 psi without fatigue failure.


Fig. 18 - Goodman diagram of maximum and minimum operating limits for $\mathrm{H}-11$ fastener at $800^{\circ} \mathrm{F}$. Bolts stressed within these limits will give infinite fatigue life.

Because of relaxation, it is necessary to determine the initial preload required to insure 1500-lb. clamping force in the joint after 1000 hr at $800^{\circ} \mathrm{F}$.

When relaxation is considered, it is necessary to calculate the maximum stress to which the fastener is subjected. Because this stress is not constant in dynamic joints, the resultant values tend to be conservative. Therefore, a maximum stress of 44,000 psi should be considered although the necessary stress at $800^{\circ} \mathrm{F}$ need be only 41,200 psi. Relaxation at 44,000 psi can be interpolated from the figure, although an actual curve could be constructed from tests made on the fastener at the specific conditions.

The initial stress required to insure a clamping stress of 44,000 psi after 1000 hr at $800^{\circ} \mathrm{F}$ can be calculated by interpolation.
$x=61,000-44,000=17,000$
$y=61,000-34,000=27,000$
$B=80,000-50,000=30,000$
$A=80,000-C$
$\frac{x}{y}=\frac{A}{B} \quad \frac{17,000}{27,000}=\frac{80,000-C}{30,000}$
C $=61,100 \mathrm{psi}$

The bolt elongation required at this temperature is calculated by dividing the stress by the modulus at temperature and multiplying by the effective length of the bolt. That is: $(61,000 \times 1.333) / 24.6 \times 10^{6}=0.0033$

Since the joint must be constructed at room temperature, it is necessary to determine the stresses at this state. Because the modulus of the fastener material changes with temperature, the clamping force at room temperature will not be the same as at $800^{\circ} \mathrm{F}$. To determine
the clamping stress at assembly conditions, the elongation should be multiplied by the modulus of elasticity at room temperature.
$.0033 \times 30.6 \times 10^{6}=101,145 \mathrm{psi}$
The assembly conditions will be affected by the difference between th ideal and actual coefficients of expansion of the joint. The ideal coeffienct for the fastener material was calculated to be 7.05 but the closest material - H-11 has a coefficient of 7.1. Since this material has a greater expansion than calculated, there will be a reduction in clamping force resulting from the increase in temperature. This amount equals the difference between the ideal and the actual coefficients multiplied by the change in temperature, the length of the fastener, and the modulus of elasticity at $70^{\circ} \mathrm{F}$.
[(7.1-7.05) X 10 ${ }^{-6}$ [ $\left.800-70\right][1.333] \times$
$\left[30.6 \times 10^{6}\right]=1,490 \mathrm{psi}$
The result must be added to the initial calculated stresses to establish the minimum required clamping stress needed for assembling the joint at room temperature.
$101,145+1,490=102,635 \mathrm{psi}$
Finally, the method of determining the clamping force or preload will affect the final stress in the joint at operating conditions. For example, if a torque wrench is used to
apply preload (the most common and simplest method available), a plus or minus 25 per cent variation in induced load can result. Therefore, the maximum load which could be expected in this case would be 1.5 times the minimum, or:
$(1.5)(102,635)=153,950 \mathrm{psi}$
This value does not exceed the room-temperature yield strength for $\mathrm{H}-11$ given in Table 19.

Since there is a decrease in the clamping force with an increase in temperature and since the stress at operating temperature can be higher than originally calculated because of variations in induced load, it is necessary to ascertain if yield strength at $800^{\circ} \mathrm{F}$ will be exceeded

$$
\begin{aligned}
& \frac{\left(m a x \text { stress at } 70^{\circ} \mathrm{F}+\text { change in stress) } \times \mathrm{E} \text { at } 800^{\circ} \mathrm{F}\right.}{E \text { at } 70^{\circ} \mathrm{F}} \\
& \frac{[153,950+(-1490)] \times 24.6 \times 10^{6}}{30.6 \times 10^{6}}=122,565
\end{aligned}
$$

This value is less than the yield strength for $\mathrm{H}-11$ at $800^{\circ} \mathrm{F}$, Table 19. Therefore, a $1 / 4-28 \mathrm{H}-11$ bolt stressed between 102,635 psi and 153,950 psi at room temperature will maintain a clamping load 1500 lb at $800^{\circ} \mathrm{F}$ after 1000 hr of operation. A cyclic loading of 100 lb , which results in a bolt loading between 1500 and 1600 lb will not cause fatigue failure at the operating conditions.

Table 16

## PHYSICAL PROPERTIES OF MATERIALS USED TO MANUFACTURE ALLOY STEEL SHCS'S

Coefficient of Thermal Expansion, $\mu \mathrm{m} / \mathrm{m} /{ }^{\circ} \mathrm{K}^{1}$

| $20^{\circ} \mathrm{C}$ to | $\mathbf{1 0 0}$ | $\mathbf{2 0 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | $\mathbf{5 0 0}$ | $\mathbf{6 0 0}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{6 8}{ }^{\circ} \mathrm{F}$ to | $\mathbf{2 1 2}$ | $\mathbf{3 9 2}$ | $\mathbf{5 7 2}$ | $\mathbf{7 5 2}$ | $\mathbf{9 3 2}$ | $\mathbf{1 1 1 2}$ |
| Material |  |  |  |  |  |  |
| 5137 M, <br> $51 \mathrm{~B} 37 \mathrm{M}^{2}$ | - | 12.6 | 13.4 | 13.9 | 14.3 | 14.6 |
| $4137^{3}$ | 11.2 | 11.8 | 12.4 | 13.0 | 13.6 | - |
| $4140^{3}$ | 12.3 | 12.7 | - | 13.7 | - | 14.5 |
| $4340^{3}$ | - | 12.4 | - | 13.6 | - | 14.5 |
| $8735^{3}$ | 11.7 | 12.2 | 12.8 | 13.5 | - | 14.1 |
| $8740^{3}$ | 11.6 | 12.2 | 12.8 | 13.5 | - | 14.1 |

Modulus of Elongation (Young's Modulus)
$E=30,000,000 \mathrm{PSI} / \mathrm{in} / \mathrm{in}$

Table 19 - Yield Strength at Various Temperatures

| Alloy | Temperature (F) |  |  |  |  |
| :--- | ---: | ---: | ---: | :---: | :---: |
|  | $\mathbf{7 0}$ | $\mathbf{8 0 0}$ | $\mathbf{1 0 0 0}$ | $\mathbf{1 2 0 0}$ |  |
| Stainless Steels |  |  |  |  |  |
| Type 302 | 35,000 | 35,000 | 34,000 | 30,000 |  |
| Type 403 | 145,000 | 110,000 | 95,000 | 38,000 |  |
| PH 15-7 Mo | 220,000 | 149,000 | 101,000 | - |  |


| High Strength Iron-Base Stainless Alloys |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| A 286 | 95,000 | 95,000 | 90,000 | 85,000 |
| AMS 5616 | 113,000 | 80,000 | 60,000 | 40,000 |
| Unitemp 212 | 150,000 | 140,000 | 135,000 | 130,000 |


| High Strength Iron-Base Alloys |  |  |  |  |  |
| :--- | ---: | :--- | ---: | :--- | :---: |
| AISI 4340 | 200,000 | 130,000 | 75,000 | - |  |
| H-11 AMS 6485) | 215,000 | 175,000 | 155,000 | - |  |
| AMS 6340 | 160,000 | 100,000 | 75,000 | - |  |
| Nickel-Base Alloys |  |  |  |  |  |
| Iconel X | 115,000 | - | - | 98,000 |  |
| Waspaloy | 115,000 | - | 106,000 | 100,000 |  |

## NOTES:

1. Developed from ASM, Metals HDBK, 9th Edition, Vol. $1\left({ }^{\circ} \mathrm{C}={ }^{\circ} \mathrm{K}\right.$ for values listed)
2. ASME SA574
3. AISI
4. Multiply values in table by .556 for $\mu \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F}$.

All fastened joints are, to some extent, subjected to corrosion of some form during normal service life. Design of a joint to prevent premature failure due to corrosion must include considerations of the environment, conditions of loading, and the various methods of protecting the fastener and joint from corrosion.

Three ways to protect against corrosion are:

1. Select corrosion-resistant material for the fastener.
2. Specify protective coatings for fastener, joint interfaces, or both.
3. Design the joint to minimize corrosion.

The solution to a specific corrosion problem may require using one or all of these methods. Economics often necessitate a compromise solution.

Fastener Material
The use of a suitably corrosion-resistant material is often the first line of defense against corrosion. In fastener design, however, material choice may be only one of several important considerations. For example, the most corrosion-resistant material for a particular environment may just not make a suitable fastener.

Basic factors affecting the choice of corrosion resistant threaded fasteners are:

- Tensile and fatigue strength.
- Position on the galvanic series scale of the fastener and materials to be joined.
- Special design considerations: Need for minimum weight or the tendency for some materials to gall.
- Susceptibility of the fastener material to other types of less obvious corrosion. For example, a selected material may minimize direct attack of a corrosive environment only to be vulnerable to fretting or stress corrosion.

Some of the more widely used corrosion-resistant materials, along with approximate fastener tensile strength ratings at room temperature and other pertinent properties, are listed in Table 1. Sometimes the nature of corrosion properties provided by these fastener materials is subject to change with application and other condi-
tions.For example, stainless steel and aluminum resist corrosion only so long as their protective oxide film remains unbroken. Alloy steel is almost never used, even under mildly corrosive conditions, without some sort of protective coating. Of course, the presence of a specific corrosive medium requires a specific corrosion-resistant fastener material, provided that design factors such as tensile and fatigue strength can be satisfied.

## Protective Coating

A number of factors influence the choice of a corrosionresistant coating for a threaded fastener. Frequently, the corrosion resistance of the coating is not a principal consideration. At times it is a case of economics. Often, less-costly fastener material will perform satisfactorily in a corrosive environment if given the proper protective coating.

Factors which affect coating choice are:

- Corrosion resistance
- Temperature limitations
- Embrittlement of base metal
- Effect on fatigue life
- Effect on locking torque
- Compatibility with adjacent material
- Dimensional changes
- Thickness and distribution
- Adhesion characteristics

Conversion Coatings: Where cost is a factor and corrosion is not severe, certain conversion-type coatings are effective. These include a black-oxide finish for alloysteel screws and various phosphate base coatings for carbon and alloy-steel fasteners. Frequently, a rustpreventing oil is applied over a conversion coating.

Paint: Because of its thickness, paint is normally not considered for protective coatings for mating threaded fasteners. However, it is sometimes applied as a supplemental treatment at installation. In special cases, a fastener may be painted and installed wet, or the entire joint may be sealed with a coat of paint after installation.

TABLE 1 - TYPICAL PROPERTIES OF CORROSION RESISTANT FASTENER MATERIALS

| Materials <br> Stainless Steel | Tensile <br> Strength <br> (1000 $\mathbf{~ p s i )}$ | Yield Strength <br> at $\mathbf{0 . 2 \%}$ offset <br> (1000 $\mathbf{p s i}$ ) | Maximum <br> Service <br> Temp (F) | Mean Coefficient <br> of Thermal Expan. <br> (in./In./deg F) | Density <br> (Ibs/cu in.) | Base Cost <br> Index | Position <br> on Galvanic <br> Scale |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 303, passive | 80 | 40 | 800 | 10.2 | 0.286 | Medium | 8 |
| 303, passive, cold worked | 125 | 80 | 800 | 10.3 | 0.286 | Medium | 9 |
| 410, passive | 170 | 110 | 400 | 5.6 | 0.278 | Low | 15 |
| 431, passive | 180 | 140 | 400 | 6.7 | 0.280 | Medium | 16 |
| 17-4 PH | 200 | 180 | 600 | 6.3 | 0.282 | Medium | 11 |
| 17-7 PH | 200 | 185 | 600 | 6.7 | 0.276 | Medium | 14 |
| AM 350 | 200 | 162 | 800 | 7.2 | 0.282 | Medium | 13 |
| 15-7 Mo | 200 | 155 | 600 | - | 0.277 | Medium | 12 |
| A-286 | 150 | 85 | 1200 | 9.72 | 0.286 | Medium | 6 |
| A-286, cold worked | 220 | 170 | 1200 | - | 0.286 | High | 7 |

Electroplating: Two broad classes of protective electroplating are: 1. The barrier type-such as chrome plating-which sets up an impervious layer or film that is more noble and therefore more corrosion resistant than the base metal. 2. The sacrificial type, zinc for example, where the metal of the coating is less noble than the base metal of the fastener. This kind of plating corrodes sacrificially and protects the fastener.

Noble-metal coatings are generally not suitable for threaded fasteners-especially where a close-tolerance fit is involved. To be effective, a noble-metal coating must be at least 0.001 in. thick. Because of screw-thread geometry, however, such plating thickness will usually exceed the tolerance allowances on many classes of fit for screws.

Because of dimensional necessity, threaded fastener coatings, since they operate on a different principle, are effective in layers as thin as 0.0001 to 0.0002 in.

The most widely used sacrificial platings for threaded fasteners are cadmium, zinc, and tin. Frequently, the cadmium and zinc are rendered even more corrosion resistant by a posting-plating chromate-type conversion treatment. Cadmium plating can be used at temperatures to $450^{\circ} \mathrm{F}$. Above this limit, a nickel cadmium or nickel-zinc alloy plating is recommended. This consists of alternate deposits of the two metals which are heat-diffused into a uniform alloy coating that can be used for applications to $900^{\circ} \mathrm{F}$. The alloy may also be deposited directly from the plating bath.

Fastener materials for use in the 900 to $1200^{\circ} \mathrm{F}$ range (stainless steel, A-286), and in the $1200^{\circ}$ to $1800^{\circ} \mathrm{F}$ range (high-nickel-base super alloys) are highly corrosion resistant and normally do not require protective coatings, except under special environment conditions.

Silver plating is frequently used in the higher temperature ranges for lubrication to prevent galling and seizing, particularly on stainless steel. This plating can cause a galvanic corrosion problem, however, because of the high nobility of the silver.

Hydrogen Embrittlement: A serious problem, known as hydrogen embrittlement, can develop in plated alloy steel fasteners. Hydrogen generated during plating can diffuse into the steel and embrittle the bolt. The result is often a delayed and total mechanical failure, at tensile levels far below the theoretical strength, high-hardness structural parts are particularly susceptible to this condition. The problem can be controlled by careful selection of plating formulation, proper plating procedure, and sufficient baking to drive off any residual hydrogen.

Another form of hydrogen embrittlement, which is more difficult to control, may occur after installation. Since electrolytic cell action liberates hydrogen at the cathode, it is possible for either galvanic or concentration-cell corrosion to lead to embrittling of the bolt material.

## Joint Design

Certain precautions and design procedures can be followed to prevent, or at least minimize, each of the various types of corrosion likely to attack a threaded joint. The most important of these are:

For Direct Attack: Choose the right corrosion resistant material. Usually a material can be found that will provide the needed corrosion resistance without sacrifice of other important design requirements. Be sure that the fastener material is compatible with the materials being joined.

Corrosion resistance can be increased by using a conversion coating such as black oxide or a phosphatebase treatment. Alternatively, a sacrificial coating such as zinc plating is effective

For an inexpensive protective coating, lacquer or paint can be used where conditions permit.

For Galvanic Corrosion: If the condition is severe, electrically insulate the bolt and joint from each other..

The fastener may be painted with zinc chromate primer prior to installation, or the entire joint can be coated with lacquer or paint.

Another protective measure is to use a bolt that is cathodic to the joint material and close to it in the galvanic series. When the joint material is anodic, corrosion will spread over the greater area of the fastened materials. Conversely, if the bolt is anodic, galvanic action is most severe.


FIG. 1.1-A method of electrically insulating a bolted joint to prevent galvanic corrosion.

## For Concentration-Cell Corrosion: Keep surfaces

 smooth and minimize or eliminate lap joints, crevices, and seams. Surfaces should be clean and free of organic material and dirt. Air trapped under a speck of dirt on the surface of the metal may form an oxygen concentration cell and start pitting.For maximum protection, bolts and nuts should have smooth surfaces, especially in the seating areas. Flushhead bolts should be used where possible. Further, joints can be sealed with paint or other sealant material.

For Fretting Corrosion: Apply a lubricant (usually oil) to mating surfaces. Where fretting corrosion is likely to occur: 1. Specify materials of maximum practicable hardness. 2. Use fasteners that have residual compressive stresses on the surfaces that may be under attack. 3. Specify maximum preload in the joint. A higher clamping force results in a more rigid joint with less relative movement possible between mating services.

For Stress Corrosion: Choose a fastener material that resists stress corrosion in the service environment. Reduce fastener hardness (if reduced strength can be tolerated), since this seems to be a factor in stress corrosion.

Minimize crevices and stress risers in the bolted joint and compensate for thermal stresses. Residual stresses resulting from sudden changes in temperature accelerate stress corrosion.

If possible, induce residual compressive stresses into the surface of the fastener by shot-peening or pressure rolling.

For Corrosion Fatigue: In general, design the joint for high fatigue life, since the principal effect of this form of corrosion is reduced fatigue performance. Factors extending fatigue performance are: 1. Application and maintenance of a high preload. 2. Proper alignment to avoid bending stresses.

If the environment is severe, periodic inspection is recommended so that partial failures may be detected before the structure is endangered.

As with stress and fretting corrosion, compressive stresses induced on the fastener surfaces by thread rolling, fillet rolling, or shot peening will reduce corrosion fatigue. Further protection is provided by surface coating.

## TYPES OF CORROSION

Direct Attack...most common form of corrosion affecting all metals and structural forms. It is a direct and general chemical reaction of the metal with a corrosive mediumliquid, gas, or even a solid.

Galvanic Corrosion...occurs with dissimilar metals contact. Presence of an electrolyte, which may be nothing more than an individual atmosphere, causes corrosive action in the galvanic couple. The anodic, or less noble material, is the sacrificial element. Hence, in a joint of stainless steel and titanium, the stainless steel corrodes. One of the worst galvanic joints would consist of magnesium and titanium in contact.

Concentration Cell Corrosion...takes place with metals in close proximity and, unlike galvanic corrosion, does not require dissimilar metals. When two or more areas on the surface of a metal are exposed to different concentrations of the same solution, a difference in electrical potential results, and corrosion takes place.

If the solution consists of salts of the metal itself, a metalion cell is formed, and corrosion takes place on the surfaces in close contact. The corrosive solution between the two surfaces is relatively more stagnant (and thus has a higher concentration of metal ions in solution) than the corrosive solution immediately outside the crevice.

A variation of the concentration cell is the oxygen cell in which a corrosive medium, such as moist air, contains different amounts of dissolved oxygen at different points. Accelerated corrosion takes place between hidden surfaces (either under the bolt head or nut, or between bolted materials) and is likely to advance without detection.

Fretting...corrosive attack or deterioration occurring between containing, highly-loaded metal surfaces subjected to very slight (vibratory) motion. Although the mechanism is not completely understood, it is probably a highly accelerated form of oxidation under heat and stress. In threaded joints, fretting can occur between mating threads, at the bearing surfaces under the head of the screw, or under the nut. It is most likely to occur in high tensile, high-frequency, dynamic-load applications. There need be no special environment to induce this form of corrosion...merely the presence of air plus vibratory rubbing. It can even occur when only one of the materials in contact is metal.

Stress Corrosion Cracking...occurs over a period of time in high-stressed, high-strength joints. Although not fully understood, stress corrosion cracking is believed to be caused by the combined and mutually accelerating effects of static tensile stress and corrosive environment. Initial pitting somehow tales place which, in turn, further increases stress build-up. The effect is cumulative and, in a highly stressed joint, can result in sudden failure.

Corrosion Fatigue...accelerated fatigue failure occurring in the presence of a corrosive medium. It differs from stress corrosion cracking in that dynamic alternating stress, rather than static tensile stress, is the contributing agent.

Corrosion fatigue affects the normal endurance limit of the bolt. The conventional fatigue curve of a normal bolt joint levels off at its endurance limit, or maximum dynamic load that can be sustained indefinitely without fatigue failure. Under conditions of corrosion fatigue, however, the curve does not level off but continues downward to a point of failure at a finite number of stress cycles.

## GALVANIC CORROSION



FIG. 19— Metals compatibility chart

## THE IMPACT PERFORMANCE OF THREADED FASTENERS

Much has been written regarding the significance of the notched bar impact testing of steels and other metallic materials. The Charpy and Izod type test relate notch behavior (brittleness versus ductility) by applying a single overload of stress. The results of these tests provide quantitive comparisons but are not convertible to energy values useful for engineering design calculations. The results of an individual test are related to that particular specimen size, notch geometry and testing conditions and cannot be generalized to other sizes of specimens and conditions.

The results of these tests are useful in determining the susceptibility of a material to brittle behavior when the applied stress is perpendicular to the major stress.

In externally threaded fasteners, however, the loading usually is applied in a longitudinal direction. The impact test, therefore, which should be applicable would be one where the applied impact stress supplements the major stress. Only in shear loading on fasteners is the major stress in the transverse direction.

Considerable testing has been conducted in an effort to determine if a relationship exists between the Charpy $V$ notch properties of a material and the tension properties of an externally threaded fastener manufactured from the same material.

Some conclusions which can be drawn from the extensive impact testing are as follows:

1. The tension impact properties of externally threaded fasteners do not follow the Charpy V notch impact pattern.
2. Some of the variables which effect the tension impact properties are:
A. The number of exposed threads
B. The length of the fastener
C. The relationship of the fastener shank diameter to the thread area.
D. The hardness or fastener ultimate tensile strength

Following are charts showing tension impact versus Charpy impact properties, the effect of strength and diameter on tension impact properties and the effect of test temperature.

Please note from figure 21 that while the Charpy impact strength of socket head cap screw materials are decreasing at sub-zero temperatures, the tension impact strength of the same screws is increasing. This compares favorable with the effect of cryogenic temperatures on the tensile strength of the screws. Note the similar increase in tensile strength shown in figure 22.

It is recommended, therefore, that less importance be attached to Charpy impact properties of materials which are intended to be given to impact properties for threaded fasteners. If any consideration is to be given to impact properties of bolts or screws, it is advisable to investigate the tension impact properties of full size fasteners since this more closely approximates the actual application.

TABLE 20
LOW-TEMPERATURE IMPACT PROPERTIES OF SELECTED ALLOY STEELS

| AISI no. | Composition, \% |  |  |  |  | Heat Temperature* |  | Hardness Rc | $\begin{aligned} & \text { Impact Energy, } \\ & \text { Ft.-lb } \end{aligned}$ |  |  |  |  | Transition <br> Temp. <br> (50\% <br> Brittle) <br> ${ }^{\circ} \mathrm{f}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | C | Mn | Ni | Cr | Mo | Temp. F+ | Temp. F |  | $-300^{\circ} \mathrm{F}$ | $-200^{\circ} \mathrm{F}$ | $-100^{\circ} \mathrm{F}$ | O ${ }^{\circ}$ | $10{ }^{\circ} \mathrm{F}$ |  |
| 4340 | 0.38 | 0.77 | 1.65 | 0.93 | 0.21 | 1550 | 400 | 52 | 11 | 15 | 20 | 21 | 21 | - |
|  |  |  |  |  |  |  | 600 | 48 | 10 | 14 | 15 | 15 | 16 | - |
|  |  |  |  |  |  |  | 800 | 44 | 9 | 13 | 16 | 21 | 25 | - |
|  |  |  |  |  |  |  | 1000 | 38 | 15 | 18 | 28 | 36 | 36 | -130 |
|  |  |  |  |  |  |  | 1200 | 30 | 15 | 28 | 55 | 55 | 55 | -185 |
| 4360 | 0.57 | 0.87 | 1.62 | 1.08 | 0.22 | 1475 | 800 | 48 | 5 | 6 | 10 | 11 | 14 | - |
|  |  |  |  |  |  |  | 1000 | 40 | 9 | 10 | 13 | 18 | 23 | -10 |
|  |  |  |  |  |  |  | 1200 | 30 | 12 | 15 | 25 | 42 | 43 | -110 |
| 4380 | 0.76 | 0.91 | 1.67 | 1.11 | 0.21 | 1450 | 800 | 49 | 4 | 5 | 8 | 9 | 10 | - |
|  |  |  |  |  |  |  | 1000 | 42 | 8 | 8 | 10 | 12 | 15 | 60 |
|  |  |  |  |  |  |  | 1200 | 31 | 5 | 11 | 19 | 33 | 38 | -50 |
| 4620 | 0.20 | 0.67 | 1.85 | 0.30 | 0.18 | 1650 | 300 | 42 | 14 | 20 | 28 | 35 | 35 | - |
|  |  |  |  |  |  |  | 800 | 34 | 11 | 16 | 33 | 55 | 55 | - |
|  |  |  |  |  |  |  | 1000 | 29 | 16 | 34 | 55 | 78 | 78 | - |
|  |  |  |  |  |  |  | 1200 | 19 | 17 | 48 | 103 | 115 | 117 | - |
| 4640 | 0.43 | 0.69 | 1.78 | 0.29 | 0.20 | 1550 | 800 | 42 | 16 | 17 | 20 | 25 | 27 | - |
|  |  |  |  |  |  |  | 1000 | 37 | 17 | 22 | 35 | 39 | 69 | -190 |
|  |  |  |  |  |  |  | 1200 | 29 | 17 | 30 | 55 | 97 | 67 | -180 |
| 4680 | 0.74 | 0.77 | 1.81 | 0.30 | 0.21 | 1450 | 800 | 46 | 5 | 8 | 13 | 15 | 16 | - |
|  |  |  |  |  |  |  | 1000 | 41 | 11 | 12 | 15 | 19 | 22 | - |
|  |  |  |  |  |  |  | 1200 | 31 | 11 | 13 | 17 | 39 | 43 | - |
| 8620 | 0.20 | 0.89 | 0.60 | 0.68 | 0.20 | 1650 | 300 | 43 | 11 | 16 | 23 | 35 | 35 | - |
|  |  |  |  |  |  |  | 800 | 36 | 8 | 13 | 20 | 35 | 45 | -20 |
|  |  |  |  |  |  |  | 1000 | 29 | 25 | 33 | 65 | 76 | 76 | -150 |
|  |  |  |  |  |  |  | 1200 | 21 | 10 | 85 | 107 | 115 | 117 | -195 |
| 8630 | 0.34 | 0.77 | 0.66 | 0.62 | 0.22 | 1575 | 800 | 41 | 7 | 12 | 17 | 25 | 31 | 0 |
|  |  |  |  |  |  |  | 1000 | 34 | 11 | 20 | 43 | 53 | 54 | -155 |
|  |  |  |  |  |  |  | 1200 | 27 | 18 | 28 | 74 | 80 | 82 | -165 |
| 8640 | 0.45 | 0.78 | 0.65 | 0.61 | 0.20 | 1550 | 800 | 46 | 5 | 10 | 14 | 20 | 23 | - |
|  |  |  |  |  |  |  | 1000 | 38 | 11 | 15 | 24 | 40 | 40 | -110 |
|  |  |  |  |  |  |  | 1200 | 30 | 18 | 22 | 49 | 63 | 66 | -140 |
| 8660 | 0.56 | 0.81 | 0.70 | 0.56 | 0.25 | 1475 | 800 | 47 | 4 | 6 | 10 | 13 | 16 | - |
|  |  |  |  |  |  |  | 1000 | 41 | 10 | 12 | 15 | 20 | 30 | -10 |
|  |  |  |  |  |  |  | 1200 | 30 | 16 | 18 | 25 | 54 | 60 | -90 |



FIG. 21


FIG. 22

## Standard Inch Socket Head Cap Screws Are Not Grade 8 Fasteners

There is a common, yet reasonable, misconception that standard, inch, alloy steel socket head cap screws are "Grade 8". This is not true. The misconception is reasonable because "Grade 8" is a term generally associated with "high strength" fasteners. A person desiring a "high strength" SHCS may request a "Grade 8 SHCS". This is technically incorrect for standard SHCSs. The term Grade 8 defines specific fastener characteristics which must
be met to be called "Grade 8". Three of the most important characteristics are not consistent with requirements for industry standard SHCSs: tensile strength, hardness, and head marking. Some basic differences between several fastener classifications are listed below. The list is not comprehensive but intended to provide a general understanding. SHCSs can be manufactured to meet Grade 8 requirements on a special order basis.

| Fastener Designation | Grade2 | Grade5 | Grade8 | $\begin{aligned} & \text { Industry } \\ & \text { SHCS } \end{aligned}$ | Unbrako SHCS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Strength Level, UTS KSI, min. | 74 <br> (1/4-3/4) <br> 60 <br> (7/8-1 1/2) | $\begin{aligned} & 120 \\ & (1 / 4-1) \\ & 105 \\ & (11 / 8-11 / 2) \end{aligned}$ | $\begin{aligned} & 150 \\ & (1 / 4-11 / 2) \end{aligned}$ | $\begin{aligned} & 180 \\ & (\leq 1 / 2) \\ & 170 \\ & (>1 / 2) \end{aligned}$ | $\begin{aligned} & 190 \\ & (\leq 1 / 2) \\ & 180 \\ & (>1 / 2) \end{aligned}$ |
| Hardness, Rockwell | $\begin{aligned} & \text { B80-B100 } \\ & \text { B70-B100 } \end{aligned}$ | $\begin{aligned} & \text { C25-C34 } \\ & \text { C19-C30 } \end{aligned}$ | C33-C39 | $\begin{aligned} & \text { C39-C45 } \\ & \text { C37-C45 } \end{aligned}$ | $\begin{aligned} & \mathrm{C} 39-\mathrm{C} 43 \\ & \mathrm{C} 38-\mathrm{C} 43 \end{aligned}$ |
| General Material Type | Low or Medium Carbon Steel | Medium <br> Carbon Steel | Medium <br> Carbon Alloy <br> Steel | Medium <br> Carbon Alloy <br> Steel | Medium <br> Carbon Alloy <br> Steel |
| Identification Requirement | None | Three Radial Lines | Six Radial Lines | SHCS Configuration | Mfr's ID |
| Typical Fasteners | Bolts Screws <br> Studs Hex Heads | Bolts Screws <br> Studs Hex Heads | Bolts Screws <br> Studs Hex Heads | Socket Head Cap Screw | Socket Head Cap Screw |

## THREADS IN BOTH SYSTEMS

Thread forms and designations have been the subject of many long and arduous battles through the years. Standardization in the inch series has come through many channels, but the present unified thread form could be considered to be the standard for many threaded products, particularly high strength ones such as socket head cap screws, etc. In common usage in U.S.A., Canada and United Kingdom are the Unified National Radius Coarse series, designated UNRC, Unified National Radius Fine series, designated UNRF, and several special series of various types, designated UNS.

This thread, UNRC or UNRF, is designated by specifying the diameter and threads per inch along with the suffix indicating the thread series, such as $1 / 4-28$ UNRF. For threads in Metric units, a similar approach is used, but with some slight variations. A diameter and pitch are used to designate the series, as in the Inch system, with modifications as follows: For coarse threads, only the prefix M and the diameter are necessary, but for fine threads, the pitch is shown as a suffix. For example, M16 is a coarse thread designation representing a diameter of 16 mm with a pitch of 2 mm understood. A similar fine thread part would be M16 x 1.5 or 16 mm diameter with a pitch of 1.5 mm .

For someone who has been using the Inch system, there are a couple of differences that can be a little confusing. In the Inch series, while we refer to threads per inch as pitch; actually the number of threads is $1 /$ pitch. Fine threads are referenced by a larger number than coarse threads because they "fit" more threads per inch.

In Metric series, the diameters are in millimeters, but the pitch is really the pitch. Consequently the coarse thread has the large number. The most common metric thread is the coarse thread and falls generally between the inch coarse and fine series for a comparable diameter.

Also to be considered in defining threads is the tolerance and class of fit to which they are made. The International Standards Organization (ISO) metric system provides for this designation by adding letters and numbers in a certain sequence to the callout. For instance, a thread designated as $\mathrm{M} 5 \times 0.84 \mathrm{~g} 6 \mathrm{~g}$ would define a thread of 5 mm diameter, 0.8 mm pitch, with a pitch diameter tolerance grade 6 and allowance " $g$ ". These tolerances and fields are defined as shown below, similar to the Federal Standard H28 handbook, which defines all of the dimensions and tolerances for a thread in the inch series. The callout above is similar to a designation class 3A fit, and has a like connotation.

## COMPLETE DESIGNATIONS



Example of thread tolerance positions and magnitudes.
Comparision 5/16 UNC and M8. Medium tolerance grades - Pitch diameter.

DEVIATIONS

| external | internal | basic clearance |
| :---: | :---: | :---: |
| h | H | none |
| g | G | small |
| e |  | large |

NOTES:
Lower case letters = external threads
Capital letters = internal threads

Close Fit: Normally limited to holes for those lengths of screws threaded to the head in assemblies in which: (1) only one screw is used; or (2) two or more screws are used and the mating holes are produced at assembly or by matched and coordinated tooling.

Normal Fit: Intended for: (1) screws of relatively long length; or (2) assemblies that involve two or more screws and where the mating holes are produced by conventional tolerancing methods. It provides for the maximum allowable eccentricity of the longest standard screws and for certain deviations in the parts being fastened, such as deviations in hole straightness; angularity between the axis of the tapped hole and that of the hole for the shank; differences in center distances of the mating holes and other deviations.

Chamfering: It is considered good practice to chamfer or break the edges of holes that are smaller than " $F$ " maximum in parts in which hardness approaches, equals or exceeds the screw hardness. If holes are not chamfered, the heads may not seat properly or the sharp edges may deform the fillets on the screws, making them susceptible to fatigue in applications that involve dynamic loading. The chamfers, however, should not be larger than needed to ensure that the heads seat properly or that the fillet on the screw is not deformed. Normally, the chamfers do not need to exceed "F" maximum. Chamfers exceeding these values reduce the effective bearing area and introduce the possibility of indentation when the parts fastened are softer than screws, or the possibility of brinnelling of the heads of the screws when the parts are harder than the screws.


| $\begin{aligned} & \text { nominal } \\ & \text { size } \end{aligned}$ | basic screw diameter | A |  |  |  | X | C | hole dimensions |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | drill size for hole A |  |  |  | counterbore diameter | countersink diameter D$\text { Max. }+2 \text { F(Max.) }$ | tap drill size |  | **body drill size | counterbore size |
|  |  | close fit |  | normal fit |  |  |  |  |  |  |  |
|  |  | nom. | dec. | nom. | dec. |  |  | UNRC | UNRF |  |  |
| 0 | 0.0600 | 51* | 0.0670 | 49* | 0.0730 | 1/8 | 0.074 | - | 3/64 | \#51 | 1/8 |
| 1 | 0.0730 | 46* | 0.0810 | 43* | 0.0890 | 5/32 | 0.087 | 1.5 mm | \#53 | \#46 | 5/32 |
| 2 | 0.0860 | 3/32 | 0.0937 | 36* | 0.1065 | 3/16 | 0.102 | \#50 | \#50 | 3/32 | 3/16 |
| 3 | 0.0990 | 36* | 0.1065 | 31* | 0.1200 | 7/32 | 0.115 | \#47 | \#45 | \#36 | 7/32 |
| 4 | 0.1120 | 1/8 | 0.1250 | 29* | 0.1360 | 7/32 | 0.130 | \#43 | \#42 | 1/8 | 7/32 |
| 5 | 0.1250 | 9/64 | 0.1406 | 23* | 0.1540 | 1/4 | 0.145 | \#38 | \#38 | 9/64 | 1/4 |
| 6 | 0.1380 | 23* | 0.1540 | 18* | 0.1695 | 9/32 | 0.158 | \#36 | \#33 | \#23 | 9/32 |
| 8 | 0.1640 | 15* | 0.1800 | 10 | 0.1935 | 5/16 | 0.188 | \#29 | \#29 | \#15 | 5/16 |
| 10 | 0.1900 | 5* | 0.2055 | 2* | 0.2210 | 3/8 | 0.218 | \#25 | \#21 | \#5 | 3/8 |
| 1/4 | 0.2500 | 17/64 | 0.2656 | 9/32 | 0.2812 | 7/16 | 0.278 | \#7 | \#3 | 17/64 | 7/16 |
| 5/16 | 0.3125 | 21/64 | 0.3281 | 11/32 | 0.3437 | 17/32 | 0.346 | F | I | 21/64 | 17/32 |
| 3/8 | 0.0375 | 25/64 | 0.3906 | 13/32 | 0.4062 | 5/8 | 0.415 | 5/16 | Q | 25/64 | 5/8 |
| 7/16 | 0.4375 | 29/64 | 0.4531 | 15/32 | 0.4687 | 23/32 | 0.483 | U | 25/64 | 29/64 | 23/32 |
| 1/2 | 0.5000 | 33/64 | 0.5156 | 17/32 | 0.5312 | 13/16 | 0.552 | 27/64 | 29/64 | 33/64 | 13/16 |
| 5/8 | 0.6250 | 41/64 | 0.6406 | 21/32 | 0.6562 | 1 | 0.689 | 35/64 | 14.5 mm | 41/64 | 1 |
| 3/4 | 0.7500 | 49/64 | 0.7656 | 25/32 | 0.7812 | 1-3/16 | 0.828 | 21/32 | 11/16 | 49/64 | 1-3/16 |
| 7/8 | 0.8750 | 57/64 | 0.8906 | 29/32 | 0.9062 | 1-3/8 | 0.963 | 49/64 | 20.5 mm | 57/64 | 1-3/8 |
| 1 | 1.0000 | 1-1/64 | 1.0156 | 1-1/32 | 1.0312 | 1-5/8 | 1.100 | 7/8 | 59/64 | 1-1/64 | 1-5/8 |
| 1-1/4 | 1.2500 | 1-9/32 | 1.2812 | 1-5/32 | 1.3125 | 2 | 1.370 | 1-7/64 | 1-11/64 | 1-9/32 | 2 |
| 1-1/2 | 1.5000 | 1-17/32 | 1.5312 | 1-9/16 | 1.5625 | 2-3/8 | 1.640 | 34 mm | 36 mm | 1-17/32 | 2-3/8 |

[^4]
## DRILL AND COUNTERBORE SIZES FOR METRIC SOCKET HEAD CAP SCREWS



| $\begin{aligned} & \text { Nominal Size } \\ & \text { or Basic } \\ & \text { Screw Diameter } \end{aligned}$ | A |  | $x$ | $Y$ |
| :---: | :---: | :---: | :---: | :---: |
|  | Nominal Drill Size |  | Counterbore Diameter | Countersink Diameter [Note (1)] |
|  | Close Fit <br> [Note (2)] | Normal Fit [Note (3)] |  |  |
| M1.6 | 1.80 | 1.95 | 3.50 | 2.0 |
| M2 | 2.20 | 2.40 | 4.40 | 2.6 |
| M2.5 | 2.70 | 3.00 | 5.40 | 3.1 |
| M3 | 3.40 | 3.70 | 6.50 | 3.6 |
| M4 | 4.40 | 4.80 | 8.25 | 4.7 |
| M5 | 5.40 | 5.80 | 9.75 | 5.7 |
| M6 | 6.40 | 6.80 | 11.25 | 6.8 |
| M8 | 8.40 | 8.80 | 14.25 | 9.2 |
| M10 | 10.50 | 10.80 | 17.25 | 11.2 |
| M12 | 12.50 | 12.80 | 19.25 | 14.2 |
| M14 | 14.50 | 14.75 | 22.25 | 16.2 |
| M16 | 16.50 | 16.75 | 25.50 | 18.2 |
| M20 | 20.50 | 20.75 | 31.50 | 22.4 |
| M24 | 24.50 | 24.75 | 37.50 | 26.4 |
| M30 | 30.75 | 31.75 | 47.50 | 33.4 |
| M36 | 37.00 | 37.50 | 56.50 | 39.4 |
| M42 | 43.00 | 44.00 | 66.00 | 45.6 |
| M48 | 49.00 | 50.00 | 75.00 | 52.6 |

ASTM Hardness Conversion Tables
ASTM Spec. E140 Based on Rockwell C (Non-austenitic steels)

|  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C | A | D | 15N | 30N | 45N | HB | HV | KSI |
| 68 | 85.6 | 76.9 | 93.2 | 844 | 75.4 |  | 940 |  |
| 67 | 85 | 76.1 | 92.9 | 83.6 | 74.2 |  | 900 |  |
| 66 | 84.5 | 75.4 | 92.5 | 82.8 | 73.3 |  | 865 |  |
| 65 | 83.9 | 74.5 | 92.2 | 81.9 | 72 | 739 | 832 |  |
| 64 | 83.4 | 73.8 | 91.8 | 81.1 | 71 | 722 | 800 |  |
| 63 | 82.8 | 73 | 91.4 | 80.1 | 69.9 | 705 | 772 |  |
| 62 | 82.3 | 72.2 | 91.1 | 79.3 | 68.8 | 688 | 746 |  |
| 61 | 81.8 | 71.5 | 90.7 | 78.4 | 67.7 | 670 | 720 |  |
| 60 | 81.2 | 70.7 | 90.2 | 77.5 | 66.6 | 654 | 697 |  |
| 59 | 80.7 | 69.9 | 89.8 | 76.6 | 65.5 | 634 | 674 |  |
| 58 | 80.1 | 69.2 | 89.3 | 75.7 | 64.3 | 615 | 653 |  |
| 57 | 79.6 | 68.5 | 88.9 | 74.8 | 63.2 | 595 | 633 |  |
| 56 | 79 | 67.7 | 88.3 | 73.9 | 62 | 577 | 613 |  |
| 55 | 78.5 | 66.9 | 87.9 | 73 | 60.9 | 560 | 595 | 301 |
| 54 | 78 | 66.1 | 87.4 | 72 | 59.8 | 543 | 577 | 291 |
| 53 | 77.4 | 65.4 | 86.9 | 71.2 | 58.6 | 525 | 560 | 283 |
| 52 | 76.8 | 64.6 | 86.4 | 70.2 | 57.4 | 512 | 544 | 273 |
| 51 | 76.3 | 63.8 | 85.9 | 69.4 | 56.1 | 496 | 528 | 264 |
| 50 | 75.9 | 63.1 | 85.5 | 68.5 | 55 | 481 | 513 | 256 |
| 49 | 75.2 | 62.1 | 85 | 67.6 | 53.8 | 469 | 498 | 246 |
| 48 | 74.7 | 61.4 | 84.5 | 66.7 | 52.5 | 455 | 484 | 237 |
| 47 | 74.1 | 60.8 | 83.9 | 65.8 | 51.4 | 443 | 471 | 231 |
| 46 | 73.6 | 60 | 83.5 | 64.8 | 50.3 | 432 | 458 | 221 |
| 45 | 73.1 | 59.2 | 83 | 64 | 49 | 421 | 446 | 215 |
| 44 | 72.5 | 68.5 | 82.5 | 63.1 | 47.8 | 409 | 434 | 208 |
| 43 | 72 | 57.7 | 82 | 62.2 | 46.7 | 400 | 423 | 201 |
| 42 | 71.5 | 56.9 | 81.5 | 61.3 | 45.5 | 390 | 412 | 194 |
| 41 | 70.9 | 56.2 | 80.9 | 60.4 | 44.3 | 381 | 402 | 188 |
| 40 | 70.4 | 55.4 | 80.4 | 59.5 | 43.1 | 371 | 392 | 181 |
| 39 | 69.9 | 54.6 | 79.9 | 58.6 | 41.9 | 362 | 382 | 176 |
| 38 | 69.4 | 53.8 | 79.4 | 57.7 | 40.8 | 353 | 372 | 170 |
| 37 | 68.9 | 53.1 | 78.8 | 56.8 | 39.6 | 344 | 363 | 165 |
| 36 | 68.4 | 52.3 | 78.3 | 55.9 | 38.4 | 336 | 354 | 160 |
| 35 | 67.9 | 51.5 | 77.7 | 55 | 37.2 | 327 | 345 | 155 |
| 34 | 67.4 | 50.8 | 77.2 | 54.2 | 36.1 | 319 | 336 | 150 |
| 33 | 66.8 | 50 | 76.6 | 53.3 | 34.9 | 311 | 327 | 147 |
| 32 | 66.3 | 49.2 | 76.1 | 52.1 | 33.7 | 301 | 318 | 142 |
| 31 | 65.8 | 48.4 | 75.6 | 51.3 | 32.5 | 294 | 310 | 139 |
| 30 | 65.3 | 47.7 | 75 | 50.4 | 31.3 | 286 | 302 | 136 |
| 29 | 64.6 | 47 | 74.5 | 49.5 | 30.1 | 279 | 294 | 132 |
| 28 | 64.3 | 46.1 | 73.9 | 48.6 | 28.9 | 271 | 286 | 129 |
| 27 | 63.8 | 45.2 | 73.3 | 47.7 | 27.8 | 264 | 279 | 126 |
| 26 | 63.3 | 44.6 | 72.8 | 46.8 | 26.7 | 258 | 272 | 123 |
| 25 | 62.8 | 43.8 | 72.2 | 45.9 | 25.5 | 253 | 266 | 120 |
| 24 | 62.4 | 43.1 | 71.6 | 45 | 24.3 | 247 | 260 | 118 |
| 23 | 62 | 42.1 | 71 | 44 | 23.1 | 243 | 254 | 115 |
| 22 | 61.5 | 41.6 | 70.5 | 43.2 | 22 | 237 | 248 | 112 |
| 21 | 61 | 40.9 | 69.9 | 42.3 | 20.7 | 231 | 243 | 110 |
| 20 | 60.5 | 40.1 | 69.4 | 41.5 | 19.6 | 226 | 238 | 104 |

* Numbers above BHN 615 are outside recommended range for Brinell testing ASTM method F10
** Tensile Strength in relation to hardness is inexac unless determined for specific material

STRESS AREAS FOR THREADED FASTENERS - INCH

| Diameter (in.) |  | Diameter (mm) | Threads Per in. |  | Square Inches |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Tensile Stress Area Per H-28 |  |  | Nominal Shank |
|  |  | UNRC | UNRF | UNRC |  | UNRF |
| \#0 | 0.06 |  | 1.52 | - | 80 | - | 0.00180 | 0.002827 |
| \#1 | 0.07 |  | 1.85 | 64 | 72 | 0.00263 | 0.00278 | 0.004185 |
| \#2 | 0.09 | 2.18 | 56 | 64 | 0.00370 | 0.00394 | 0.005809 |
| \#3 | 0.10 | 2.51 | 48 | 56 | 0.00487 | 0.00523 | 0.007698 |
| \#4 | 0.11 | 2.84 | 40 | 48 | 0.00604 | 0.00661 | 0.009852 |
| \#5 | 0.13 | 3.18 | 40 | 44 | 0.00796 | 0.00830 | 0.012272 |
| \#6 | 0.14 | 3.51 | 32 | 40 | 0.00909 | 0.01015 | 0.014957 |
| \#8 | 0.16 | 4.17 | 32 | 36 | 0.0140 | 0.01474 | 0.021124 |
| \#10 | 0.19 | 4.83 | 24 | 32 | 0.0175 | 0.0200 | 0.028353 |
| 1/4 | 0.25 | 6.35 | 20 | 28 | 0.0318 | 0.0364 | 0.049087 |
| 5/16 | 0.31 | 7.94 | 18 | 24 | 0.0524 | 0.0580 | 0.076699 |
| 3/8 | 0.38 | 9.53 | 16 | 24 | 0.0775 | 0.0878 | 0.11045 |
| 7/16 | 0.44 | 11.11 | 14 | 20 | 0.1063 | 0.1187 | 0.15033 |
| 1/2 | 0.50 | 12.70 | 13 | 20 | 0.1419 | 0.1599 | 0.19635 |
| 9/16 | 0.56 | 14.29 | 12 | 18 | 0.182 | 0.203 | 0.25 |
| 5/8 | 0.63 | 15.88 | 11 | 18 | 0.226 | 0.256 | 0.31 |
| 3/4 | 0.75 | 19.05 | 10 | 16 | 0.334 | 0.373 | 0.44179 |
| 7/8 | 0.88 | 22.23 | 9 | 14 | 0.462 | 0.509 | 0.60132 |
| 1 | 1.00 | 25.40 | 8 | 12 | 0.606 | 0.663 | 0.79 |
| 1-1/8 | 1.13 | 28.58 | 7 | 12 | 0.763 | 0.856 | 0.99402 |
| 1-1/4 | 1.25 | 31.75 | 7 | 12 | 0.969 | 1.073 | 1.2272 |
| 1-3/8 | 1.38 | 34.93 | 6 | 12 | 1.155 | 1.315 | 1.4849 |
| 1-1/2 | 1.50 | 38.10 | 6 | 12 | 1.405 | 1.581 | 1.7671 |
| 1-3/4 | 1.75 | 44.45 | 5 | 12 | 1.90 | 2.19 | 2.4053 |
| 2 | 2.00 | 50.80 | 4-1/2 | 12 | 2.50 | 2.89 | 3.1416 |
| 2-1/4 | 2.25 | 57.15 | 4-1/2 | 12 | 3.25 | 3.69 | 3.9761 |
| 2-1/2 | 2.50 | 63.50 | 4 | 12 | 4.00 | 4.60 | 4.9088 |
| 2-3/4 | 2.75 | 69.85 | 4 | 12 | 4.93 | 5.59 | 5.9396 |
| 3 | 3.00 | 76.20 | 4 | 12 | 5.97 | 6.69 | 7.0686 |

STRESS AREAS FOR THREADED FASTENERS — METRIC

| Nominal Dia. Thread <br> and Pitch <br> $(\mathbf{m m})$ | Thread Tensile <br> Stress Area <br> $\left(\mathbf{m m}^{2}\right)$ | Nominal <br> Shank Area <br> $\left(\mathbf{m m}^{2}\right)$ |
| :---: | :---: | :---: |
| $1.6 \times 0.35$ | 1.27 | 2.01 |
| $2.0 \times 0.4$ | 2.07 | 3.14 |
| $2.5 \times 0.45$ | 3.39 | 4.91 |
| $3.0 \times 0.5$ | 5.03 | 7.07 |
| $4.0 \times 0.7$ | 8.78 | 12.6 |
| $5.0 \times 0.8$ | 14.2 | 19.6 |
| $6.0 \times 1$ | 20.1 | 28.3 |
| $8.0 \times 1.25$ | 36.6 | 50.3 |
| $10 \times 1.5$ | 58.00 | 78.5 |
| $12 \times 1.75$ | 84.3 | 113 |
| $14 \times 2$ | 115 | 154 |
| $16 \times 2$ | 157 | 201 |


| Nominal Dia. Thread <br> and Pitch <br> $(\mathbf{m m})$ | Thread Tensile <br> Stress Area <br> $\left(\mathbf{m m}^{2}\right)$ | Nominal <br> Shank Area <br> $\left(\mathbf{m m}^{2}\right)$ |
| :---: | :---: | :---: |
| $18 \times 2.5$ | 192 | 254 |
| $20 \times 2.5$ | 245 | 314 |
| $22 \times 2.5$ | 303 | 380 |
| $24 \times 3$ | 353 | 452 |
| $27 \times 3$ | 459 | 573 |
| $30 \times 3.5$ | 561 | 707 |
| $33 \times 3.5$ | 694 | 855 |
| $36 \times 4$ | 817 | 1018 |
| $42 \times 4.5$ | 1120 | 1385 |
| $48 \times 5$ | 1470 | 1810 |


| METRIC PRODUCTS |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SIZE | THREAD PITCH \& T.P.I. |  |  |  | Major Dia |  |
|  | COARSE |  | FINE |  |  |  |
|  | PITCH mm | T.P.I. | PITCH mm | T.P.I. | mm | inch |
| M3 | 0.50 | 51 | - | - | 3.00 | 0.118 |
| M4 | 0.70 | 36 | - | - | 4.00 | 0.157 |
| M5 | 0.80 | 32 | - | - | 5.00 | 0.197 |
| M6 | 1.00 | 25 | - | - | 6.00 | 0.236 |
| M8 | 1.25 | 20 | 1.00 | 25 | 8.00 | 0.315 |
| M10 | 1.50 | 17 | 1.25 | 20 | 10.00 | 0.394 |
| M12 | 1.75 | 14.50 | 1.25 | 20 | 12.00 | 0.472 |
| (M14) | 2.00 | 12.50 | 1.50 | 17 | 14.00 | 0.551 |
| M16 | 2.00 | 12.50 | 1.50 | 17 | 16.00 | 0.630 |
| (M18) | 2.50 | 10 | 1.50 | 17 | 18.00 | 0.709 |
| M20 | 2.50 | 10 | 1.50 | 17 | 20.00 | 0.787 |
| (M22) | 2.50 | 10 | 1.50 | 17 | 22.00 | 0.866 |
| M24 | 3.00 | 8.50 | 2.00 | 12.50 | 24.00 | 0.945 |
| (M27) | 3.00 | 8.50 | 2.00 | 12.50 | 27.00 | 1.063 |
| M30 | 3.50 | 7.25 | 2.00 | 12.50 | 30.00 | 1.181 |
| (M33) | 3.50 | 7.25 | 2.00 | 12.50 | 33.00 | 1.299 |
| M36 | 4.00 | 6.40 | 3.00 | 8.5 | 36.00 | 1.417 |
| (M39) | 4.00 | 6.40 | 3.00 | 8.5 | 39.00 | 1.535 |
| M42 | 4.50 | 5.60 | 3.00 | 8.5 | 42.00 | 1.653 |


| UNIFIED INCH PRODUCTS |  |  |  | B.S. INCH PRODUCTS |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SIZE | T.P.I. |  | Major Dia inch | SIZE | T.P.I. |  | Major Dia inch |
|  | UNC | UNF |  |  | BSW | BSF |  |
| \#5 | 40 | 44 | 0.125 | 1/8 | 40 | - | 0.125 |
| \#6 | 32 | 40 | 0.138 |  |  |  |  |
| \#8 | 32 | 36 | 0.164 |  |  |  |  |
| \#10 | 24 | 32 | 0.190 | 3/16 | 24 | 32 | 0.187 |
| 1/4 | 20 | 28 | 0.250 | 1/4 | 20 | 26 | 0.250 |
| 5/16 | 18 | 24 | 0.313 | 5/16 | 18 | 22 | 0.313 |
| 3/8 | 16 | 24 | 0.375 | 3/8 | 16 | 20 | 0.375 |
|  |  |  |  | 7/16 | 14 | 18 | 0.438 |
| 1/2 | 13 | 20 | 0.500 | 1/2 | 12 | 16 | 0.500 |
| 5/8 | 11 | 18 | 0.625 | 5/8 | 11 | 14 | 0.625 |
| 3/4 | 10 | 16 | 0.750 | 3/4 | 10 | 12 | 0.750 |
| 7/8 | 9 | 14 | 0.875 | 7/8 | 9 | 11 | 0.875 |
| 1 | 8 | 12 | 1.000 | 1 | 8 | 10 | 1.000 |
| $11 / 8$ | 7 | 12 | 1.125 | $11 / 8$ | 7 | 9 | 1.125 |
| $11 / 4$ | 7 | 12 | 1.250 | $11 / 4$ | 7 | 9 | 1.250 |
| $11 / 2$ | 6 | 12 | 1.500 | $11 / 2$ | 6 | 8 | 1.500 |


| SAE | $\begin{aligned} & \text { I.S. } \\ & \text { I.S.O. } \\ & \text { DIN } \end{aligned}$ | ULTIMATE TENSILE STRENGTH |  | YIELD STRENGTH MIN. |  | HARDNESS |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Newtons/mm ${ }^{2}$ Min (kgf/mm²) | Pounds/in ${ }^{2}$ <br> Min <br> (kgf/mm²) | Newtons $/ \mathrm{mm}^{2}$ (kgf/mm²) | Pounds/in ${ }^{2}$ <br> (kgf/mm²) | BHN | HRb | HRc |
| - | 4.6 | 400 (40.8) | - | 240 (24.5) | - | 114 / 238 | $67 / 99.5$ |  |
| Grade 1 |  |  | 60.000 (42.3) |  | 36,000 (25.4) | (121) / (241) | 70/100 |  |
|  | 4.8 | 420 (42.8) |  | 340 (34.7) |  | 124 / 238 | $71 / 99.5$ |  |
|  | 5.6 | 500 (51.0) |  | 300 (30.6) |  | 147 / 238 | 79 / 99.5 |  |
| Grade 2 |  |  | 74.000 (52.1) |  | 57,000 (40.2) | (154) / (241) | $80 / 100$ |  |
|  | 5.8 | 520 (53.0) |  | 420 (42.8) |  | 152 / 238 | 82 / 99.5 |  |
|  | 6.8 | 600 (61.2) |  | 480 (48.9) |  | 181 / 238 | 89 / 99.5 |  |
|  | 8.8 | $\begin{aligned} & 800 \leqslant M 16(81.6) \\ & 830 \geqslant \text { M16 (84.6) } \end{aligned}$ |  | $\begin{aligned} & 640 \text { (65.2) } \\ & 660 \text { (67.3) } \end{aligned}$ |  | $\begin{aligned} & 238 / 304 \\ & 242 / 319 \end{aligned}$ |  | $\begin{aligned} & 22 / 32 \\ & 23 / 34 \end{aligned}$ |
| Grade 5 |  |  | 1,20.000 (84.6) |  | 92,000 (64.8) | (266) / (318) |  | $25 / 34$ |
| Grade 8 |  |  | 1,50.000 (105.7) |  | 1,30,000 (91.6) | (311) / (362) |  | 33 / 39 |
|  | 10.9 | 1,040 (106.0) |  | 940 (95.8) |  | 304 / 362 |  | 32 / 39 |
|  | 12.9 | 1,220 (124.4) |  | 1100 (112.0) |  | 366 / 412 |  | $39 / 44$ |

notes
notes
$\stackrel{2}{2}$ 8

2
*


[^0]:    Sizes in brackets are non-preferred standards

[^1]:    Pieces per Box Property Class: 45 H

[^2]:    **Torque application only to minimum, nominal lengths shown or longer.

[^3]:    **Torque application only to minimum, nominal lengths shown or longer.

[^4]:    ** Break edge of body drill hole to clear screw fillet.

